ADOT

Prepared for: **Arizona Department of Transportation**



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In Association with EcoPlan, Wood, Corral Design Group, ACS, and **Newton Environmental Consulting**

Concept Report I-17, Anthem Way Traffic Interchange to Jct. SR 69 (Cordes Junction) MP 229-262 ADOT Project No. 17 MA 229 H6800 01L Federal Project No. STP-017-A(ARV)S **Phoenix – Cordes Junction Highway APRIL 2019**

Final Design



PROJECT DETERMINATION FORM

| Project Number and Federal ID | County and ADOT District | Project Name and Highway | Final Design Concept Report Date |
|-------------------------------|------------------------------|-----------------------------------|----------------------------------|
| 017 MA 229 H6800 01L | Maricopa, Yavapai Counties | I-17, Anthem Way TI to Jct. SR 69 | April 2019 |
| 017-A(ARV)S | Central, Northwest Districts | Phoenix-Cordes Junction Highway | |
| | | | |

Project Description: Widen I-17 Anthem Wy to Black Cyn City; construct flex lanes Black Cyn City to Sunset Point

| Exis | Existing | | Program Year | Programmed Budget | | Operating Partnership | | | | | |
|---------|----------|--|--------------|--------------------------------|--|-----------------------|---|---|---|---|-----|
| Program | | | 2020-2023 | \$207,800,000 | | Category | | | | | |
| | | | | DCR Construction Cost Estimate | | | | | | | |
| Yes | No | | | \$221,800,000 | | S | F | Т | D | Z | N/A |
| Х | | | | \$331,800,000 | | Х | | | | | |

Public Hearing: In the Highway Development Process, at least one public hearing or the opportunity for a hearing will be offered for any project that:

| Requires a significant amount of new right-of-way: |
|--|
| Substantially changes the layout or function of connecting roadway or the facility being improved; |
| Has a significant adverse impact on abutting real property; |

| | Otherwise has a significant social, economic, environmental or other effect |
|---|--|
| | Is controversial on environmental grounds; |
| | Or has significant floodplain encroachment |
| Х | None of the above conditions apply |

Recommends: Voc

| Yes: | <u>No:</u> | | | | |
|------|------------|--|---------|----------------------|-----------|
| | Х | Public Forum | | Environmental Catego | ry |
| | Х | Offer a combined Location / Design Hearing | Class 1 | Class II | Class III |
| | Х | Offer Separate Location/Design Hearing | | Х | |
| | Х | Hold a Design Public Hearing | | | |

DocuSigned by: - Larison 5/2/2019 salu Date

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Project Manager Major Projects 605E

Concur:

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|---------------------------|--|--------|
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| Gregory Byres | 5/3 | 3/2019 |
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| Alvin Stump, P.E. | District Engineer Northwest District F | Date 2800 |

Comments:

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Glossary of Acronyms and Abbreviations

| AA | aesthetic area |
|--------|--|
| AADT | annual average daily traffic |
| AASHTO | American Association of State Highway and Transportation Officials |
| ABC | accelerated bridge construction |
| AC | asphaltic concrete |
| AC | alternating current |
| ADEQ | Arizona Department of Environmental Quality |
| ADOT | Arizona Department of Transportation |
| AFNM | Agua Fria National Monument |
| AGFD | Arizona Game and Fish Department |
| ASLD | Arizona State Land Department |
| AT&T | American Telephone and Telegraph |
| BCC | Black Canyon City |
| BLM | Bureau of Land Management |
| CA | character area |
| CBC | concrete box culvert |
| CCTV | closed circuit television |
| CE | Categorical Exclusion |
| CIP | cast in place |
| CLOMR | Conditional Letter of Map Revision |
| CMP | corrugated metal pipe |
| COE | US Army Corps of Engineers |
| CV | connected vehicle |
| DCR | Design Concept Report |
| DDHV | directional design hourly volume |
| DEA | Draft Environmental Assessment |
| DMS | dynamic message sign |
| DPS | Department of Public Safety |
| DSRC | dedicated short range communications |
| EPA | Environmental Protection Agency |
| FEMA | Federal Emergency Management Agency |
| FHWA | Federal Highway Administration |
| FIRM | flood insurance rate map |
| FY | fiscal year |
| HSIP | Highway Safety Improvement Program |
| I-10 | Interstate 10 |
| I-17 | Interstate 17 |
| I-40 | Interstate 40 |
| ICO | Issues, concerns, and opportunities |
| IDCR | Initial Design Concept Report |
| IHSDM | Interactive Highway Safety Design Model |
| ITS | Intelligent Transportation Systems |
| LED | light emitting diode |
| LOS | Level of Service |
| LRTP | Long Range Transportation Plan |
| MP | mile post |
| mph | miles per hour |
| | |

| MUTCD NB | Manual on Uniform Traffic Control Devices |
|-------------|---|
| NEPA | National Environmental Policy Act |
| NISCP | Noxious and Invasive Species Control Plan |
| PFI | Planning and Environmental Linkages |
| RCBC | reinforced concrete box culvert |
| RDG | Roadway Design Guidelines |
| RDS | Roadside Design Section (ADOT) |
| RHRS | Rock Hazard Rating System |
| RMP | Resource Management Plan |
| RPM | raised pavement marker |
| ROW | right-of-way |
| SB | southbound |
| SE | superelevation |
| SN | structural number |
| SR | State Route |
| SWPPP | Storm Water Pollution Prevention Plan |
| TI | traffic interchange |
| TOC | Traffic Operations Center |
| TSM&O | Transportation Systems Management and O |
| US | United States |
| USFWS | US Fish and Wildlife Service |
| USGS | US Geological Survey |
| Waters | Waters of the United States |
| Western | Western Area Power Administration |

Operations Group

EXECUTIVE SUMMARY

The Arizona Department of Transportation (ADOT), in partnership with the Federal Highway Administration (FHWA), has initiated Project No. 17 MA 229 H6800 01L [Federal Reference Number STP-017-A(ARV)S], a study to prepare the design concept for the addition of capacity to Interstate 17 (I-17) from the Anthem Way Traffic Interchange (TI) to the I-17 interchange with State Route 69 (SR 69). This project is located within the Arizona Department of Transportation's Central District and Northwest District in Maricopa and Yavapai counties. The overall study area begins at the I-17/Anthem Way TI at milepost (MP) 229.1 and extends north to the I-17/ SR 69 TI (also known as Cordes Junction) (MP 262.0).

ADOT has identified I-17 as a Key Commerce Corridor, which indicates that improvements to the transportation infrastructure support the greatest potential commercial and economic benefits. Key Commerce Corridors connect the major economic centers of Arizona with their major markets. As such, these inter-regional routes are the most essential for future, quality economic growth in Arizona and support high quality job growth. Efficient movement of supplies and goods support growth and expansion of base industries and the state's overall economy. The I-17 corridor is an important commerce and tourism corridor, connecting southern Arizona to northern Arizona. It connects the major east-west corridors of I-10 and I-40, facilitating the movement of goods, economic development, and tourism.

The study provides a long-range implementation strategy that will guide future decisions regarding the near-term and ultimate improvements to modify I-17 to meet the capacity and operational needs of the traveling public over the next 20-25 years. Implementation of the study recommendations will depend on funding availability and prioritization of roadway construction projects.

The No Build Alternative and Build alternatives were developed and evaluated for mainline I-17. The **Recommended Alternatives** are described as follows:

- In the near term, the **recommended widening** would provide an additional through lane in each direction between the Anthem Way TI and the Black Canyon City TI. It would add capacity in both directions, as well as match the improvements already completed south of the Anthem Way TI. This project is partially programmed for construction in fiscal year 2020.
- In the near term, two flex lanes would be constructed between Black Canyon City and Sunset Point. The flex lanes are new lanes that would be added along the median side of southbound I-17 and would be used by northbound traffic on Friday and Saturday and by southbound traffic on Sunday. It would add capacity in the peak direction, as well as provide flexibility for managing traffic during maintenance activities and crash-related restrictions.
- In the longer term, Alternative E is recommended, which would provide three southbound lanes on a new roadway alignment west of existing I-17 and four northbound lanes on the existing northbound and southbound roadways between Black Canyon City and Sunset Point. Alternative E would also widen the existing roadway between Sunset Point and Cordes Junction to three lanes in both directions. Constructing a new alignment provides incident management flexibility and opportunities for re-routing traffic for maintenance activities.

The Bureau of Land Management (BLM) manages nearly all of the land on both sides of I-17 and in several wide median areas between the existing northbound and southbound I-17 alignments. Approximately 4.5 acres of new right-of-way (ROW) and 2.9 acres of drainage easement are required for near-term improvements.

The following implementation strategy is recommended for the proposed improvements to I-17:

<u>Near Term</u>: Construct one additional general purpose lane in each direction from the Anthem Way TI to the Black Canyon City TI.

<u>Near Term</u>: Construct two flex lanes adjacent to existing SB I-17 from Black Canyon City to Sunset Point.

Long Term: Alternative E – construct two southbound lanes (three if the flex lanes were not previously constructed) on new alignment.

ADOT's Tentative 2020-2024 Five-Year Transportation Facilities Construction Program includes five line items for I-17 in the project area as shown in the table below.

| Beg. MP I-17 | County | ADOT District | Location | Type of Work | Length (mile) | Amount (in thousands) | Fiscal Year |
|-----------------|--------|------------------|---------------------------------------|---|------------------|----------------------------------|----------------------|
| 229 | | MAG | Anthem Way-Yavapai County Line, SB | Construct Widening ROW for Widening Design Widening | | \$40,000 \$5,000 \$5,000 | 2020 |
| 238 | MA | Northwest | Moores Gulch Bridge | Construct Bridge Replacement | 1 | \$10,500 | 2023 |
| 245 | YV | Northwest | Black Canyon – Sunset Point | Final Design Widen Roadway | 5 | \$15,000 \$62,402 \$65,907 | 2020 2021 2022 |
| 248 | YV | Northwest | Bumble Bee TI OP NB | Construct Bridge Rehabilitation | 1 | \$4,000 | 2020 |
| 252 | YV | Northwest | Sunset Point Rest Area | Design (Water & WW Repairs) Construct (Water & | | \$575 \$4,800 | 2021 2022 |

Work began on an Environmental Assessment (EA) in 2006; however, the scope of the environmental studies was reduced when FHWA/ADOT policies changed regarding the approval of environmental documents for projects that were not included in an approved transportation improvement program. A Planning and Environmental Linkages (PEL) Checklist was prepared in 2015 to document the efforts completed with the EA (e.g., biological resources, cultural resources), identify important issues identified during the study process, and provide a basis for identifying smaller projects which may accomplish some improvements at a lower cost. The preparation of a Categorical Exclusion (CE) is currently underway.

Additional reports prepared for this study include an AASHTO Controlling Design Criteria Report, Scoping Report, Preliminary Traffic Report, Preliminary Geotechnical Assessment, Preliminary Drainage Report, Cultural Resources Assessment, Visual Impact Assessment, Biological Evaluation, Air Quality Report, Preliminary Noise Analysis, Initial Site Assessment, and a Bridge Selection Report.

ADOT Multimodal Planning Division prepared a Corridor Profile Report for I-17 between Phoenix and Flagstaff in 2017. The profile study evaluated key performance measures relative to the I-17 corridor and used those measures as a means to set priorities for future improvements in areas that show critical deficiencies.

1.0 Introduction

Foreword 1.1

The Arizona Department of Transportation (ADOT), in partnership with the Federal Highway Administration (FHWA), has initiated a design concept study and related environmental studies to evaluate proposed improvements to Interstate 17 (I-17) in Maricopa and Yavapai counties, Arizona. The overall study area begins at the I-17/Anthem Way Traffic Interchange (TI) at milepost (MP) 229.1 and extends north to the I-17/Junction State Route 69 (SR 69) TI (Cordes Junction).

The design concept study area is located north of the Phoenix metropolitan area in south-central Arizona. The study area is located ADOT's Central and Northwest districts.

The study will provide a long-range implementation strategy that will guide future decisions regarding the interim and ultimate improvements required to modify I-17 to meet the capacity and operational needs of the traveling public over the next 20-25 years. A Categorical Exclusion is being prepared for I-17 between the Anthem Way TI and the Sunset Point TI. Implementation of the study recommendations will depend on funding availability and prioritization of roadway construction projects.

The functional classification for I-17 is Principal Arterial Interstate-Rural. The posted speed limit varies from 75 mph at the south end of the project, 65 mph in the Black Canyon Hill area (MP 244 to MP 252), and 75 mph from Sunset Point to Cordes Junction (MP 252 to MP 262).

Purpose of and Need for the Project

ADOT has identified I-17 as a Key Commerce Corridor, which indicates that improvements to the transportation infrastructure support the greatest potential commercial and economic benefits. Key Commerce Corridors connect the major economic centers of Arizona with their major markets. As such, these inter-regional routes are the most essential for future, guality economic growth in Arizona and supporting high guality job growth. Efficient movement of supplies and goods support growth and expansion of base industries and the state's overall economy. The I-17 corridor is an important commerce and tourism corridor, connecting southern Arizona to northern Arizona. It also connects the major east-west corridors of I-10 and I-40, two of the nation's principal east-west highways, and facilitates goods movement, economic development, and tourism.

The preliminary priorities list from ADOT's 2015 Passing Lane/Climbing Lane Study reflects the segment of northbound I-17 between MP 246 and MP 250 as the highest-ranked need for a climbing lane on multi-lane highways in the state of Arizona. Another segment of I-17 within the study area, northbound from MP 255 to MP 256, also ranks high on the statewide list.

The purpose of this project is to add capacity to and improve operations of I-17 from the Anthem Way TI to Cordes Junction. The study will develop and evaluate feasible alternatives for the future expansion of I-17, as well as near-term improvements, to improve traffic operations and to accommodate projected traffic volumes in the 2040 design year. The results of the engineering analyses are fully documented in this Design Concept Report (DCR).

North of the New River TI, most of the study route is located adjacent to land that is administered by the Bureau of Land Management (BLM), including the Agua Fria National Monument (AFNM) abutting the eastern ADOT right-of-way between MP 245.0 and MP 260.3. BLM also manages the land west of I-17 for most of the project length, as well as portions of the median area between northbound and southbound I-17. The Arizona State Land Department (ASLD) administers most of the remaining adjacent land; however, the adjacent land between Anthem Way TI and just north of New River Road TI is owned by the City of Phoenix or is privately-owned.

The existing roadway is a four-lane divided rural highway with full access control, traversing level to rolling to mountainous terrain. I-17 from the Anthem Way TI to New River TI is in level terrain, while New River TI to Black Canyon City TI is in rolling terrain. The mountainous terrain extends from approximately MP 244.5 to MP 250.5 (Black Canyon City to Sunset Point). The I-17 horizontal and vertical alignments in this mountainous terrain present challenges related to steep grades and horizontal curves with limited sight distance. In addition, crashes can result in closures of I-17 that cause lengthy travel delays along the route. I-17 experiences heavy volumes during weekends and holidays as the main route for traffic between the Phoenix metropolitan area, Flagstaff, and recreational destinations to the north. The combination of large volumes of passenger cars, trucks, and recreational vehicles results in a substantial speed differential condition on the steep grades of the Black Canyon Hill. This condition affects the operational capacity of the interstate and results in congestion and long traffic back-ups. There are distant detour options for long-term closures; however, there are no alternate routes in the area for short-term closures.

The remaining segments of the northbound and southbound alignments are located within rolling terrain from MP 250.5 to Cordes Junction at MP 262.0, the north end of the study area.

1.3 Description of the Project

The study area begins on I-17 at approximately MP 229, at its interchange with Anthem Way, and extends north to approximately MP 262, just south of the junction with SR 69. The I-17/SR 69 interchange, also known as the Cordes Junction TI, was reconstructed in 2013. A vicinity map detailing the study limits and the surrounding area is shown on Figure 1.

In the long term, constructing three southbound lanes on new alignment and converting the existing roadways to carry northbound traffic is recommended from MP 245 to MP 252 (approximately Black Canyon City to Sunset Point). The long-term project will add one new lane in each direction from MP 252 to MP 262 by widening to the inside of the existing northbound and southbound roadways.

In the nearer term, one additional through lane in each direction is recommended between Anthem Way and Black Canyon City, as well as two flex lanes on the Black Canyon Hill to add capacity and incident management flexibility.



1.4 **Project Objectives**

The addition of roadway capacity will help ADOT meet its long-range goal of providing an improved roadway from the Phoenix area to Flagstaff. Widening the roadway will lessen traffic congestion and improve the level of service.

The primary objectives of this study include the addition of mainline capacity to accommodate projected future traffic volumes. The addition of mainline lanes is anticipated to reduce congestion and travel times. The addition of an alternative alignment would provide flexibility for ADOT to more effectively manage incidents related to crashes, as well as relieve congestion and facilitate maintenance.

1.4.1 Public Involvement

To ensure that the community was given ample opportunity to provide comments and be involved in the development and evaluation of alternatives, this study included a public involvement process with public meetings, question and answer sessions, newspaper advertisements, and a project web site.

1.4.1.1 Scoping

ADOT initiated the I-17 design concept study in 2006 by conducting scoping meetings with federal, state, county, and local agency representatives and the public. The scoping meetings for the project were held on July 13, 2006, in Spring Valley, Arizona. The purpose of these meetings was to provide a general overview of the study area and to obtain information from the agency representatives, business people, and area residents about the existing roadway and surrounding area, and to identify the issues, concerns, and opportunities (ICOs) that should be addressed by the evaluation criteria for use during the development and analysis of alternatives in the DCR and environmental document.

1.4.1.2 Public Information Meetings

Public information meetings were held on January 23, 2007, in Black Canyon City at Cañon School and on January 25, 2007, in Spring Valley at Mayer Junior/Senior High School. In total, 116 community members attended the meetings. Seventy people attended the meeting in Black Canyon City; 12 comment forms were completed. Forty-six people attended the meeting in Spring Valley; eight comment forms were completed. The purpose of these meetings was to present the preliminary alternatives initially developed for study and to solicit public comments on the alternatives.

An additional public meeting was held on April 3, 2018, from 6:00 to 8:00 pm at Cañon Elementary School to provide the public an update on potential improvements along I-17 within the project area. The format for the meeting was an open house; 216 people signed in at the meeting. There were three areas with project study boards on display for attendees to view, ask questions directly of project team, and leave comments if desired. There were also two areas with video capability for the public to view areas of interest; this method was used in lieu of roll plot maps. A ten-minute PowerPoint presentation by Alvin Stump, Northwest District Engineer, provided the public with an overview/history of the project and descriptions of the current project, including a video simulation of the proposed flex lanes. There was no formal question and answer at the end of presentation; rather, the public was invited to visit display areas and remain as long as necessary to ask questions and obtain the information they desired.



1.4.1.3 Other Activities

Throughout the study duration, a project web site has been used to provide up-to-date study information and to collect feedback from the public. The current web site address is <u>https://www.azdot.gov/I17AnthemWaySR69</u>.

1.5 Characteristics of the Corridor

Interstate 17 extends north from Jct. I-10 in central Phoenix to its northern terminus in Flagstaff, connecting I-10 to I-40.

Table 1 lists the previous projects constructed within the study section, sorted by construction date.

| PROJECT NO. | BEG. MP | END MP | CONSTR. DATE | DESCRIPTION |
|--------------|---------|--------|-----------------|---|
| FAS-39(1947) | 225.1 | 230.6 | 1947 | GRADING & PAVING |
| NS 39(47)A | 225.1 | 231.88 | 1948 | BST |
| NS 39(48)A | 231.9 | 231.92 | 1948 | BRIDGE & ABUTMENTS |
| S 38(1) | 244.8 | 247.87 | 1948 | AGUA FRIA RIVER-ARRASTRE CREEK BST |
| S 39(4) | 232.1 | 236.55 | 1949 | BST |
| NS 38(50)A | 247.9 | 251.35 | 1949 | ROCK SPRINGS-CORDES JCT MBS |
| S 38(2) | 247.9 | 251.35 | 1949 | ARRASTRE CREEK-BLACK MESA BST |
| S 38(3) | 251.2 | 259.59 | 1949 | BLACK MESA STATION BST |
| NS 38(49)A | 251.4 | 262.9 | 1949 | ROCK SPRINGS-CORDES JCT MBS |
| NS 39(51)A | 220.5 | 234.5 | 1950 | PHOENIX - ROCK SPRINGS SEAL COAT |
| S 39(5) | 236.6 | 239.66 | 1950 | GD |
| S 39(6) | 236.6 | 242 | 1950 | BST |
| NS 38(50)C | 244.8 | 259.72 | 1950 | ROCK SPRINGS-CORDES JCT GUARD RAIL |
| 538(5) | 262 | 262 | 1950 | BIG BUG CREEK BRIDGE |
| S 38(5) | 259.7 | 262.21 | 1951 | BLACK MESA-CORDES JCT BST |
| NS 39(55)A | 229 | 236 | 1954 | NEW RIVER - TABLE MESA SEAL COAT |
| NS 38(54)A | 252.4 | 259.73 | 1954 | BADGER SPRINGS-SOUTH SEAL COAT |
| NF 156(56)A | 236.6 | 241.8 | 1955 | NEW RIVER - COUNTY LINE SEAL COAT |
| NF 156(56)B | 244.8 | 253.3 | 1955 | SPRINGS-NORTH SEAL COAT |
| FI 156(4) | 259.7 | 269.67 | 1955 | BIG BUG CREEK- CORDES JCT BST |
| F 003-2(58) | 217 | 229.7 | 1957 | PHOENIX - CORDES JUNCTION HWY SEAL COAT |
| NI 003-2-58A | 217 | 229.7 | 1957 | SKUNK CREEK BRIDGE – NORTH SEAL COAT |
| NI 17-1(60)A | 251 | 260 | 1959 | ROCK SPRINGS-CORDES JCT SEAL COAT |
| l 17-1(23) | 261 | 264 | 1960 | CORDES JCT-SOUTH AC |
| NI 17-1-501 | 228.5 | 234.5 | 1961 | BELL ROAD - YAVAPAI COUNTY LINE SEAL COAT |
| NI 17-1(61)A | 259.7 | 261.36 | 1961 | CORDES INTERCHANGE-SOUTH SEAL COAT |

TABLE 1 – PREVIOUS PROJECTS WITHIN STUDY AREA

| PROJECT NO. | BEG. MP | END MP | CONSTR. DATE | DESCRIPTION | |
|--------------|---------|--------|-----------------|---|--|
| l 17-1(56) | 220.5 | 225.08 | 1963 | AC PAVEMENT | |
| l 17-1(29)22 | 220.7 | 233.1 | 1963 | AC PAVEMENT | |
| l 17-1(44) | 254 | 260.98 | 1963 | BADGER SPRINGS-CORDES JCT OVERLAY | |
| I-17-1(57) | 225.1 | 230.57 | 1964 | AC PAVEMENT | |
| l 17-1(37) | 242.3 | 244.93 | 1964 | NORTH GD | |
| l 17-1(59) | 242.3 | 244.93 | 1964 | NORTH BC AC | |
| l 17-1(54) | 245 | 247.86 | 1964 | BLACK CYN-BUMBLE BEE TI (NB) GD | |
| l 17-1(62) | 236.8 | 243.11 | 1965 | AC PAVEMENT | |
| l 17-1-905 | 241.8 | 251.6 | 1965 | MARICOPA COUNTY LINE - NORTH SEAL COAT | |
| l 17-1-907 | 242 | | 1965 | NORTH CMP FOR ACCESS ROAD | |
| l 17-1(67) | 242.5 | | 1965 | GRADE SEPARATION/STRUCTURES | |
| l 17-1-503 | 244.8 | 245.19 | 1965 | BLACK CANYON TI REVAMP OFFRAMP | |
| l 17-1(60) | 248 | 250.37 | 1965 | BUMBLEE TI-SUNRISE PT GD/STR (NB) | |
| l 17-2(29) | 262 | 263 | 1965 | CORDES JCT INTERCHANGE LANDSCAPING | |
| l 17-1(61) | 230.5 | 236.33 | 1966 | AC | |
| l 17-1(55) | 245 | 254.18 | 1966 | BLACK CYN-BADGER SPRING (NB) BC-AC | |
| I-17-1(74) | 226.95 | | 1967 | | |
| l 17-1(65) | 245 | 254.13 | 1967 | BLACK CANYON-BADGER SPRING AC (SB) | |
| l 17-1-916 | 213.4 | 230.5 | 1968 | BELL ROAD – NEW RIVER SEAL COAT | |
| LSI 17-1(77) | 216.7 | 233.95 | 1968 | DEER VALLEY - BLACK CANYON TI LANDSCAPING | |
| l 17-1(70) | 242.1 | | 1969 | ROCK SPRINGS TI LIGHTING | |
| l 17-1-924 | 242.5 | 253 | 1969 | ROCK SPRINGS - CORDES JUNCTION SEAL COAT | |
| l 17-1(49) | 252 | 252 | 1969 | SUNSET POINT REST AREA FACILITIES | |
| l 17-1-926 | 252 | 252 | 1969 | SUNSET REST AREA TEST WELL | |
| l 17-1-929 | 213.4 | 241.6 | 1970 | BELL ROAD - YAVAPAI COUNTY LINE SEAL COAT | |
| I-17-1(113) | 232 | 232 | 1973 | NEW RIVER TI LIGHTING | |
| 17-2(22)64 | 261.4 | 262.3 | 1973 | CORDES JUNCTION TI | |
| l 17-1-951 | 229.1 | 233.1 | 1974 | DESERT HILLS - NEW RIVER SEAL COAT | |
| l 17-2-908 | 262 | 269.14 | 1974 | CORDES JCT-ASH CREEK SEAL COAT | |
| l 17-1-971 | 239.5 | | 1975 | SB REPAIR | |
| l 17-1(120) | 230.7 | 233.3 | 1976 | NEW RIVER TI SIGNING | |
| ER 17-1-988 | 243.3 | 243.5 | 1979 | AGUA FRIA RIVER BRIDGE – DEMOL (STRM) 12/78 SEE (139) | |
| l 17-1-989 | 243.3 | 243.3 | 1979 | AGUA FRIA RIVER BRIDGE 12/78 FLOOD DETOUR | |
| ER 17-1(139) | 243.4 | | 1979 | FLOOD DAMAGE | |
| I-17-1(994) | 231.4 | | 1980 | NEW RIVER BRIDGE MAINTENANCE | |
| l 17-1-995 | 248.4 | 248.4 | 1980 | BUMBLE BEE TI UP(SB) BRIDGE REPAIRS | |
| l 17-1(82) | 251 | 261.75 | 1980 | SUNSET PT TI-CORDES JCT TI SAFETY | |

| PROJECT NO. | BEG. MP | END MP | CONSTR. DATE | DESCRIPTION |
|------------------------|---------|--------|-----------------|--|
| l 17-1(136) | 220.5 | 236.62 | 1981 | RESURFACING |
| ER 17-1(144) | 252 | 252 | 1981 | SUNSET POINT REST AREA WATER LINE |
| l 17-1(145) | 252 | 252 | 1981 | SUNSET POINT REST AREA SEWER SYSTEM |
| IR 17-1(149) | 225 | 238 | 1983 | AC OVERLAY |
| l 17-1(83) | 236.6 | 251.6 | 1984 | TABLE MESA TI - SUNSET POINT TI PERMANENT SIGNING |
| IR 17-1(153) | 238 | 244 | 1984 | AC&ACFC |
| l 17-3-911 | 239.5 | | 1984 | SB REPAIR |
| IR 17-1(157) | 252.5 | 252.5 | 1984 | SUNSET POINT REST AREA INCREASE LGHTG |
| IR 17-1(159) | 244 | 250 | 1985 | ACFC |
| IR 17-1(164) | 250 | 256 | 1986 | SUNSET POINT-BADGER SPRINGS AC OVERLAY |
| IR 17-1(168) | 244 | 250.6 | 1989 | REMOVE /REPLACE |
| I-17-1-891 | 252 | 252 | 1989 | SUNSET POINT REST AREA VENDING MACHINES |
| IR 17-1(190) | 245 | 245 | 1991 | NB/SB BLACK CYN-SUNSET MILL REPL OLAY ACFC |
| l 17-1-514 | 251.8 | 251.8 | 1991 | SUNSET POINT R A INFO BOARD |
| ER 17-1(224) | 238 | 240 | 1993 | BANK PROTECTION/SPUR DYKE STR |
| MA 17-1(226) | 226 | 232 | 1994 | OVERLAY NB & SB LANES |
| ER-17-1-(224) | 238.2 | 239.55 | 1995 | SCOUR PROTECTION AT MOORES GULCH AND LITTLE SQUAW CREEK |
| IM-17-1(327) | 252.5 | 256.5 | 1998 | SUNSET PT TI-BADGER SPRINGS TI PVMT PRES |
| I-17-1-549 | 229 | 229 | 1999 | ANTHEM WAY TI |
| ITS-020-4(511)A | 245.5 | 300.5 | 2006 | INSTALLATION OF 511 SIGNING |
| 017 YV 250 H720501C | 250.4 | 252.5 | 2007 | MILL AND REPLACE (NB) |
| IM-017-A(213) | 229 | 279.34 | 2010 | ANTHEM WAY TO CHERRY RD SIGN REHABILITATION |
| 17-A(207)B | 229.17 | 224.32 | 2010 | SR 74 TO ANTHEM WAY – ROADWAY WIDENING |
| IM-HES-017- B(007)A | 245.00 | 254.90 | 2010 | MILL AND REPLACE, SAFETY IMPROVEMENTS |
| IM-017-1(345)A | 251.27 | 251.87 | 2010 | REST AREA REHABILITATION |
| 17-A(214)A | 239.36 | 239.74 | 2012 | SB BRIDGE REPLACEMENT & NB BRIDGE DECK REHABILITATION |
| STP-017-A(223)A | 251.27 | 251.87 | 2013 | SUNSET PT REST AREA REHABILITATION |
| IM-017-B(001)N | 261.52 | 263.68 | 2013 | RECONSTRUCT TI |
| IM-017-A(229)T | 245.0 | 250.4 | 2014 | COLDWATER CYN RD-CROWN KING RD (NB) |
| 17-A(226)T | 231 | 232 | 2017 | NEW RIVER BRIDGES – SCOUR RETROFIT |
| IM 17-1(220) | 216 | 280 | | PINNACLE PEAK ROAD - CHERRY ROAD SIGN UPDATE |
| IM 17-1(329) | 232 | 238.6 | | PHOENIX - CORDES JUNCTION HWY (I-17) - NEW RIVER - MOORES GULCH |
| N 900-0-538 | 232 | | | PRESCOTT DISTRICT I-17 MINOR TI IMPROVEMENT PROGRAM |

| PROJECT NO. | BEG. MP | END MP | CONSTR. DATE | |
|------------------|---------|--------|-----------------|---------------------|
| IM 17-1(342) | 238.55 | 245 | | PHOENIX - BLACK |
| IM 17-1(228) | 245 | 250.4 | | BLACK C |
| I 017-A-504 | 245.2 | 249.8 | | PHOENI> 249.8 |
| IM 17-1(340) | 246 | 252.5 | | PHX-CRI |
| AC IM-17-1(343)P | 250 | 250 | | PHX-CR |
| TEA 17-1(332) | 251.87 | 252.37 | | CONSTR |
| IM 17-1(341)P | 256 | 262.7 | | PHX-CR |
| AC- 017-B(005)A | 256.02 | 263.0 | | PHX-COF CREEK- I |

1.5.1 Roadway Characteristics

Traffic interchanges exist at the following locations:

TABLE 2 – ROADWAY CHARACTERISTICS

| I-17 CROSSING | MP | COMMENTS |
|-----------------------------|-------|-------------------------------------|
| Anthem Way TI | 229.1 | Southern study limit - c |
| New River TI | 232.0 | Diamond Interchange |
| Table Mesa TI | 236.0 | Trumpet-type Intercha |
| Rock Springs TI | 242.2 | Diamond Interchange |
| Black Canyon City TI | 244.4 | Diamond Interchange |
| Bumble Bee TI | 248.4 | Diamond Interchange |
| Sunset Point TI / Rest Area | 252.5 | Rest area in southwes |
| Badger Springs TI | 256.1 | Diamond Interchange |
| Bloody Basin TI | 259.4 | Diamond Interchange |
| Big Bug Creek bridges | 262.0 | Northern study limit |
| SR 69 / Cordes Jct TI | 262.7 | TI reconstructed in 20 ² |

Interstate 17 is a four-lane divided highway within the study limits. The existing mainline lane widths are twelve feet, with ten-foot outside shoulders and four-foot inside shoulders. The existing pavement structure consists of asphaltic concrete (AC). The existing normal highway cross slope varies from 1.5% to 2.0%. The southbound roadway was the original two-lane highway built in 1949 and was constructed with a parabolic crown rather than a straight left-to-right cross slope. The northbound roadway was constructed in 1965 with a constant cross slope.

DESCRIPTION

X - CORDES JUNCTION HWY (I-17) - MOORES GULCH CANYON - MI

CYN T.I-SUNSET POINT (NB)-MILL & REPLACE X-CORDES JCT. HIGHWAY (I-17), SB MP 245.2-MP

DS JCT HWY (I-17)-SNST PNT-SNST PT TI-M DS JCT HWY I-17-SNST PNT-RCKFLL CNTNMNT RUCT MEMORIAL OVERLOOK DS JCT HWY (I-17)-BDGR SPRNGS-CRDS JCT-RDES JCT HWY I-17 BADGER SPRINGS RD. BIG BUG MILL & BRIDGE FIX

diamond interchange ange with loop ramp in SW quadrant - wide median st quadrant – compact diamond interchange – wide median 13

FIGURE 2 – EXISTING TYPICAL CROSS SECTION



Two-way frontage roads exist on both sides of I-17 from Anthem Way TI to New River Road TI (west frontage road ends south of New River bridge) and north of the Rock Springs TI.

The American Association of State Highway and Transportation Officials (AASHTO) publishes guidelines for a range of geometric design criteria, including horizontal degree of curvature, superelevation rate, profile grade, and stopping sight distance in the 2005 *A Policy on Design Standards, Interstate System* and the 2011 *A Policy on Geometric Design of Highways and Streets* (Green Book). The AASHTO Controlling Design Criteria Report documents characteristics of the existing alignment and notes which criteria exceed limits set forth by the guidelines. Appendix A contains a summary of the mainline horizontal and vertical design data.

The study area was separated into three segments based on terrain:

- ◆ MP 229.1-244.5 Rolling Terrain
- MP 244.5-250.5 Mountainous Terrain
- ♦ MP 250.5-262.0 Rolling Terrain

Rolling Segment (MP 229.1 to MP 244.5)

The southern limit of the study area is the I-17/Anthem Way TI. North of the interchange, I-17 is a four-lane divided highway with a posted speed limit of 75 mph. The northbound and southbound roadways follow symmetrical horizontal alignments to New River Road TI at MP 232.0. I-17 crosses over New River at MP 231.4. The southbound I-17 roadway was originally constructed as SR 69. There are two-way frontage roads along both sides of the freeway in this area. The west frontage road ends just south of New River and the east frontage road ends north of New River Road.

North of the New River TI, the northbound and southbound roadways follow independent alignments, with the northbound roadway generally following the west side of New River. Much of this area will require roadway or rock excavation for widening. One exception is MP 235.3, where southbound I-17 is on a 50-foot tall embankment.

The Table Mesa TI is at MP 236.0. The bifurcated alignments become parallel and symmetrical just north of the Rock Springs TI at MP 242.2 and cross the Agua Fria River at MP 243.3.

Mountainous Segment (MP 244.5 to MP 250.5)

The mountainous segment begins at the Black Canyon City TI. North of this interchange, I-17 is a four-lane divided highway with a posted speed limit of 65 mph. This mountainous segment extends from Black Canyon City to the top of Black Mesa near Sunset Point. The roadway elevation increases by over 1,250 feet through the six-mile mountainous segment, from an approximate elevation of 2,130 feet at Black Canyon City to 3,390 feet at the top of Black Mesa. The northbound roadway grades range from +0.4% to +6.0% and the southbound grades range from +1.7% to -6.3%.

The northbound and southbound roadways follow independent alignments through this segment. The existing horizontal alignments consist of curves with degrees of curvature ranging from 0°30' to 4°00'. The superelevation on many curves does not meet current AASHTO standards; this condition occurs more often in the southbound direction, which was constructed as SR 69 in 1949.

The alignments follow the terrain up the Black Canyon Hill with winding curves which cut into the hillside and, in some locations, limit the available sight distance. The northbound and the southbound vertical alignments differ in elevation because of the steep terrain and do not provide opportunities for traffic to cross over between the roadways in case of an incident. At approximately MP 248, the southbound and northbound roadways are cut into an area known as Cape Horn. Rockfall issues exist in this area.

The Bumble Bee TI is located roughly halfway up the hill at MP 248.4. The TI provides access to the town of Bumble Bee and the Black Canyon valley floor. There are no services at this interchange.

North of the Bumble Bee TI, the I-17 roadways follow separate, divergent alignments to the top of the mesa. The northbound roadway continues along the face of the Black Canyon Hill until it reaches the top of the mesa. Just below the top of the mesa, a large cut segment with steep rock faces on both sides of the roadway require wire mesh draping over the slopes to prevent falling rock debris on the roadway. The southbound roadway north of the Bumble Bee TI follows a more westerly route around the face of the hill to the top of the mesa. This segment of roadway is winding and has grades steeper than 6%. At the top of the mesa (MP 250.5), the terrain changes from mountainous to rolling and the posted

speed increases from 65 mph to 75 mph.

Rolling Segment (MP 250.5 to MP 262.0)

On the mesa, the terrain becomes less severe, with existing roadway grades ranging from -4.8% to +5.0% in the northbound direction and from -6.2% to +4.5% in the southbound direction.

From the Sunset Point TI (MP 252.5) to Big Bug Creek (MP 262.0), a 176-foot median separates the parallel northbound and southbound lanes. South of the Badger Springs TI (MP 256.1), the northbound and southbound roadway alignments diverge for several miles, then converge again near the Bloody Basin TI (MP 259.4). Median widths within the study limits vary from 64 feet to more than 1800 feet.

STANLEY CONSULTANTS, INC.



The Sunset Point Rest Area at MP 252.5 opened in 1970. Improvements at the rest area in 2013 included the construction of a new restroom building and new scenic overlook area. A new 60,000-gallon water tank and pump house were constructed as part of the renovation project, which also provided relief to the existing pump within the Agua Fria National Monument, collecting water from the Agua Fria River.

1.5.2 Land Use

The land adjacent to I-17 through the project area is mostly undeveloped, except for the southern end near the Anthem Way and New River Road TIs. On the west side of I-17, just north of Anthem Way, there are commercial developments including Outlets at Anthem and Old West Cactus Farm. Also in this area along both sides of I-17 are several residential developments including Circle Mountain, Anthem Coventry Homes, and two RV parks.

The area north of New River is comprised mostly of grazing and undeveloped lands. Some residences and commercial properties are also present. However, this area is growing and an increasing number of residential and commercial properties are becoming established.

On the east side of I-17 from Black Canyon City to south of Cordes Junction is the Agua Fria National Monument, which is administered by the BLM. BLM also manages the land on the west side of I-17 and in several wide median areas between the existing northbound and southbound I-17 alignments.

Small areas of State land and private land exist near Black Canyon City and near Cordes Junction. Scattered residential development exists in both areas.

Recreation use is common on adjacent BLM and ASLD land.

A number of grazing allotments and mining claims are located in the study area. A multi-use transportation and utility corridor has been designated in BLM's Agua Fria National Monument/ Bradshaw-Harguahala Resource Management Plan. The multi-use corridor begins north of New River and continues north to SR 69 and ranges from one to three miles wide. A natural gas pipeline operated by Transwestern Pipeline Company was recently constructed in a 200-foot easement west of the I-17 mainline. The pipeline is located within BLM's multi-use corridor.

1.5.3 Utilities

The major existing utilities in the I-17 corridor are presented in Table 3.



BLM

State Land

Agua Fria

National

Monument

JUNCTION LAND USE

| TA | BL | .E | 3 - | - E | XI | ST |
|----|----|----|-----|-----|----|----|
| | | | | | | |

| UTILITY TYPE | |
|--------------------------------|--|
| AT&T Fiber Optic | |
| Fiber Optic (1 ¼ " inner duct) | The line lies west of I-17, turnin Lake Pleasant Road to New Riv |
| Fiber Optic (1 ¼ " inner duct) | Crosses I-17 SB at Sta 2011+50 |
| Fiber Optic (1 ¼" inner duct) | Crosses I-17 NB at Sta 2052+5 |
| Fiber Optic (1 ¼ " inner duct) | Along east ROW line from I-17 I |
| Fiber Optic (1 ¼ " inner duct) | Crosses I-17 NB at Sta 2110+50 |
| Fiber Optic (1 ¼ " inner duct) | Crosses I-17 SB at Sta 2117+50 |
| Fiber Optic (1 ¼ " inner duct) | Along west ROW line from Sta |
| Fiber Optic (1 ¼ " inner duct) | West of Black Canyon City TI (N paralleling I-17 |
| Fiber Optic (1 ¼ " inner duct) | Follows old Route 69 alignmen (MP 248.4) to the Badger Spring |
| Fiber Optic (1 ¼ " inner duct) | Follows old Route 69 alignment |
| Arizona Public Service | |
| Overhead Power | Crosses I-17 at NB Sta 1503+5 |
| Overhead Power | Crosses I-17 at Sta 1538+00 (M |
| Overhead Power | Crosses I-17 at Sta 1611+50 (M |
| Overhead Power | Crosses I-17 at Sta 1671+00 (M |
| Overhead Power | Crosses I-17 at NB Sta 1863+5 |
| Overhead Power | Crosses I-17 at NB Sta 1883+0 |
| Overhead Power | Crosses I-17 at SB Sta 1991+5 |
| Overhead Power | Crosses I-17 at NB Sta 2202+0 |
| Overhead Power | Crosses I-17 at NB Sta 2225+0 |
| Overhead Power | Crosses I-17 at NB Sta 2248+8 |
| Overhead Power | Crosses I-17 at NB Sta 2284+2 |
| Overhead Power | West of Black Canyon City TI (N paralleling I-17 |
| Overhead Power | Crosses I-17 at 2431+40 (MP 2 |
| Overhead Power | Continues north east to Radio T |
| Western Area Power Ad | Iministration |
| 345 kV Transmission Line | Crosses I-17 at Table Mesa TI |
| 345 kV Transmission Line | Within ROW from Sta 1881+00 SB I-17 at Sta 1886+50 (MP 23 |
| 345 kV Transmission Line | Within SB I-17 ROW from Sta 1 |
| 345 kV Transmission Line | Crosses SB I-17 at Sta 1995+0 243.43) and NB I-17 at Sta 210 (MP 245.97) |
| 345 kV Transmission Line | West of Black Canyon City TI (N |
| | |

FING UTILITIES

LOCATION

g west along Anthem Way and then running north, paralleling ver, then paralleling the gas pipeline north.

0 (MP 238.96)

0 (MP 239.69)

NB Sta 2057+00 to NB Sta 2110+50 (MP 239.74 to 240.69)

60 (MP 240.69)

0 (MP 240.85)

2117+50 to Sta 2185+00 (MP 240.85 to MP 242.18)

MP 244.5) follows old Route 69 alignment (Maggie Mine Road)

t (Crown King Road) paralleling I-17 from the Bumble Bee TI as TI (MP 256.1)

(Crown King Road) in the northwest direction to Cordes

0 (MP 229.29) and SB Sta 1502+20 (MP 229.24)

IP 229.96)

IP 231.35)

IP 232.35)

0 and SB Sta 1860+80 (MP 236.09 and MP 236.04)

0 and SB Sta 1883+50 (MP 236.46 and MP 236.47)

5 and NB Sta 2007+47 (MP 238.50 and MP 238.80)

0 and SB Sta 2201+70 (MP 242.77 and MP 242.76)

0 and SB Sta 2223+80 (MP 243.22 and MP 243.19)

0 and SB Sta 2248+50 (MP 243.68 and MP 243.67)

0 and SB Sta 2283+70 (MP 244.37 and MP 244.36)

MP 244.5) follows old Route 69 alignment (Maggie Mine Road)

47.4)

ower east of the Bumble Bee TI (MP 248.4)

(MP 236.42) (SB) to Sta 1931+50 (MP 237.36) (NB); Crosses 6.52) and NB I-17 at Sta 2040+00 (MP 239.43)

965+00 to Sta 1976+20 (MP 238.00 to MP 238.21)

00 (MP 238.58), Sta 2198+00 (MP 251.34), Sta 2236+00 (MP 03+50 (MP 239.00), Sta 2195+00 (MP 251.28), Sta 2367+00

/IP 244.5) paralleling I-17

2356+80 (MP 245.88)

| UTILITY TYPE | LOCATION |
|-----------------------------|---|
| 345 kV Transmission Line | Crosses northbound (NB) I-17 2367+62 (MP 246.11) |
| 345 kV Transmission Line | Paralleling East of I-17 within the Agua Fria National Monument |
| 345 kV Transmission Line | Crosses NB I-17 2950+02 (MP 257.20) |
| 345 kV Transmission Line | Crosses SB I-17 2998+04 (MP 258.11) |
| There are numerous transmis | ssion towers supporting overhead (OH) lines throughout the project limits. |
| El Paso Natural Gas | |
| 20" Gas Pipeline | Crosses SB I-17 at Sta 2012+50 (MP 238.91) |
| 20" Gas Pipeline | Crosses NB I-17 at Sta 2054+00 (MP 239.69) |
| 20" Gas Pipeline | Crosses I-17 at Sta 2208+80 (MP 242.87) (south of Agua Fria River) |
| 20" Gas Pipeline | West of Black Canyon City TI (MP 244.5) paralleling I-17 |
| 20" Gas Pipeline | Crosses I-17 at 2431+40 (MP 247.4) |
| 20" Gas Pipeline | Crosses I-17 NB at 2920+90 (MP 256.65) |
| 20" Gas Pipeline | Crosses I-17 SB at 2929+24 (MP 256.81) |
| Southwest Gas | |
| 1 1/4" Gas | Crosses I-17 NB at Sta 1657+00 (MP 232.20) and SB I-17 at 1656+00 (MP 232.18) |
| Eagle West Cable | |
| Cable | Aerial crossing over I-17 at Mud Springs |
| Transwestern Pipeline | Company |
| 42" Gas Pipeline | West of Black Canyon City TI (MP 244.5) paralleling I-17 |
| Black Canyon City Wat | er Improvement District |
| 4" Water line (Abandoned) | Crosses I-17 at Sta 2205+00 (MP 242.83) |
| 2" Water line | Crosses I-17 at Sta 2216+50 (MP 243.02) |
| 4" Water line | Crosses I-17 at Sta 2232+00 (MP 243.35) |
| 6" Water line | Crosses I-17 at Sta 2233+00 (MP 243.37) |

There are no railroad crossings in the study area.

1.5.4 Drainage

Existing Drainage Conditions and Facilities

In addition to the bridge crossings at washes, the drainage facilities along the I-17 corridor range from smalldiameter corrugated metal pipe culverts to multi-cell reinforced concrete box culverts (RCBC). There are approximately 39 reinforced concrete box culverts and 257 corrugated metal or reinforced concrete pipe culverts from Anthem Way TI to Cordes Junction. Other existing drainage features include catch basins connected to small-diameter pipes to drain median areas.

The watershed contributing to the project area between Anthem and Black Canyon City generally originates in the hills and mountains to the northeast. The drainage typically flows in a southwest direction and first crosses the northbound lanes of I-17 and then the southbound lanes. Some drainage basins originate to the west of I-17 beginning 0.5 mile north of the New River TI. These basins flow in a southeasterly direction, crossing I-17 and

then reversing direction and crossing the roadway again, flowing southwest. Slopes range from 1% in the lower alluvial areas to approximately 25%.

Rock outcrops interspersed with shallow deposits of sandy loams overlying bedrock characterize the upper, steeper portion of the watershed. The lower watershed soils are made up of alluvial materials washed down from the surrounding hills. Gravelly/sandy loam soils make up much of this area.

Vegetation is sparse (approximately 10-20%) and representative of the Sonoran desert region. Species noted within the project limits include palo verde, mesquite, saguaro cacti, cholla, and prickly pear cacti. Desert shrubs such as greasewood and desert grasses constitute an additional percentage of the vegetative cover.

North of Black Canyon City, the existing I-17 roadway alignments are situated between major drainage tributaries. In general, the northbound lanes parallel the Agua Fria River and Badger Springs Wash to the east and the southbound lanes parallel Black Canyon Creek and Bumble Bee Creek to the west. Relative to these tributaries, the existing I-17 alignments are located away from major watercourses, with many smaller washes crossing the existing roadway alignments.

There are five major drainage crossings of the existing I-17 alignments within the study area. New River crosses under I-17 south of the New River Road TI, Little Squaw Creek and Moores Gulch cross I-17 near MP 239, the Agua Fria River crosses under I-17 at Black Canyon City, and Big Bug Creek crosses under I-17 at the north end of the project, just south of the Cordes Junction TI.

The existing onsite drainage is characterized by sheet flow off the roadway, with the runoff being intercepted by open ditches or channels and conveyed to offsite cross-drain outfalls. Roadway curb has been constructed to intercept the pavement drainage at some locations. This curb conveys the runoff to either down drain pipes or spillways, where the flows are conveyed down the roadway embankment.

A listing of large box and pipe culverts is shown in Table 4. Large culverts are defined as having a diameter of 54 inches or larger.

TABLE 4 – EXISTING LARGE BOX CULVERTS AND PIPES GREATER THAN 54 INCHES

| MILEPOST | ROADWAY | SIZE LENGTH (FT) | | TYPE |
|----------|---------|------------------|-----|------|
| 229.4 | NB & SB | 2-6'X5' | 428 | RCBC |
| 230.5 | NB &SB | 6'X4' | 277 | RCBC |
| 230.8 | NB & SB | 6'X4' | 251 | RCBC |
| 231.2 | NB & SB | 2-10'x7' | 201 | RCBC |
| 232.2 | NB & SB | 60" | 348 | CMP |
| 232.5 | NB | 2-10'X8' | 201 | RCBC |
| 232.5 | SB | 2-10'X8' | 199 | RCBC |
| 233.0 | NB | 10'X8' | 134 | RCBC |
| 233.2 | SB | 10'X8' | 198 | RCBC |
| 233.8 | NB | 2-10'X8' | 95 | RCBC |
| 233.9 | SB | 2-10'X8' | 125 | RCBC |
| 234.4 | NB | 2-8'X7' | 107 | RCBC |
| 234.5 | SB | 10'X10' | 167 | RCBC |
| 235.6 | SB | 6'X7' | 134 | RCBC |
| 235.6 | NB | 6'X7' | 87 | RCBC |

| MILEPOST | ROADWAY | SIZE | LENGTH (FT) | ТҮРЕ |
|----------|---------|-----------|-------------|------|
| 236.4 | SB | 6'X4' | 169 | RCBC |
| 236.8 | SB | 60" | 112 | CMP |
| 236.8 | SB | 78" | 104 | CMP |
| 236.8 | NB | 72" | 223 | CMP |
| 237.1 | SB | 60" | 136 | CMP |
| 237.1 | NB | 60" | 212 | CMP |
| 237.4 | NB | 10'X3' | 55 | RCBC |
| 238.1 | NB | 72" | 216 | SPP |
| 238.2 | SB | 84" | 140 | CMP |
| 238.6 | NB | 3-10'X10' | 142 | RCBC |
| 238.8 | NB | 10'X4' | 49 | RCBC |
| 239.1 | SB | 84" | 134 | CMP |
| 239.6 | NB | 78" | 180 | CMP |
| 239.6 | SB | 8'X7' | 104 | RCBC |
| 239.7 | NB | 10'X10' | 151 | RCBC |
| 239.8 | NB | 60" | 307 | CMP |
| 240.4 | NB | 54" | 200 | CMP |
| 240.5 | SB | 60" | 90 | CMP |
| 240.7 | NB | 10'X10' | 114 | RCBC |
| 240.8 | SB | 8'X7' | 92 | RCBC |
| 241.8 | SB | 2-10X8' | 143 | RCBC |
| 241.8 | NB | 6'X6' | 110 | RCBC |
| 242.0 | NB | 2-10'X8' | 169 | RCBC |
| 242.1 | NB & SB | 60" | 511 | CMP |
| 244.8 | NB & SB | 6'x7' | 266 | RCBC |
| 245.6 | NB | 54" | 190 | CMP |
| 246.7 | SB | 54" | 113 | CMP |
| 246.8 | SB | 2-8'X7' | 230 | RCBC |
| 247.6 | SB | 54" | 112 | CMP |
| 248.3 | SB | 78" | 594 | CMP |
| 249.0 | SB | 6'x7' | 563 | RCBC |
| 249.6 | SB | 2-10'X8' | 253 | RCBC |
| 249.7 | SB | 6x7 | 105 | RCBC |
| 250.8 | SB | 60" | 180 | CMP |
| 248.8 | SB | 6'x7' | 103 | RCBC |
| 251.0 | NB | 6'x7' | 86 | RCBC |
| 251.0 | SB | 6'x7' | 160 | RCBC |
| 252.9 | NB | 6'x7' | 96 | RCBC |
| 253.0 | SB | 6'x7' | 88 | RCBC |
| 255.0 | SB | 8'X7' | 87 | RCBC |
| 255.0 | NB | 8'X7' | 86 | RCBC |
| 255.7 | NB | 72" | 372 | CMP |
| 256.0 | NB | 60" | 228 | CMP |

| MILEPOST | ROADWAY | SIZE | LENGTH (FT) | ТҮРЕ |
|----------|---------|--------|-------------|------|
| 256.2 | NB | 8'X7' | 174 | RCBC |
| 256.6 | SB | 60" | 169 | CMP |
| 256.9 | SB | 84" | 101 | CMP |
| 257.0 | NB | 60" | 120 | CMP |
| 259.1 | NB | 10'x8' | 74 | RCBC |
| 259.2 | SB | 10'X8' | 100 | RCBC |
| 260.0 | SB | 8'X7' | 141 | RCBC |
| 260.5 | NB | 6'x7' | 71 | RCBC |
| 260.8 | NB | 60" | 348 | CMP |
| 260.9 | NB | 72" | 290 | CMP |
| 261.8 | NB | 72" | 259 | CMP |

1.5.5 Right-of-Way

Existing right-of-way widths vary widely along the corridor as detailed in Table 5. In areas where the northbound and southbound roadways are parallel, right-of-way widths are typically 200 feet east of the northbound centerline and 200 feet west of the southbound centerline. In sections where the northbound and southbound alignments are bifurcated and in interchange areas, right-of-way widths increase to as much as 2100 feet.

Several of the wide median areas are under the jurisdiction of BLM.

TABLE 5 – EXISTING RIGHT-OF-WAY WIDTHS

| | FROM | | то | ROW WIDTH | |
|--------|--------------|------------|--------------|--|----------------------------|
| MP | STATION | MP STATION | | (FEET) | COMMEN I S |
| 228.76 | 1475+00 | 230.77 | 1581+00 | 249 | Includes Anthem Way TI |
| 230.77 | 1581+00 | 231.85 | 1638+00 | 300 | Includes New River Road TI |
| 231.85 | 1638+00 | 233.12 | 1705+00 | Varies Typ. 96' West of SB centerline (cl) and 96' East of NB cl | |
| 233.12 | 1705+00 | 233.41 | 1720+00 | Varies Typ. 96' West of SB cl and 100' East of NB cl | |
| 233.41 | 1720+00 | 234.64 | 1788+00 (NB) | Varies Typ. 96' West of SB cl and 200' East of NB cl | |
| 234.64 | 1788+00 (NB) | 234.91 | 1802+00 (NB) | Varies Typ. 96' West of SB cl and 100' East of NB cl | |
| 234.91 | 1802+00 (NB) | 235.41 | 1828+69 (NB) | Varies Typ. 96' West of SB cl and 200' East of NB cl | |
| 235.41 | 1828+69 (NB) | 235.67 | 1842+00 (NB) | 496 | |
| 235.67 | 1842+00 (NB) | 237.00 | 1912+00 (SB) | Varies Typ. 100' West of SB cl and 96' East of NB cl | Includes Table Mesa TI |
| 237.00 | 1912+00 (SB) | 237.37 | 1932+00 (NB) | Varies Typ. 184' West of SB cl and 96' East of NB cl | |

| MP STATION MP STATION (FEET) COMMENTS 237.37 1932+00 (NB) 238.36 1984+40 (NB) 225 237.37 1936+27 (SB) 238.66 1999+47 (SB) 230.66 1999+47 (SB) 230.77 238.66 1994+47 (SB) 238.77 2005+47 (SB) 700 Moores Guich 238.66 1994-47 (SB) 238.77 20054-00 (NB) 239.68 2051+00 (SB) 300 Little Squaw Creek 239.57 2028+00 (NB) 239.63 2051+00 (SB) 350 2051 239.72 2032+00 (NB) 239.63 2056+00 (SB) 300 239.85 2051+45 (NB) 239.84 2062+50 (NB) 200 200 239.85 2051+45 (NB) 240.42 2090+417 (SB) 400 240.65 2110+00 (NB) 241.53 2151+42 (NB) 4706 241.50 2151+42 (NB) 24154+47 (NB) 24154+47 (NB) | | FROM | | то | ROW WIDTH | COMMENTO |
|--|--------|--------------|--------|--------------|--|---|
| 237.37 1932+00 (NB) 238.36 1984+40 (NB) 225 237.37 1936+27 (SB) 238.66 1999+47 (SB) 200 238.66 1999+47 (SB) 239.19 2028+00 (NB) 200 238.66 1999+47 (SB) 239.17 2005+47 (SB) 230.52 2032+00 (NB) 300 Little Squaw Creek 239.77 2032-00 (NB) 239.32 2032-00 (NB) 230.63 2051+45 (NB) 200 239.82 2032-00 (NB) 239.33 2056+00 (SB) 300 239.82 2053+00 (SB) 230.0 2002+00 (NB) 2250 239.84 2062+50 (NB) 240.37 2096+43 (NB) 200 240.49 2090+48 (NB) 240.65 2110+00 (NB) Varies Typ. 200 West of SB cl and 100 East of NB cl 241.53 2151+42 (NB) 24154+87 (NB) Varies Typ. 100 West of SB cl and 100 East of NB cl 241.53 2154+87 (NB) 241.53 2164+87 (NB) 300 <td< th=""><th>MP</th><th>STATION</th><th>МР</th><th>STATION</th><th>(FEET)</th><th>COMMEN I S</th></td<> | MP | STATION | МР | STATION | (FEET) | COMMEN I S |
| 237.37 1936+27 (SB) 238.66 1999+47 (SB) 200 238.66 1999+47 (SB) 238.77 2005+47 (SB) 700 Moores Gulch 238.77 2005+47 (SB) 238.77 2005+47 (SB) 700 Moores Gulch 238.77 2005+47 (SB) 239.68 2053+00 (SB) 400 239.75 2032+00 (NB) 239.73 2056+00 (SB) 350 239.78 2056+00 (SB) 239.73 2056+00 (SB) 350 239.84 2062+50 (NB) 239.84 2062+50 (NB) 200 239.84 2062+50 (NB) 240.49 2096+41 (NB) 240.49 240.49 240.49 240.49 2406+41 (NB) 241.59 2154+87 (NB) 241.59 2154+87 (NB) 241.59 2154+87 (NB) 241.59 2169+65 (NB) 240.49 2334+00 (NB) 240.49 2314+00 (NB) 240.49 232 | 237.37 | 1932+00 (NB) | 238.36 | 1984+40 (NB) | 225 | |
| 238.36 1984+40 (NB) 239.19 2028+00 (NB) 200 238.66 1999+47 (SB) 238.77 2005+47 (SB) 239.68 2053+00 (SB) 400 239.55 2028+00 (NB) 239.68 2053+00 (SB) 300 Little Squaw Creek 239.57 2002+00 (NB) 239.33 2051+45 (NB) 200 2032+00 (NB) 239.72 2032+00 (NB) 239.33 2062+50 (SB) 300 2051+45 (NB) 239.85 2051+45 (NB) 239.84 2062+50 (SB) 300 2051+45 (NB) 239.86 2062+50 (NB) 240.49 2090+41 (NB) 240.49 2090+41 (NB) 240.49 240.65 2110+00 (NB) 241.53 2151+42 (NB) Varies Typ. 200 West of SB cl and 1007 East of NB cl 200 241.53 2151+42 (NB) 241.59 2154+87 (NB) Varies Typ. 100 West of SB cl and 1007 East of NB cl 200 241.53 2151+42 (NB) 241.59 2164+81 (NB) Varies Typ. 100 West of SB cl and 1007 East of NB cl 200 241.53 22154+50 243.33 2231+00 (NB) | 237.37 | 1936+27 (SB) | 238.66 | 1999+47 (SB) | 400 | |
| 238.66 1999+47 (SB) 238.77 2005+47 (SB) 239.87 2005+47 (SB) 239.85 2005+47 (SB) 239.87 2005+47 (SB) 239.87 2005+47 (SB) 239.87 2005+40 (NB) 239.77 2005+40 (NB) 239.77 2005+00 (NB) 239.73 2056+00 (SB) 239.73 2056+00 (SB) 350 239.86 2053+00 (NB) 239.86 2051+45 (NB) 239.86 2062+50 (NB) 220.00 200 239.85 2062+50 (NB) 239.84 20062+50 (NB) 200 200 239.84 2062+50 (NB) 240.49 2096+17 (SB) 400 200 200 240.49 2090+48 (NB) 240.55 2110+00 (NB) Varies Typ. 200 West of SB cl and 100 'East of NB cl 200 241.53 2151+42 (NB) 241.57 2169+65 (NB) Varies Typ. 100 West of SB cl and 100 'East of NB cl 200 241.53 2154+47 (NB) 241.87 2169+65 (NB) Varies Typ. 100 West of SB cl and 100 'East of NB cl 200 241.53 2154+47 (NB) 241.87 2169+65 (NB) Varies Typ. 100 West of SB cl and 100 'Ea | 238.36 | 1984+40 (NB) | 239.19 | 2028+00 (NB) | 3) 200 | |
| 238.77 2005+47 (SB) 239.68 2053+00 (NB) 239.27 2032+00 (NB) 239.63 2051+45 (NB) 200 239.62 2053+00 (NB) 239.63 2056+00 (SB) 239.73 2056+00 (SB) 239.73 2056+00 (SB) 239.73 2056+00 (SB) 239.84 2062+50 (NB) 240.37 2056+00 (SB) 239.84 2062+50 (NB) 240.37 2056+145 (NB) 240.37 2056+145 (NB) 240.37 2056+145 (NB) 240.49 2090+48 (NB) 240.49 2090+48 (NB) 240.49 2090+48 (NB) 240.49 2090+48 (NB) 241.53 2151+42 (NB) Varies Typ. 200 West of SB cl and 100'East of NB cl 100.0000000000000000000000000000000000 | 238.66 | 1999+47 (SB) | 238.77 | 2005+47 (SB) | 700 | Moores Gulch |
| 233.55 2028+00 (NB) 239.27 2032+00 (NB) 239.68 2003+00 (NB) 239.73 2056+00 (SB) 239.73 2056+00 (SB) 239.84 2062+50 (SB) 3300 239.85 2051+45 (NB) 239.84 2062+50 (SB) 230.84 2062+50 (SB) 240.47 239.86 2062+50 (SB) 240.49 2090+48 (NB) 200 239.86 2062+50 (SB) 240.49 2090+48 (NB) 240.65 2110+00 (NB) Varies Varies 240.66 210+00 (NB) 241.53 2151+42 (NB) Varies Typ. 100 West of SB cl and 125 East of NB cl 241.53 2151+42 (NB) 241.57 2169+65 (NB) Varies Typ. 100 West of SB cl and 125 East of NB cl 241.54 2154+87 (NB) 241.87 2169+65 (NB) Varies Typ. 100 West of SB cl and 100 East of NB cl 241.53 2215+42 (NB) 241.87 2169+65 (NB) Varies Typ. 100 West of SB cl and 100 East of NB cl 243.33 2231+00 (NB) 243.33 2231+00 (NB) Varies Typ. 100 West of SB cl and 100 East of NB cl | 238.77 | 2005+47 (SB) | 239.68 | 2053+00 (SB) | 400 | |
| 233.27 2032+00 (NB) 239.63 2051+45 (NB) 200 239.68 2053+00 (SB) 239.73 2056+00 (SB) 3300 239.73 2056+00 (SB) 239.84 2062+50 (NB) 240.47 239.84 2062+50 (SB) 240.37 2090+48 (NB) 200 239.86 2062+50 (SB) 240.49 2090+48 (NB) 240.65 2110+00 (NB) 4400 240.49 2090+48 (NB) 241.53 2151+42 (NB) Varies Typ. 200 West of SB d and 100' East of NB d | 239.55 | 2028+00 (NB) | 239.27 | 2032+00 (NB) | 300 | Little Squaw Creek |
| 239.68 2053-00 (SB) 239.73 2056-00 (SB) 330 239.73 2056400 (SB) 239.84 2062+50 (SB) 300 239.85 2051+45 (NB) 239.84 2062+50 (NB) 240.37 2090+48 (NB) 200 239.84 2062+50 (SB) 240.49 2090+48 (NB) 240.65 2110+00 (NB) Varies Typ. 200'West of SB cl and 100'East of NB cl 240.65 2110+00 (NB) 241.53 2151+42 (NB) Varies Typ. 100'West of SB cl and 100'East of NB cl 241.59 2154+87 (NB) 241.87 2169+65 (NB) Varies Typ. 100'West of SB cl and 100'East of NB cl 241.51 2169+65 (NB) 241.87 2169+65 (NB) Varies Typ. 100'West of SB cl and 100'East of NB cl 241.52 2169+65 (NB) 241.87 2169+65 (NB) 300 Includes Rock Springs TI 242.20 2186+81 (NB) 243.33 2231+00 (NB) 246.52 3286+08 500-1100+ Includes Back Canyon City TI 244.94 2313+95 (NB) 245.23 3286+08 2468+67 575-780 245.02 2469+75 248.72 246 | 239.27 | 2032+00 (NB) | 239.63 | 2051+45 (NB) | 200 | |
| 233.73 2056+00 (SB) 239.86 2062+50 (SB) 300 239.84 2061+45 (NB) 239.84 2062+50 (NB) 240.37 2090+48 (NB) 200 239.84 2062+50 (SB) 240.37 2090+48 (NB) 200 400 240.49 2090+48 (NB) 240.55 2110+00 (NB) Varies 400 240.55 2110+00 (NB) 241.53 2151+42 (NB) Varies Typ. 200 West of SB cl and 125 East of NB cl and 100 East of NB cl ano 100 East of NB cl ano 10 | 239.68 | 2053+00 (SB) | 239.73 | 2056+00 (SB) | 350 | |
| 239.85 2051+45 (NB) 239.84 2062+50 (NB) 240.37 2090+48 (NB) 200 239.84 2062+50 (NB) 240.37 2090+48 (NB) 2006 1 240.49 2090+48 (NB) 240.65 2110+00 (NB) 241.53 2151+42 (NB) Varies Typ. 200 West of SB cl and 100 East of NB cl 241.53 2151+42 (NB) 241.57 2169+65 (NB) Varies Typ. 100 West of SB cl and 100 East of NB cl 241.59 2154+87 (NB) 241.87 2169+65 (NB) Varies Typ. 100 West of SB cl and 100 East of NB cl 241.81 2169+65 (NB) 242.02 2186+81 (NB) Varies Includes Rock Springs TI 241.82 2169+65 (NB) 243.3 2231+00 (NB 300 243.33 2231+00 (NB 242.02 2186+81 (NB) Varies Includes Back Canyon City TI 244.84 2313+95 (NB 242.33 2231+00 (NB 246.46 2386+08 500-1100+ Includes Back Canyon City TI 244.94 2313+95 (NB 246.46 23 | 239.73 | 2056+00 (SB) | 239.86 | 2062+50 (SB) | 300 | |
| 239.84 2062+50 (NB) 240.37 2090+48 (NB) 200 239.86 2062+50 (SB) 240.49 2096+17 (SB) 400 240.49 2090+48 (NB) 240.65 2110+00 (NB) 241.53 2151+42 (NB) Varies Typ. 200 West of SB cl and 100 East of NB cl 241.53 2151+42 (NB) 241.59 2154+87 (NB) Varies Typ. 100 West of SB cl and 125 East of NB cl 241.59 2154+87 (NB) 241.87 2169+65 (NB) Varies Typ. 100 West of SB cl and 100 East of NB cl 241.59 2154+87 (NB) 241.87 2169+65 (NB) Varies Typ. 100 West of SB cl and 100 East of NB cl 241.50 2169+65 (NB) 242.02 2186+81 (NB) Varies Includes Rock Springs TI 242.20 2186+81 (NB) 243.33 2231+00 (NB) 300 244.33 2231+00 (NB) 244.34 2313+95 (NB) Varies Includes Rock Springs TI 244.33 2238+00 246.84 2386+08 500-1100+ Includes Bumble Bee TI 244.52 2328+50 246.87 575-780 | 239.85 | 2051+45 (NB) | 239.84 | 2062+50 (NB) | 250 | |
| 239.86 2062+50 (SB) 240.9 2096+17 (SB) 400 240.49 2090+48 (NB) 240.65 2110+00 (NB) Varies 240.65 2110+00 (NB) 241.53 2151+42 (NB) Varies Typ. 200 West of SB cl and 100 East of NB cl 241.53 2151+42 (NB) 241.59 2154+87 (NB) Varies Typ. 100 West of SB cl and 125 East of NB cl 241.59 2154+87 (NB) 241.87 2169+65 (NB) Varies Typ. 100 West of SB cl and 100 East of NB cl 241.87 2169+65 (NB) 242.02 2186+81 (NB) Varies Includes Rock Springs TI 242.20 2186+81 (NB) 243.33 2231+00 (NB) 243.33 2231+00 (NB) 243.33 243.33 2231+00 (NB) 244.94 2313+95 (NB) 406 246.23 245.23 2328+50 246.46 2386+08 500-1100+ Includes Back Canyon City TI 244.94 2313+95 (NB) 246.87 575-780 Includes Sunset Point rest area and TI 245.23 2386+00 246.94 2400+00 600 Includes Sunset Point rest area and TI | 239.84 | 2062+50 (NB) | 240.37 | 2090+48 (NB) | 200 | |
| 240.49 2090+48 (NB) 240.65 2110+00 (NB) 241.53 2151+42 (NB) Varies Typ. 200 West of SB cl and 100 East of NB cl 241.53 2151+42 (NB) 241.59 2151+42 (NB) 241.59 2151+42 (NB) Varies Typ. 100 West of SB cl and 125 East of NB cl 241.53 2151+42 (NB) 241.87 2169+65 (NB) Varies Typ. 100 West of SB cl and 125 East of NB cl 241.54 2169+65 (NB) 241.87 2169+65 (NB) Varies Typ. 100 West of SB cl and 100 East of NB cl 241.87 2169+65 (NB) 242.20 2186+81 (NB) Varies Includes Rock Springs TI 242.20 2186+81 (NB) 243.33 2231+00 (NB) 244.94 2313+95 (NB) Varies Includes Rock Springs TI 244.20 2186+81 (NB) 245.23 2328+50 (NB) 406 245.23 2328+50 (NB) 246.46 2386+08 2468+67 575.780 248.05 2469.75 248.72 2490+00 610-1100 Includes Bunble Bee TI 248.05 2655+00 253.91 2742+00 430-430.0 | 239.86 | 2062+50 (SB) | 240.49 | 2096+17 (SB) | 400 | |
| 240.65 2110+00 (NB) 241.53 2151+42 (NB) Varies Typ. 200 West of SB cl and 100 East of NB cl and 125 East of NB cl and 125 East of NB cl 241.53 2151+42 (NB) 241.59 2154+87 (NB) Varies Typ. 100 West of SB cl and 125 East of NB cl 241.59 2154+87 (NB) 241.87 2169+65 (NB) Varies Typ. 100 West of SB cl and 100 East of NB cl 241.7 2169+65 (NB) 242.20 2186+81 (NB) Varies Typ. 100 West of SB cl and 100 East of NB cl 242.20 2186+81 (NB) 243.33 2231+00 (NB) 300 243.33 2231+00 (NB) 244.40 2313+95 (NB) Varies 244.44 2313+95 (NB) 245.23 2328+50 (NB) 406 245.23 2328+50 246.46 2386+08 500-1100+ Includes Back Canyon City TI 244.45 2386+08 246.87 575-780 248.72 2505+00 25.311 2742+00 490-1300 Includes Sunset Point rest area and TI 253.11 2742+00 2400+00 600 254.46 2809+00 256.44 </td <td>240.49</td> <td>2090+48 (NB)</td> <td>240.65</td> <td>2110+00 (NB)</td> <td>Varies</td> <td></td> | 240.49 | 2090+48 (NB) | 240.65 | 2110+00 (NB) | Varies | |
| 241.53 2151+42 (NB) 241.59 2154+87 (NB) Varies Typ. 100' West of SB cl and 125' East of NB cl 241.59 2154+87 (NB) 241.87 2169+65 (NB) 241.87 2169+65 (NB) Varies Typ. 100' West of SB cl and 100' East of NB cl 241.87 2169+65 (NB) 242.20 2186+81 (NB) 243.33 2231+00 (NB) 243.33 2231+00 (NB) 243.33 2231+00 (NB) 244.94 2313+95 (NB) Varies Includes Black Canyon City TI 244.94 2313+95 (NB) 245.23 2328+50 (NB) 406 Includes Mach Canyon City TI 245.23 2238+50 246.46 2386+08 500-1100+ Includes Bumble Bee TI 246.46 2386+08 2468+67 575-780 Includes Sumble Bee TI 248.72 2505+00 250.99 2625+00 400 NB, 400 SB BLM land 250.99 2625+00 253.11 2742+00 490-1300 Includes Sumset Point rest area and TI 253.11 2742+00 254.46 2809+00 430-490 Includes Badger Springs TI and median area as ADOT ROW 256.44 2910+00 <td>240.65</td> <td>2110+00 (NB)</td> <td>241.53</td> <td>2151+42 (NB)</td> <td>Varies Typ. 200' West of SB cl and 100' East of NB cl</td> <td></td> | 240.65 | 2110+00 (NB) | 241.53 | 2151+42 (NB) | Varies Typ. 200' West of SB cl and 100' East of NB cl | |
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| 258.62 3025+00 259.26 3060+00 700-1100 259.26 3060+00 259.76 3087+00 430-870 Includes Bloody Basin TI 259.76 3090+00 260.82 3145+00 400-830 100-460 260.82 3170+00 262.2 3220+00 400-460 100-460 | 257.01 | 2940+00 | 258.62 | 3025+00 | 760-2200 Includes median area | |
| 259.26 3060+00 259.76 3087+00 430-870 Includes Bloody Basin TI 259.76 3090+00 260.82 3145+00 400-830 100-830 260.82 3145+00 261.29 3180+00 400 100-460 261.29 3170+00 262.2 3220+00 400-460 100-460 | 258.62 | 3025+00 | 259.26 | 3060+00 | 700-1100 | |
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| 261.29 3170+00 262.2 3220+00 400-460 | 260.82 | 3145+00 | 261 29 | 3180+00 | 400 | |
| | 261 20 | 3170±00 | 262.2 | 3220±00 | 400-460 | |

1.5.6 Structures

General

There are six precast prestressed concrete girder bridges, eight steel girder bridges, and fourteen continuous reinforced concrete slab bridges within the project limits. Newer structures include the Anthem Way TI Underpass, constructed in 2000, and the Little Squaw Creek bridge SB, constructed in 2011. The Big Bug Creek NB and SB bridges were replaced in 2013 with the Cordes Junction TI reconstruction project. The oldest structure, I-17 SB over Moores Gulch, was constructed in 1950. The remaining structures were constructed between 1960 and 1970. In most cases, the bridges are supported on spread footings or H piles, except for the newer bridges at Big Bug Creek and Little Squaw Creek SB. In general, the bridges are founded on granitic and volcanic rocks, with siltstone and claystone at the Badger Springs NB TI overpass (OP). None of the waterway crossings are listed as scour critical. The existing (2018) National Bridge Inventory bridges are listed in Table 6.

TABLE 6 – EXISTING STRUCTURES

| STRUCTURE NAME | STRUCT. NO. | МР | YEAR BUILT | MIN. VERTICAL CLEARANCE (Ft) | INVENTO RY RATING | SUFFICIENCY RATING |
|------------------------------|----------------|--------|---------------|---------------------------------------|-------------------------|-----------------------|
| Anthem Way TI UP | 2537 | 229.0 | 2000 | 17.4 | HS-26 | 99 |
| New River Bridge NB | 1290 | 231.4 | 1968 | N/A | HS-20 | 96 |
| New River Bridge SB | 1291 | 231.4 | 1968 | N/A | HS-20 | 96 |
| New River TI OP NB | 1292 | 232.0 | 1968 | 19.9 | HS-24 | 94 |
| New River TI OP SB | 1293 | 232.0 | 1968 | 15.9 | HS-24 | 95 |
| Table Mesa TI UP SB | 1294 | 235.9 | 1968 | 16.1 | HS-22 | F 96 |
| Table Mesa TI UP NB | 1295 | 235.9 | 1968 | 16.6 | HS-21 | F 96 |
| Moores Gulch Bridge NB | 0967 | 238.2 | 1967 | N/A | HS-25 | 95 |
| Moores Gulch Bridge SB | 0339 | 238.6 | 1950 | N/A | HS-16 | F 65 |
| Little Squaw Creek Bridge NB | 0968 | 239.2 | 1967 | N/A | HS-24 | 89 |
| Little Squaw Creek Bridge SB | 2965 | 239.6 | 2011 | N/A | HS-34 | 91 |
| Rock Springs TI UP NB | 0969 | 242.2 | 1967 | 15.9 | HS-27 | 97 |
| Rock Springs TI UP SB | 0970 | 242.2 | 1967 | 16.0 | HS-27 | 97 |
| Mud Springs UP | 0863 | 243.0 | 1965 | 16.5 | HS-21 | 91 |
| Agua Fria River Bridge NB | 1807 | 243.3 | 1980 | N/A | HS-21 | 97 |
| Agua Fria River Bridge SB | 1808 | 243.3 | 1980 | N/A | HS-21 | 97 |
| Coldwater Canyon TI OP NB | 0764 | 244.4 | 1964 | 14.3 | HS-22 | 96 |
| Coldwater Canyon TI OP SB | 0765 | 244.4 | 1964 | 14.7 | HS-22 | 96 |
| Bumble Bee TI UP SB | 1170 | 248.40 | 1966 | 16.3 | HS-29 | 99 |
| Bumble Bee TI OP NB | 1171 | 248.40 | 1966 | 15.3 | HS-18 | 93 |
| Sunset Point TI OP SB | 1352 | 252.50 | 1969 | 17.4 | HS-21 | 94 |
| Sunset Point TI OP NB | 1237 | 252.50 | 1969 | 16.5 | HS-20 | 94 |
| Badger Springs TI OP SB | 0750 | 255.90 | 1963 | 16.1 | HS-21 | F 93 |
| Badger Springs TI OP NB | 0749 | 256.05 | 1963 | 15.0 | HS-21 | F 93 |

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I-17, ANTHEM WAY T.I. TO JCT. SR 69 FINAL DESIGN CONCEPT REPORT

| STRUCTURE NAME | STRUCT. NO. | MP | YEAR BUILT | MIN. VERTICAL CLEARANCE (Ft) | INVENTO RY RATING | SUFFICIENCY RATING |
|-------------------------|----------------|--------|---------------|---------------------------------------|-------------------------|-----------------------|
| Bloody Basin TI OP SB | 0752 | 259.43 | 1963 | 15.8 | HS-21 | F 93 |
| Bloody Basin TI OP NB | 0751 | 259.43 | 1964 | 15.1 | HS-21 | F 93 |
| Big Bug Creek Bridge SB | 20028 | 262.05 | 2012 | N/A | HS-27 | 97 |
| Big Bug Creek Bridge NB | 20027 | 262.05 | 2012 | N/A | HS-27 | 97 |

Note: A sufficiency rating preceded by an "F" denotes functional obsolescence and is assigned by ADOT Bridge Operations Service, Bridge Management Section. Functional obsolescence refers to bridges with lane widths, shoulder widths, or vertical or lateral clearances that do not meet current standards, or the bridge may not be able to handle occasional roadway flooding.

The existing bridges are generally in good structural condition, with sufficiency ratings above 90 in all but four crossings and load ratings of HS-20 or above in all but two locations. The bridge sufficiency rating is a formula-based calculation that considers structural condition and adequacy, functional obsolescence, level of service, and essentiality for public use to present a numeric value representing the bridge's sufficiency to remain in service. The result is a percentage from zero to 100, in which 100 percent would represent a bridge entirely sufficient for its intended use.

Some bridges are reported to have lateral and/or vertical clearances that do not conform to current design standards. These are typically listed as "Functionally Obsolete" in the structure inventory and appraisal data. A functionally obsolete bridge is one that does not meet the current minimum federal geometric or clearance requirements for a new bridge.

Bridges with structural or load capacity issues are listed as "Structurally Deficient"; however, there are no structures classified as structural deficient within the project limits. A structurally deficient bridge typically requires maintenance and/or repair and eventual rehabilitation or replacement to address deficiencies; however, the term does not imply that a bridge is unsafe.

Underpass Bridges

There are seven underpasses within the project limits. In most locations, the proposed I-17 widening requires a 63-foot lateral underclearance, including the anticipated concrete barriers, 10-foot shoulders and two-foot barrier offsets. Limited lateral underclearances exist at the Table Mesa and Bumble Bee TI underpasses. The remaining underpass bridges have sufficient horizontal clearance to accommodate the proposed I-17 widening.

Vertical clearances on these underpasses are currently adequate but surplus clearance is limited, so widening will need to be configured to avoid reducing vertical clearances over I-17 below sixteen feet.

Overpass Bridges

Eleven existing bridges are overpasses. The six overpasses at the Sunset Point, Badger Springs, and Bloody Basin TIs will not be impacted by the near-term proposed widening but will be impacted by the future long-term widening plans for this corridor.

As with the underpasses, overpasses have limited surplus vertical clearance and, in some cases, belowstandard clearances such that widening will need to be configured to avoid reducing vertical clearances to less than sixteen feet. For overpasses with existing clearances below sixteen feet, the clearances cannot be reduced further by the I-17 improvements.

Waterway Bridges

Ten of the bridges are over waterways. Only the recently-constructed Little Squaw Creek Bridge SB and the Big Bug Creek bridges offer surplus deck width that can accommodate I-17 widening. Any scour issues have been addressed by previous ADOT scour mitigation improvements; none of the waterway crossings are currently identified as scour critical.

1.5.7 Geotechnical Profile

Geologic Setting

The section of the I-17 alignment from Anthem Way to Sunset Point in central Arizona is located within the northern limits of the Basin and Range Physiographic Province (Basin and Range) and the southern limits of the Arizona Transition Zone. The Basin and Range is characterized by rugged isolated fault-bounded mountain ranges separated by broad alluvium-filled valleys. Mountain ranges in the Basin and Range generally trend in a north to northwesterly direction. The Transition Zone separates the Basin and Range to the southwest from the Colorado Plateau to the northeast. The rugged terrain of the Transition Zone is characterized by dissected alluvial basins and large bedrock ranges comprised of some of the oldest rocks in Arizona. These old Precambrian basement rocks commonly are overlain with younger Tertiary sedimentary and volcanic rocks.

The generalized geologic units encountered along the project alignment consist of Precambrian metavolcanic rocks, schist and granite intrusions; and interbedded sequence of Tertiary basalts, tuffs, volcaniclastic deposits; Quaternary/Tertiary pediment deposits; and Quaternary surface deposits. In the vicinity of New River, the valley fill consists of well-stratified lake deposits and poorly sorted stream deposits. Numerous Quaternary landslide deposits are present, especially north of Black Canyon City.

The local vegetation consists of various desert grasses, mesquites, palo verdes, creosote, saguaros, and other varieties of small cacti.

The project alignment begins at MP 229 within the valley floor of the New River, west of Daisy Mountain. The corridor circumvents the town of New River, located at an approximate elevation of 2,000 feet. At approximate MP 234, immediately east of Table Mountain, the northbound and southbound lanes of I-17 divide to follow two different alignments. The I-17 alignment begins to traverse mountainous terrain that is wedged between the southwest extension of the Bradshaw Mountains in the Castle Creek Wilderness Area and the New River Mountains. The two alignments then traverse Moore's Gulch at approximate MP 239 and join back together just north of the Rock Springs TI at MP 242. The project alignment continues north towards Black Canyon City and the Black Canyon TI (MP 244.4), also at an approximate elevation of 2,000 feet.

The main drainage systems within these areas are the Agua Fria River and New River, which flow from the northeast to the southwest. From north to south, the major tributaries to these rivers that are paralleled and traversed by the project corridor are Little Squaw Creek and Deadman Wash. Numerous tributaries to these waterways also traverse the alignment, predominantly in a northeast to southwest direction.

North of the Black Canyon City TI, I-17 lies primarily in mountainous bedrock terrain along the west edge of the New River Mountains and just east of the larger Bradshaw Mountains. A fault crosses southbound I-17 north of Black Canyon City (approx. MP 247.8). Movement of this fault, which may be attributed to a nearby landslide,





has caused the need for increased roadway maintenance in this area. The terrain along the corridor generally consists of rolling hills and ridges typical of mountain foothills at the south and north ends of the corridor and a large flat-topped mesa that marks the western edge of the New River Mountains referred to as Black Mesa. Landslide deposits locally occur along the alignment and are exposed just south of, and on the approach up to, the flat-topped mesa.

The existing I-17 corridor between MP 244.4 and MP 247 is predominantly underlain by Tertiary sediments, with a minor amount of metavolcanic rock located north of MP 246. Between approximately MP 247 and MP 248, the existing roadway is predominantly underlain by Hickey Formation basalt.

North of MP 248, the northbound roadway roughly follows the contact between Hickey Formation basalt metavolcanic rock until the road tops out on Black Mesa at approximately MP 250. The southbound roadway is underlain by metavolcanic rock from approximately MP 248 until it tops out on Black Mesa at MP 250.5. The southbound and northbound roadways are then underlain by basalt to approximately MP 256.5 and metavolcanic rock from MP 256.5 to Big Bug Creek at MP 262. Several old landslide deposits have recently been mapped by the Arizona Geological Survey north of the Black Canyon City TI and south of Bumble Bee Road. While there is no indication that this represents a fatal flaw for the project, these landslides and others yet to be identified may impact the existing I-17 roadways and will need to be investigated further in final design.

There are several inclinometer locations between the Black Canyon City TI and Bumble Bee TI. These locations were designated to measure the stability of the cut slopes along the northbound roadway. Four inclinometers are located along the outside shoulder of the northbound roadway at MP 247.4 between the outside edge of roadway striping and the existing guardrail. Another location is at the top of the large cut known as Cape Horn, MP 247.5. Another inclinometer is located between the northbound and southbound roadways at MP 247.5. The functionality of these monitoring stations should be maintained; the contractor will need to protect or replace the units during the construction of the recommended alternative.

Groundwater/Surface Water Conditions

Water was observed in Bumble Bee Creek at the bridge crossing just south of Bumble Bee Ranch (2007). Residents in the area indicated that this water originates from springs along the flanks of the creek upstream of the bridge. A small amount of water was also observed in a small wash immediately west of existing I-17 near MP 245 (2007). Within Little Squaw Creek SB, test boring B-3, located at the bridge pier location, was completed as an open standpipe piezometer. Water was observed in Little Squaw Creek prior to bridge construction (2009) with an approximate groundwater depth ranging from 12 to 33 feet (elevation of 1887 to 1908 feet). It is assumed the piezometer was abandoned in accordance with Arizona Department of Water Resources requirements during construction. Shallow groundwater may be anticipated in other drainages and low-lying areas throughout the project corridor, especially following large and/or prolonged rain storms.

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Roadway Cuts

Information on the existing roadway cuts is presented in Table 7. Recent wedge and block failures and slope deterioration were observed along several existing cut slopes within the project corridor. The existing slopes are susceptible to continued block erosion when exposed to water and may require continued maintenance. In general, in areas where rockfall has been noted, the existing pavement surface has been dented and otherwise slightly damaged.

TABLE 7 – ROADWAY CUTS

| Milepost | Geologic Material | Observed Potential Geological Hazards |
|---------------------|---|--|
| NB MP 232 to MP 240 | Quaternary sediments and Precambrian metavolcanics | Moderate to large scale sloughing, some rockfall |
| SB MP 251 to MP 248 | Tertiary basalt and Precambrian metavolcanics | Rockfall and large wedge failures, moderate sloughing |
| SB MP 248 to MP 245 | Tertiary basalt, Precambrian metavolcanics, and Tertiary sandstone and tuff | Rockfall, moderate to large scale sloughing, mapped landslides |
| SB MP 244 to MP 242 | Quaternary sediments | Heavily eroded, undercutting |
| SB MP 240 to MP 238 | Quaternary alluvial sediments | Rockfall on both center lane and shoulder (large cobbles and medium to large boulders), seep on center lane over slough material |
| SB MP 238 to MP 236 | Quaternary sediments | Sloughs on both center lane and shoulder, right of way on road adjacent to I-17 is being undercut and cut has eroded back to guard rail |
| SB MP 235 to MP 234 | Precambrian metavolcanics | Large scale wedge failure |

Ditches and containment walls appeared to be completely full in most cases (as recently as 2018) and should be cleaned out more regularly in order to decrease rock material from making its way onto the roadway. In addition, larger catchment areas and alterations in slope geometry should be considered during final design.

Roadway Fills

The roadway alignment typically is constructed on two approximately three- to five-foot high embankments divided by an intermediate ditch. These fill sections increase to heights in excess of 60 feet at select locations near drainage/canal crossings. Existing fill slopes along the alignment are approximately 6H:1V (horizontal to vertical) at the south end of the project area but increase significantly by the north end of the study segment. The slopes appear to be stable with a significant amount of desert vegetation growing on them. However, minor to moderate rain-induced surface erosion was observed locally along the project corridor.

Pavement Subgrade Conditions

In general, it is anticipated that subgrade conditions will be suitable for most of the alignment. The preliminary investigation identified the following areas of poor subgrade:

- SB Sta 1877+50 to 1957+00 (~MP 236 to 238);
- NB and SB Sta 2289+00 to 2320+00 (~MP 244 to 245); and
- SB Sta 2625+00 to 2710+00 (~MP 251 to 252).

Pavement Conditions

I-17 is a divided four-lane highway with 12-foot wide primary travel lanes and paved shoulders. Pea gravel or recycled AC placement has occurred beyond the paved shoulder in some areas of the southbound lanes.

In 2007, except for select localized areas in the shoulder, the existing pavements along both northbound and southbound lanes of I-17 was in good to very good condition throughout the length of the project alignment. In general, the pavements did not display potholes, rutting, corrugation, depressions, swells, and/or slippage cracking. In reviewing ADOT Pavement Management System Information it is apparent that neither cracking nor rutting is a concern in the study section.

Review of ADOT's Pavement Management System Information shows that both the northbound and southbound segments have received varying surface treatments. Table 2 of the 2007 Preliminary Geotechnical Assessment in the project geotechnical assessment report summarizes the treatments that have been applied to the existing project alignment since its construction. More than 20 roadway construction and/or resurfacing projects have been conducted within the project corridor since 1949. Most of the project length has been re-paved since 2007.

The entire roadway has been milled and overlaid since 1992. A 2003 project involved milling and filling, realignment, and bridge repair from MP 256 to MP 263. The northbound roadway from MP 240 to MP 245 was repaved in mid-2013. Based on the review of the as-built plans, the existing pavement section varies from 0.5 inches of friction course over 3.0 to 11.0 inches of bituminous materials over 3 to 13 inches of aggregate base (AB) over 6 to 24 inches of select material. Occasional areas had sealed subgrade up to 12 inches thick, but generally any treatment of the subgrade is not apparent from the review of the as-built plans.

2.0 Traffic and Crash Data

2.1 Traffic Analysis

2.1.1 Introduction

A Preliminary Traffic Report (March 2007), a traffic Technical Memorandum (November 2014), and an updated Preliminary Traffic Report (October 2017) were prepared in support of the development of the Design Concept Report for this project. The traffic analyses present traffic volume projections and roadway capacity analyses for mainline I-17 beginning at the I-17/Anthem Way TI and extending north to approximately MP 262, south of the Cordes Junction TI. The scope of the study assumed no major modifications to the traffic interchanges. Therefore, no traffic volume projections or ramp terminal capacity calculations were performed as part of the traffic analysis.

A design year of 2030 was used in the original 2007 analysis. Because work on this study stopped for several years and economic conditions changed substantially, growth projections were revised downward and the design year is now 2040. The purpose of the 2014 memorandum was to summarize the criteria and methodology for developing 2035 and 2040 traffic volumes, capacity analysis, and level of service results, which are included in this chapter, along with updated crash data. The current traffic report uses 2040 traffic volumes.

2.1.2 Year 2040 Traffic Volume Development

Projected traffic growth rates have changed substantially since the original traffic study for this project was completed in 2007. Traffic volumes for the study section of I-17 and for sections north and south of the study area were obtained from the ADOT Transportation Planning website. The process included collection of 2016 traffic data, including volumes, K, D, and T factors. Table 8 presents a summary of 2016 traffic data.

| Location | Two Way AADT | к | D | т |
|-----------------------------------|--------------|-----|-----|-------|
| Anthem Way to New River Road | 45,900 | 10% | 61% | 11.6% |
| New River to Black Canyon City | 41,600 | 10% | 60% | 24.1% |
| Black Canyon City to Sunset Point | 34,200 | 10% | 56% | 26.1% |
| Sunset Point to Cordes Junction | 36,200 | 10% | 60% | 26.1% |

TABLE 8 - I-17 MAINLINE 2016 TRAFFIC DATA SUMMARY

The peak hour traffic on I-17 fluctuates widely in the study area depending on day of week and time of year. This section of I-17 serves a mix of traffic that can be described as rural/recreational traffic. The rural/recreational traffic has a unique traffic characteristic, where the weekend peak hour traffic exceeds the weekday peak hour. This characteristic is considerably different than the typical urban weekday morning and late afternoon workhome commuting peak hour of traffic. In addition to the weekend peak hour of traffic, the rural/recreational traffic is typically subject to seasonal volume variations. For example, there are generally more recreational trips in the

summer season. The rural segments of I-17 have many of the highest hourly volumes occurring on popular travel holidays such as Memorial Day and Labor Day.

By examining the existing 2016 volumes, it was determined that Saturday traffic volumes are on average 20% greater than the seven-day average volumes. These seven-day averages are typically considered to be the traditional AADT.

Traffic volume projections for the year 2030 and existing K, D, and T factors for the study section of I-17 were obtained from ADOT Transportation Planning website. Traffic volume projections for the year 2040 were provided by ADOT Multimodal Planning Division. In addition to obtaining AADT projections for the years 2030 and 2040, the Saturday AADT was calculated by increasing the seven-day volumes by 20%. The Saturday AADT was used to represent volumes for a peak weekend traffic condition.

Once the 2040 traffic volumes were determined, the K and D factors were applied to determine the directional design hourly volume (DDHV=AADT*K*D). Table 9 presents a summary of the DDHV. The values for Monday through Sunday were considered seven-day DDHV and the values for Saturday were considered Weekend DDHV.

TABLE 9 – I-17 MAINLINE DDHV SUMMARY

| Location | 2016 (Mon-Sun) | 2016 (Sat) | 2040 (Mon-Sun) | 2040 (Sat) |
|-------------------------------------|-------------------|---------------|-------------------|---------------|
| Anthem Way to New River Road | 2,797 | 3,356 | 3,595 | 4,315 |
| New River Road to Black Canyon City | 2,498 | 2,998 | 3,391 | 4,069 |
| Black Canyon City to Sunset Point | 1,913 | 2,295 | 2,918 | 3,501 |
| Sunset Point to Cordes Junction | 2,171 | 2,605 | 3,145 | 3,774 |

2.1.3 Capacity Analysis and Results

Level of service (LOS) is a method of describing the operating characteristics of a section of highway. Broadly defined in terms of traffic flow, LOS A is associated with free flow traffic, LOS B indicates reasonable free flow, LOS C is stable operations, LOS D is the lower range of stable flow, LOS E is unstable flow, and LOS F indicates breakdowns in flow.

The Highway Capacity Manual (HCM) was used to evaluate freeway capacity and level of service. The measure used to provide an estimate of freeway LOS is density expressed in terms of the number of equivalent passenger cars per mile per lane (pc/mi/ln). Table 10 summarizes the LOS and density thresholds for freeway analysis.

TABLE 10 – HCM LEVEL OF SERVICE AND DENSITY CRITERIA



| ine Density | (pc/mi/ln) |
|-------------|------------|
| ≤11 | |
| >11-18 | |
| >18-26 | |
| >26-35 | |
| >35-45 | |
| >45 | |

General design levels of service and capacity for Arizona state roadways are described in the *Roadway Design Guidelines* (RDG) from the ADOT Roadway Engineering Group. The design levels of service and capacity for various conditions are shown in Table 103.2A of the guidelines. Table 11 summarizes the design levels of service. The RDG indicates that where a range is given, the higher level of service should be provided except where costs or environmental constraints dictate a lower level of service.

Using the DDHV and roadway characteristics, the capacity analysis was conducted using the Highway Capacity Software (HCS). Table 13 and Table 14 summarize the results of the capacity analysis:

TABLE 13 - 2016 AND 2040 7-DAY DDHV LEVEL OF SERVICE

| Roadway Section | No. of Lanes in | 2016 7-Day DDHV | | 2040 7-Day DDHV | |
|-----------------------|--------------------|-----------------------|-----|-----------------------|-----|
| and Terrain | Each Direction | Density (pc/mi/ln) | LOS | Density (pc/mi/ln) | LOS |
| NB and SB (MP229-232) | 2 | 25.9 | С | 40.0 | Е |
| Level | 3 | | | 21.1 | С |
| | · | | | | |
| NB and SB (MP232-244) | 2 | 31.2 | D | 63.8 | F |
| Rolling | 3 | | | 26.7 | D |
| | | | | | |
| NB (MP244-252) | 2 | 27.4 | D | 72.0 | F |
| Mountainous Upgrade | 3 | | | 28.1 | D |
| | | | | | |
| SB (MP252-244) | 2 | 19.5 | С | 36.3 | Е |
| Mountainous Downgrade | 3 | | | 19.9 | С |
| | | | | | • |
| NB and SB (MP252-262) | 2 | 25.9 | С | 53.7 | F |
| Rolling | 3 | | | 24.7 | С |

TABLE 11 – ADOT DESIGN LEVELS OF SERVICE

| Design Levels of Service |
|-----------------------------|
| |
| В |
| В |
| B-C |
| C-D |
| |

Source: Table 103.2A, ADOT Roadway Design Guidelines.

The portion of I-17 included in this study area is unique in many ways. Primary factors include the mix of traffic and the connection to major urban areas from northern Arizona. Weekend traffic is approximately 20 percent higher than the average weekday traffic. As growth continues in Maricopa, Yavapai, and Coconino counties, the area in between is predicted to develop into an urban / urban fringe area.

Taking into account the varying traffic demands, mix of vehicles, seasonal travel demand and the urbanization of northern and central Arizona, ADOT has selected LOS D as the appropriate level of service to be utilized for I-17 in this study.

Because terrain and speed impact the capacity analysis results, the I-17 mainline was broken into four segments for evaluation. The southern portion (MP 229-232) was evaluated as level terrain. The next segment to the north (MP 232-244) was evaluated as rolling terrain. On the Black Canyon Hill, MP 244-252 was evaluated using the composite grade methodology for mountainous terrain. The northern portion of the project area (MP 252-262) was evaluated as rolling terrain. The northbound and southbound roadways in the mountainous terrain portion of the project were analyzed separately, based on the specific grades. Table 12 summarizes each segment and the respective roadway characteristics evaluated.

TABLE 12 – I-17 MAINLINE SEGMENTS

| Segment | Terrain | Speed |
|--|-----------------------------|--------|
| I-17, Anthem Way to New River (MP 229-232) | Level | 75 MPH |
| I-17, New River to Black Canyon City (MP 232-244) | Rolling | 75 MPH |
| I-17, Black Canyon City to Sunset Point (MP 244-252) | Mountainous/Composite Grade | 65 MPH |
| I-17, Sunset Point to Cordes Junction (MP 252-262) | Rolling | 75 MPH |

TABLE 14 – 2016 AND 2040 WEEKEND DDHV LEVEL OF SERVICE

| Roadway Section | No. of Lanes in | 2016 Weekend DDHV | | 2040 Weekend DDHV | |
|---|--------------------|-----------------------|-----|-----------------------|-----|
| and Terrain | Each Direction | Density (pc/mi/ln) | LOS | Density (pc/mi/ln) | LOS |
| | 2 | 34.8 | D | 65.5 | F |
| NB and SB (MP229-232) | 3 | | | 27.0 | D |
| | 4 | | | 18.6 | С |
| | · | | | | |
| | 2 | 44.9 | Е | 174.0 | F |
| NB and SB (MP232-244) | 3 | | | 36.3 | Е |
| Troining | 4 | | | 23.0 | С |
| | | | | | • |
| | 2 | 37.5 | Е | 257.2 | F |
| NB (MP244-252) Mountainous Upgrade | 3 | | | 38.7 | E |
| | 4 | | | 24.1 | С |
| | - | | | | |
| | 2 | 24.6 | С | 56.1 | F |
| SB (MP252-244) Mountainous Downgrade | 3 | | | 25.2 | С |
| Mountaineus Downgrade | 4 | | | 17.6 | В |
| | · | | | | |
| | 2 | 34.9 | D | 114.1 | F |
| NB and SB (MP252-262) | 3 | | | 32.8 | D |
| | 4 | | | 21.5 | С |

2.1.4 Two-Lane and Three-Lane Failure Year Sensitivity Analyses

As part of the capacity analysis, the last year during which each segment of the study area exhibits LOS D (the minimum acceptable design level of service) with two lanes and three lanes was determined. Utilizing the HCS, the maximum DDHV that corresponds with a density of 34.9 pc/mi/ln was calculated for each portion of the study area. Once the DDHV was calculated, the K and D factors were used to determine the AADT associated with the "failure year." Failure year is defined as the last year in which forecasted traffic volumes result in the segment operating at an acceptable LOS D; the following year, operations deteriorate to LOS E. Upon determining the failure year AADT values, linear relationships between the 2016 and 2040 Saturday AADTs were used to estimate the failure year for peak weekend traffic conditions.

Table 15 shows the predicted two-lane failure year for each representative segment. Table 16 shows the predicted three-lane failure year for each representative segment.

TABLE 15 – TWO-LANE FAILURE YEAR SUMMARY

| Location on I-17 Mainline | MP | Failure Year AADT | Weekend Failure Year |
|---|-----------|-------------------|-------------------------|
| Anthem Way to New River Rd | 229 – 232 | 55,080 | 2016* |
| New River Rd to Black Canyon City | 232 – 244 | N/A | Currently Failing |
| Black Canyon City to Sunset Point (NB) | 244 252 | N/A | Currently Failing |
| Sunset Point to Black Canyon City (SB) | 244 – 252 | 50,980 | 2027 |
| Sunset Point to Cordes Jct. | 252 – 262 | 43,420 | 2016* |

* Minimal growth in the 2016 traffic counts should result in LOS E in 2017

TABLE 16 – THREE-LANE FAILURE YEAR SUMMARY

| Location on I-17 Mainline | MP | Failure Year AADT | Weekend Failure Year |
|---|-----------|-------------------|-------------------------|
| Anthem Way to New River Rd | 229 – 232 | 82,620 | 2058 |
| New River Rd to Black Canyon City | 232 – 244 | 66,500 | 2038 |
| Black Canyon City to Sunset Point (NB) | 244 252 | 59,290 | 2036 |
| Sunset Point to Black Canyon City (SB) | 244 – 232 | 76,520 | 2056 |
| Sunset Point to Cordes Jct. | 252 – 262 | 65,080 | 2043 |

2.1.5 Flex Facility (Black Canyon City TI to Sunset Point TI)

As part of the capacity analysis, two-lane reversible, or "flex" roadway facilities were evaluated for the segment of I-17 from Black Canyon City to Sunset Point.

An estimate of 45% of the Weekend DDHV was assigned to the new flex roadway. This estimate of traffic using the flex lane facility assumes that traffic will be fairly well balanced between the mainline and flex facility. Speed, density, and travel time data will be collected and displayed on DMS prior to the mainline/flex facility split to allow motorists to select the fastest route. As the volume increases on one facility and travel times increase, this information can be provided to motorists, allowing them to select the route with the fastest travel time, balancing traffic between the two routes.

It was assumed that the 2040 volumes would follow the same trend as the existing 2016 volumes, with peak volumes in the northbound direction Monday through Saturday and the off-peak volume in the southbound direction. In addition, the peak volumes would occur in the southbound direction on Sunday, with the off-peak volume in the northbound direction. To address this trend, the two-lane flex roadway would operate in the northbound direction Friday and Saturday, and in the southbound direction on Sunday. The 2040 Weekend DDHV volumes were analyzed to consider the peak traffic conditions along the corridor.

Table 17 summarizes the DDHV for the flex facility:

TABLE 17 – I-17, MAINLINE AND FLEX ROADWAY PEAK WEEKEND DDHV

| Year | Peak Week | C Direction | Off-Peak Direction Weekend DDHV |
|-------|---------------|---------------|------------------------------------|
| . oui | I-17 Mainline | Flex Facility | I-17 Mainline |
| 2040 | 1,926 | 1,575 | 2,751 |

Using the Weekend DDHV, peak hour characteristics, and roadway characteristics, the capacity analysis was conducted using the HCS. Results of the I-17 northbound and southbound two-lane flex lane capacity analysis are summarized in Table 18 and Table 19, respectively, below:

TABLE 18 - I-17, NORTHBOUND TWO-LANE FLEX LANE LOS RESULTS

| Description | Number | 2040 \$ | Saturday | Commont |
|-------------|----------|---------|----------|----------------------|
| Description | of Lanes | LOS | Density | comment |
| NB | 2 | П | 27.6 | 55% of 2040 |
| Mainline | 2 | U | 27.0 | Peak DDHV |
| NB | 2 | C | 10.7 | 45% of 2040 |
| Flex | 2 | U | 19.7 | Peak DDHV |
| SB | 2 | П | 32.6 | 2010 Off-Pook DDHV |
| Mainline | 2 | D | 52.0 | 2040 OII-Feak DDI IV |

TABLE 19 – I-17, SOUTHBOUND TWO-LANE FLEX LANE LOS RESULTS

| Description | Number | 2040 | Sunday | Commont | |
|-------------|----------|------|---------|--------------------|--|
| Description | of Lanes | LOS | Density | Comment | |
| SB | 2 | D | 15.7 | 55% of 2040 | |
| Mainline | 2 | D | 15.7 | Peak DDHV | |
| SB | 2 | C | 21.0 | 45% of 2040 | |
| Flex | 2 | C | 21.0 | Peak DDHV | |
| NB | 2 | ⊏* | 59.7 | | |
| Mainline | 2 | Г | 56.7 | 2040 OII-FEAK DDHV | |

* The off-peak direction will operate at a LOS D until exceeding a volume of approximately 2,210 vehicles per hour. This volume is expected to be exceeded after the year 2026.

2.1.6 Flex Facility Merge and Diverge Analysis (Black Canyon City TI to Sunset Point TI)

As part of the flex facility capacity analysis, the merge and diverge areas were evaluated to determine the recommended number of lanes exiting or entering I-17 to and from the flex lanes. The merge and diverge analysis was conducted using HCS.

As assumed with the flex facility capacity analysis, a peak directional volume of 3,501 vehicles between Black Canyon City and Sunset Point was assumed by 2040. It was also assumed that 55% of the 2040 volume (1,926 vehicles) would utilize the existing I-17 alignment and 45% (1,575 vehicles) would utilize the flex lanes. The truck percentage for this segment is 26%, which represents a total of 910 trucks (501 on the I-17 alignment and 409 on the flex lane alignment).

Table 20 summarizes the results of the merge analysis for both northbound and southbound I-17 with the flex lanes.

TABLE 20 - SUMMARY OF MERGE ANALYSIS

| Configuration at Gore Point | Overall LOS | I-17 LOS (V/C) | Flex Lane Ramp LOS (V/C) | | |
|-----------------------------------|---|--------------------|-----------------------------|--|--|
| South Crossover, Se | outhbound Flex | c Lanes Merging wi | th SB I-17 | | |
| Two I-17 Lanes, One Flex Lane | F | F (1.08) | F (1.06) | | |
| Two I-17 Lanes, Two Flex Lanes | A | F (1.08) | N/A (0.53) | | |
| North Crossover, N | North Crossover, Northbound Flex Lanes Merging with NB I-17 | | | | |
| Two I-17 Lanes, One Flex Lane | F | F (1.09) | F (1.07) | | |
| Two I-17 Lanes, Two Flex Lanes | F | F (1.09) | N/A (0.54) | | |

The results of the HCS analysis for the southbound flex lanes merging with southbound I-17 show that a onelane ramp from the flex lanes will not provide enough capacity for the vehicles on the flex lane. The analysis also shows that the I-17 segment following the merge will not provide enough capacity for the total number of vehicles. However, the software assumes this segment is only two lanes as it cannot model an added lane from the on-ramp. Based on adjusted calculations, a three-lane segment following the merge would provide enough capacity. A two-lane ramp from the flex lanes will provide enough capacity for the vehicles on the flex lanes. The two-lane ramp may be one exit-only lane and one option lane.

The results of the HCS analysis for the northbound flex lanes merging with northbound I-17 show that neither a one-lane ramp nor a two-lane ramp from the flex lanes will provide enough capacity for the vehicles on the flex lane. The analysis also shows that the I-17 segment following the merge will not provide enough capacity for the total number of vehicles.

A sensitivity analysis was conducted to determine when the northbound flex lanes merge with northbound I-17 will fail. The results of the sensitivity analysis determined that the last year that the merge would operate at an acceptable level of service is 2034. However, the Preliminary Traffic Report shows that the basic freeway segment directly after this merging area will fail much sooner than this, within the (past) year of 2016, if the segment is left as a two-lane roadway.

Table 21 summarizes the results of the diverge analysis for both northbound and southbound I-17 with the flex lanes.

TABLE 21 – SUMMARY OF DIVERGE ANALYSIS

| Configuration at Gore Point | Overall LOS | I-17 LOS (V/C) | Flex Lane Ramp LOS (V/C) | | | |
|---|---|-------------------|-----------------------------|--|--|--|
| South Crossover, NB Flex Lanes Diverging with NB I-17 | | | | | | |
| Three I-17 Lanes, One Optional Exit Lane | F | N/A (0.42) | F (1.13) | | | |
| Three I-17 Lanes, One Trapped Exit Lane | F | N/A (0.42) | F (1.136) | | | |
| Three I-17 Lanes, One Trapped & One Optional Exit Lane | А | N/A (0.42) | N/A (0.57) | | | |
| North Crossover, SB Fl | North Crossover, SB Flex Lanes Diverging with SB I-17 | | | | | |
| Two I-17 Lanes, One Optional Exit Lane | F | N/A (0.59) | F (1.06) | | | |
| Two I-17 Lanes, One Trapped Exit Lane | F | N/A (0.59) | F (1.06) | | | |
| Two I-17 Lanes, One Trapped & One Optional Exit Lane | А | N/A (0.59) | N/A (0.53) | | | |

The results of the HCS analysis for the northbound flex lanes diverging from northbound I-17 show that a onelane ramp, either optional or trapped lane, exiting to the flex lanes from I-17 will not provide enough capacity. The analysis shows that the I-17 segment north of the diverge area will provide enough capacity for the number of vehicles remaining on I-17. The results also indicate that a two-lane ramp exiting to the flex lanes from I-17 will provide enough capacity. The two-lane ramp may be one exit-only lane and one option lane.

The results of the HCS analysis for the southbound flex lanes diverging with southbound I-17 show that a onelane ramp, either optional or trapped lane, exiting to the flex lanes from I-17 will not provide enough capacity. The analysis shows that the I-17 segment south of the diverge area will provide enough capacity for the number of vehicles remaining on I-17. The results also indicate that a two-lane ramp exiting to the flex lanes from I-17 will provide enough capacity. The two-lane ramp may be one exit-only lane and one option lane.

2.1.7 Northbound Climbing Lane (Black Canyon City TI to Sunset Point TI)

A northbound climbing lane from Black Canyon City to Sunset Point was also evaluated as part of the capacity analysis. In that analysis, the climbing lane was found to improve the LOS from a borderline LOS C/D to a solid LOS C. According to the analysis results, construction of a northbound climbing lane between Black Canyon City and Sunset Point would improve the level of service in 2040 from LOS F to LOS E. The results indicate that the last year this segment would operate at LOS D with the implementation of a climbing lane is the year 2036.

The beginning of a freeway climbing lane depends on the speeds at which trucks approach the grade. According to AASHTO, this point should occur at or prior to a ten mph decrease in truck speed below the average running speed. The climbing lane should extend to a point beyond the crest, where a typical truck could attain a speed that is within ten mph of the speed of other vehicles. Based on the criteria established by AASHTO and a normal operating speed of 65 mph, the northbound climbing lane should begin at approximately MP 244.44 and end at approximately 252.65.

2.2 Crash Analysis

2.2.1 Source of Data

Crash data was obtained from ADOT for the I-17 mainline from MP 228 to MP 262. The data covers a five-year period from June 2012 to May 2017.

2.2.2 Crash Data

The five-year crash history for the study section is summarized in Table 22 and Table 23. Table 22 shows the number of crashes by manner of collision. On average, there are more crashes in the northbound direction, with 215 crashes per year in the study section. There are approximately 150 crashes per year in the southbound direction. The majority of the crashes in the study section are single vehicle crashes. There is also a large proportion of rear-end crashes, particularly in the northbound direction.

TABLE 22 – I-17, MP 229 – 262 CRASHES BY MANNER OF COLLISION

| MANNER OF COLLISION | 6/1/2012 TO 12/31/2012 | 1/1/2013 TO 12/31/2013 | 1/1/2014 TO 12/31/2014 | 1/1/2015 TO 12/31/2015 | 1/4/2016 TO 12/31/2016 | 1/1/2017 TO 5/31/2017 | 5- YEAR TOTAL | YEARLY AVG TOTAL |
|-----------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|-----------------------------|---------------------|------------------------|
| Northbound | | | | | | | | |
| Angle | 0 | 2 | 2 | 1 | 5 | 0 | 10 | 2 |
| Head on | 0 | 1 | 2 | 1 | 1 | 0 | 5 | 1 |
| Rear End | 34 | 54 | 63 | 103 | 108 | 39 | 401 | 80.2 |
| Sideswipe (Opposite Direction) | 0 | 2 | 0 | 2 | 2 | 0 | 6 | 1.2 |
| Sideswipe (Same Direction) | 15 | 27 | 19 | 28 | 33 | 13 | 135 | 27 |
| Single Vehicle | 52 | 92 | 92 | 109 | 103 | 44 | 492 | 98.4 |
| Rear to Rear | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0.2 |
| Left Turn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Rear to Side | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0.2 |
| Other | 1 | 5 | 3 | 9 | 5 | 1 | 24 | 4.8 |
| Northbound Total | 102 | 183 | 182 | 253 | 257 | 98 | 1075 | 215 |
| O south has south | | | | | | | | |
| Southbound | 4 | | 0 | 4 | 4 | 0 | | 0.0 |
| Angle | 1 | 1 | 0 | 1 | 1 | 0 | 4 | 0.8 |
| Head on | 0 | 1 | 1 | 0 | 1 | 0 | 3 | 0.6 |
| Rear End | 18 | 19 | 22 | 34 | 46 | 13 | 152 | 30.4 |
| Sideswipe (Opposite Direction) | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0.2 |
| Sideswipe (Same Direction) | 11 | 12 | 16 | 12 | 24 | 6 | 81 | 16.2 |
| Single Vehicle | 41 | 80 | 86 | 88 | 121 | 51 | 467 | 93.4 |
| Rear to Rear | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0.2 |
| Left Turn | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 0.4 |
| Rear to Side | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other | 1 | 6 | 6 | 8 | 11 | 2 | 34 | 6.8 |
| Southbound Total | 72 | 120 | 131 | 143 | 205 | 74 | 745 | 149 |

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Table 23 shows the number of crashes by severity. The data indicates the northbound and southbound roadways exhibit similar levels of severe crashes. The southbound roadway tends to have slightly more fatal crashes, with a mean of approximately three fatal crashes per year compared to the northbound roadway's approximately two and a half fatal crashes per year.

FIGURE 4 – NORTHBOUND I-17 AVERAGE NUMBER OF CRASHES BY MILEPOST





FIGURE 5 – SOUTHBOUND I-17 AVERAGE NUMBER OF CRASHES BY MILEPOST



TABLE 23 - I-17, MP 229 - 262 CRASHES BY SEVERITY

| SEVERITY | 6/1/2012 TO 12/31/2012 | 1/1/2013 TO 12/31/2013 | 1/1/2014 TO 12/31/2014 | 1/1/2015 TO 12/31/2015 | 1/4/2016 TO 12/31/2016 | 1/1/2017 TO 5/31/2017 | 5- YEAR TOTAL | YEARLY AVG TOTAL |
|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|-----------------------------|---------------------|------------------------|
| Northbound | | | | | | | | |
| No Injury | 77 | 125 | 120 | 181 | 174 | 72 | 749 | 149.8 |
| Possible Injury | 11 | 22 | 26 | 28 | 27 | 10 | 124 | 24.8 |
| Non-Incapacitating Injury | 10 | 27 | 24 | 34 | 44 | 11 | 150 | 30 |
| Incapacitating Injury | 2 | 8 | 8 | 9 | 10 | 3 | 40 | 8 |
| Fatal | 2 | 1 | 4 | 1 | 2 | 2 | 12 | 2.4 |
| Northbound Total | 102 | 183 | 182 | 253 | 257 | 98 | 1075 | 215 |
| Southbound | | | | | | | | |
| No Injury | 55 | 75 | 72 | 93 | 141 | 48 | 484 | 96.8 |
| Possible Injury | 6 | 20 | 21 | 15 | 25 | 7 | 94 | 18.8 |
| Non-Incapacitating Injury | 8 | 16 | 27 | 23 | 32 | 15 | 121 | 24.2 |
| Incapacitating Injury | 0 | 6 | 7 | 9 | 6 | 4 | 32 | 6.4 |
| Fatal | 3 | 3 | 4 | 3 | 1 | 0 | 14 | 2.8 |
| Southbound Total | 72 | 120 | 131 | 143 | 205 | 74 | 745 | 149 |

The crash data was also sorted and grouped by MP location to identify potential high crash locations within the study area. The results of this analysis are presented in the bar charts shown in Figure 4 and Figure 5. Each bar represents the average number of crashes within a one-mile segment. For example, there were an average of approximately eight crashes per year on northbound I-17, between MP 244.00 and MP 244.99.

The data indicate that in the northbound direction, the average number of crashes per mile tends to be higher in the mountainous portions of the study area (MP 244 to 252). As a result, the manner of collision and severity analyses were refined to focus on this area. The results are shown in Table 24 and Table 25.

Table 24 shows the number of crashes by manner of collision for the mountainous section. On average, there was almost twice as many crashes in the northbound direction, with approximately 85 crashes per year. There were approximately 47 crashes per year in the southbound direction. Approximately 50% of the crashes in the northbound mountainous section were rear-end crashes. The number of northbound rear-end crashes in this segment account for more than half of all northbound rear-end crashes within the entire project area. Approximately 60% of the crashes in the southbound mountainous section were single-vehicle crashes.

TABLE 24 – I-17, MP 244 – 252 CRASHES BY MANNER OF COLLISION

| | 1 | - | | | 1 | | | |
|----------------------|------------|------------|------------|------------|------------|-----------|-------|-------------|
| MANNER OF | 6/1/2012 | 1/1/2013 | 1/1/2014 | 1/1/2015 | 1/4/2016 | 1/1/2017 | 5- | YEARLY |
| COLLISION | 10 | 10 | | TO | 10 | 10 | YEAR | AVG |
| Newth Leaves 1 | 12/31/2012 | 12/31/2013 | 12/31/2014 | 12/31/2015 | 12/31/2016 | 5/31/2017 | IUIAL | TOTAL |
| Northbound | _ | - | - | | - | - | | |
| Angle | 0 | 0 | 0 | 1 | 2 | 0 | 3 | 0.6 |
| Head on | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Rear End | 24 | 23 | 31 | 58 | 60 | 17 | 213 | 42.6 |
| Sideswipe | 0 | 0 | 0 | 1 | 1 | 0 | 2 | 0.4 |
| (Opposite Direction) | Ű | Ű | | | | | | 0.1 |
| Sideswipe | 8 | 16 | 5 | 10 | 14 | 4 | 57 | 11.4 |
| (Same Direction) | | | | | | | 407 | a- 4 |
| Single Vehicle | 11 | 26 | 22 | 40 | 31 | 1 | 137 | 27.4 |
| Rear to Rear | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0.2 |
| Left Turn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Rear to Side | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0.2 |
| Other | 0 | 2 | 1 | 4 | 2 | 0 | 9 | 1.8 |
| Northbound Total | 43 | 67 | 60 | 114 | 110 | 29 | 423 | 84.6 |
| | | | | | | | | |
| Southbound | 1 | | r | r | | r | | |
| Angle | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0.2 |
| Head on | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 0.4 |
| Rear End | 8 | 3 | 5 | 13 | 20 | 5 | 54 | 10.8 |
| Sideswipe | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0.2 |
| (Opposite Direction) | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0.2 |
| Sideswipe | 2 | 1 | 6 | 4 | 4 | 0 | 17 | 34 |
| (Same Direction) | - | • | | • | • | Ű | | 0.1 |
| Single Vehicle | 10 | 26 | 33 | 30 | 28 | 20 | 147 | 29.4 |
| Rear to Rear | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Left Turn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Rear to Side | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Other | 0 | 1 | 3 | 1 | 4 | 2 | 11 | 2.2 |
| Southbound Total | 21 | 33 | 48 | 48 | 56 | 27 | 233 | 46.6 |

exhibits approximately 60% of the number of incapacitating injury crashes per year compared to the northbound roadway.

TABLE 25 – I-17. MP 244 – 252 CRASHES BY SEVERITY

| SEVERITY | 6/1/2012 TO 12/31/2012 | 1/1/2013 TO 12/31/2013 | 1/1/2014 TO 12/31/2014 | 1/1/2015 TO 12/31/2015 | 1/4/2016 TO 12/31/2016 | 1/1/2017 TO 5/31/2017 | 5- YEAR TOTAL | YEARLY AVG TOTAL |
|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|-----------------------------|---------------------|------------------------|
| Northbound | | | | | | | | |
| No Injury | 38 | 53 | 41 | 80 | 78 | 25 | 315 | 63 |
| Possible Injury | 0 | 5 | 7 | 19 | 14 | 1 | 46 | 9.2 |
| Non-Incapacitating Injury | 3 | 6 | 9 | 12 | 13 | 3 | 46 | 9.2 |
| Incapacitating Injury | 2 | 3 | 1 | 2 | 5 | 0 | 13 | 2.6 |
| Fatal | 0 | 0 | 2 | 1 | 0 | 0 | 3 | 0.6 |
| Northbound Total | 43 | 67 | 60 | 114 | 110 | 29 | 423 | 84.6 |
| | | | | | | | | |
| Southbound | | | | | r | | | |
| No Injury | 13 | 16 | 31 | 32 | 43 | 18 | 153 | 30.6 |
| Possible Injury | 5 | 7 | 4 | 5 | 6 | 3 | 30 | 6 |
| Non-Incapacitating Injury | 3 | 6 | 8 | 8 | 6 | 5 | 36 | 7.2 |
| Incapacitating Injury | 0 | 2 | 2 | 2 | 1 | 1 | 8 | 1.6 |
| Fatal | 0 | 2 | 3 | 1 | 0 | 0 | 6 | 1.2 |
| Southbound Total | 21 | 33 | 48 | 48 | 56 | 27 | 233 | 46.6 |

Table 25 shows the number of crashes by severity for the mountainous section. The data indicates the northbound and southbound roadways exhibit similar levels of severe crashes. The southbound roadway tends to have more fatal crashes within the mountainous section of the study area, with approximately twice the number of fatal crashes per year compared to the northbound roadway. However, the southbound roadway also

2.3 Conclusions

The following conclusions were presented in the 2017 updated preliminary traffic report:

1. The representative 2016 AADTs reported by ADOT's Transportation Planning website and the 2040 AADTs projected by ADOT for the study section of I-17 (MP 229-MP 262) are as follows:

| Location on I-17 Mainline | MP | 2016 7-Day AADT | 2040 7-Day AADT |
|-----------------------------------|-----------|--------------------|--------------------|
| Anthem Way to New River Rd | 229 – 232 | 45,900 | 58,944 |
| New River Rd to Black Canyon City | 232 – 244 | 41,600 | 56,505 |
| Black Canyon City to Sunset Point | 244 – 252 | 34,200 | 52,101 |
| Sunset Point to Cordes Jct. | 252 – 262 | 36,200 | 52,420 |

- 2. The following traffic behaviors were observed based on the 2016 traffic data collected at this ATR:
 - This study area experiences rural/recreational characteristics as opposed to typical urban characteristics. Instead of a weekday morning and late afternoon peak hour work-home commute traffic, the study area experiences weekend peak traffic. The average Saturday volumes are a factor of 1.2 larger than an average 7-day volume.
 - This study area experiences a large number of trips traveling away from the Phoenix metropolitan area at the beginning of the weekend on Friday and Saturday and returning to the area at the end of the weekend on Sunday.
 - This study area does not experience substantial seasonal changes. Many of the months exhibit relatively similar volumes on an average Saturday, except for the month of December, which is lower.
- 3. There was an average of approximately 365 crashes per year within the study area, based on 5 years of crash data.
- 4. There tends to be more crashes in the northbound direction as compared to the southbound direction.
- 5. The crashes in both the northbound and southbound directions tend to exhibit similar levels of severity.
- 6. Traveling northbound, the average number of crashes per mile tends to be higher in the mountainous terrain as compared to the level and rolling terrain.
- 7. Rear-end crashes are the predominant manner of collision on the northbound roadway in the mountainous area.
- 8. Single vehicle crashes are the predominant manner of collision on the southbound roadway in the mountainous area.
- 9. To maintain a LOS D in the study section, I-17 should be widened to three lanes in each direction, with an additional fourth lane in both directions south of Black Canyon City as well as climbing or flex lanes in the northbound direction in the mountainous segment between Black Canyon City and Sunset Point.
- 10. Based on the criteria established by AASHTO and a normal operating speed of 65 MPH, the northbound climbing lane should begin at approximately MP 244.44 and end at approximately 252.65.
- 11. The capacity analysis for the flex roadway indicates construction of a two-lane flex roadway would provide acceptable levels of service in the peak direction for the mainline lanes and the flex lanes. However, the northbound mainline lanes would operate at LOS F during the off-peak (Sunday) hours after the year 2026.

3.0 Design Concept Alternatives

Introduction 3.1

This section includes background information explaining why particular alternatives are being evaluated and what issues are driving development of the alternatives. This chapter is divided into several sections to discuss the various project elements:

- Anthem Way to Black Canyon City (MP 229.1 MP 244.5)
- Black Canyon City to Cordes Junction (MP 244.5 MP 262.0)
 - Alternatives Eliminated from Further Study
 - Long Term Alternatives
 - Near Term Alternatives
- **Evaluation Criteria** •
- **Evaluation Matrices**
- Recommended Alternatives

Anthem Way to Black Canyon City Alternatives 3.2

This segment of I-17 was included in the 2004 ADOT Project H5162 01L, which consisted of design concept development and long-range implementation strategies for the addition of general purpose and HOV lanes from SR 101L to the Black Canyon City TI. Four general purpose lanes and one HOV lane were recommended on I-17 between Anthem Way and New River Road; four general purpose lanes were recommended between New River Road and Black Canyon City.

The traffic volumes and projections developed in 2004 far exceed those developed for the current report. Based on current traffic projections, three travel lanes in each direction will be adequate until 2058 from Anthem Way to New River Road, and until 2038 from New River Road to Black Canyon City. Based on the current traffic projections, three travel lanes in each direction are recommended from the Anthem Way TI to the Black Canyon City TI.

The 2004 report considered inside, outside, and centered widening. Because that report considered a much wider typical section, the widening recommendations have been re-evaluated based on a three-lane typical section.

No Build Alternative

The No Build Alternative assumes that no major improvements would be made to I-17 from the Anthem Way TI to Black Canyon City. Under the No Build Alternative, traffic flow within the study area would continue to deteriorate due to increasing congestion. This congestion would intensify in future years from traffic growth generated by ongoing land development and urbanization. The No Build Alternative would not fulfill the purpose

Anthem Way TI to New River Road TI

This section of I-17 is considered fringe-urban as there are large, urban commercial, and residential developments near the Anthem Way TI. This three-mile segment of I-17 is similar to the five miles to the south (Carefree Highway to Anthem Way) in that the horizontal alignments are parallel, the speed limits are the same, and the areas are both fringe-urban. The five-mile section to the south was widened to three lanes in 2010 by sawcutting and widening the existing pavement on the median-side in both directions. In addition to widening the pavement in this area, half barrier was installed on the high (northbound) side since the remaining median width is 75 feet or less.

This segment of I-17 should match the typical section of the segment to the south by sawcutting and widening existing pavement on the median side, as well as adding half barrier along the northbound inside shoulder. An advantage to inside widening in this area is that there are two-way frontage roads along the outside of I-17 on both sides of the freeway; inside widening avoids the need to reconstruct the frontage roads. The median in this area is generally flat and should accommodate inside widening well, except for a segment starting 2,000 feet south of and continuing to the New River Road TI, where rock excavation is required. However, rock excavation would be required in this area regardless of inside or outside widening.

New River Road TI to Black Canyon City TI

North of the New River Road TI (MP 232), the northbound and southbound roadways diverge and follow different horizontal alignments and partially separate rights-of-way for approximately ten miles. The northbound and southbound horizontal alignments become parallel near the Rock Springs TI, at approximately MP 242.1. From this point north to Black Canyon City TI (MP 244.4), the alignments are parallel with a 76-foot median.

Physical features and widening constraints include rock slopes, the New River floodplain, existing bridges. utilities, and an adjacent frontage road/ramp. Because of these constraints and the rolling terrain from MP 232 to Black Canyon City, the widening is recommended to be a combination of inside and outside widening. Tables 26 and 27 detail the widening recommendations for the northbound and southbound roadways and note constraints for each section.

TABLE 26 – NORTHBOUND WIDENING RECOMMENDATIONS MP 232 – 245

| Start MP | End MP | Constraint | Recommen- dation | Comment |
|-------------|--------|-------------------------|---------------------|---|
| 232.0 | 233.0 | | Inside | Match widening to south |
| 233.0 | 233.5 | Local road | Inside | Avoid impacts to local road |
| 233.5 | 235.5 | Floodplain | Inside | Avoid impacts to floodplain |
| 235.5 | 236.5 | Table Mesa Tl | Inside | Avoid reconstruction of Table Mesa TI ramps |
| 236.5 | 237.2 | | Inside | Match widening to south |
| 237.2 | 240.4 | Rock | Inside | More removal necessary on outside |
| 240.4 | 241.8 | | Inside | Match widening to south |
| 241.8 | 242.5 | Rock Springs TI | Inside | Avoid reconstruction of Rock Springs TI ramps |
| 242.5 | 244.1 | Local road, ROW | Inside | Parallel alignments accommodate inside widening; existing Mud Springs bridge better accommodates inside widening |
| 244.1 | 245.0 | Black Canyon City TI | Inside | Avoid impacts to Black Canyon City TI ramps |

Inside widening is recommended along northbound I-17 between New River Road and Black Canyon City.

| TABLE 27 – SOUTHBOUND WIDENING RECOMMENDATIONS MP 232 – 245 |
|---|
|---|

| Start MP | End MP | Constraint | Recommendation | Comment |
|----------|--------|------------------------------|----------------|--|
| 232.0 | 232.5 | | Inside | Match widening to south |
| 232.5 | 235.5 | Rock | Inside | More removal necessary on outside |
| 235.5 | 236.5 | Table Mesa TI | Inside | Avoid reconstruction of Table Mesa TI ramps |
| 236.5 | 237.0 | Rock | Inside | More removal necessary on outside |
| 237.0 | 239.0 | Rock | Outside | More removal necessary on inside |
| 239.0 | 240.7 | Little Squaw Creek Bridge | Outside | New bridge constructed in 2010 accommodates outside widening |
| 240.7 | 242.5 | Rock Springs TI | Inside | Avoid reconstruction of Rock Springs TI ramps |
| 242.5 | 244.1 | ROW | Inside | Parallel alignments and 76' median accommodate inside widening; existing Mud Springs bridge better accommodates inside widening |
| 244.1 | 245.0 | Black Canyon City TI | Inside | Avoid reconstruction of Black Canyon City TI ramps |

A combination of inside and outside widening is recommended along southbound I-17 between New River Road and Black Canyon City. A new horizontal curve is used for the two transitions between inside and outside widening.

3.3 Black Canyon City to Junction SR 69 (Cordes Junction) Alternatives

This project (H6800 01L) began in 2006 with engineering studies extending from the Black Canyon City TI to Cordes Junction. In addition to the No Build alternative, nine "build" alternatives were developed and evaluated in the 2007 Alternative Selection Report for the project. The no build alternative considers that no improvements would be made to the existing facility.

In addition to the alternatives that were developed to satisfy the long-term needs of I-17, several near-term alternatives were developed more recently. The near-term alternatives are discussed later in this chapter.

The identification and evaluation of feasible improvement alternatives for the I-17 mainline, from the Black Canyon City TI to Jct. SR 69, has been conducted to accommodate projected traffic volumes for the 2040 design year. The development of these alternatives incorporated input from other agencies, such as BLM, the US Army Corps of Engineers (COE), Arizona Game & Fish Department (AGFD), Western Area Power Administration (Western), Central Yavapai Metropolitan Planning Organization, as well as the public. A number of issues, concerns, and opportunities surfaced during discussions. Some of the major concerns included rapidly increasing congestion, safe flow of traffic through the corridor, protection of natural and cultural resources, a possible bypass route that could be used by motorists to avoid crash locations that result in lengthy closures of I-17 between Black Canyon City and SR 69, future land use, impacts to communities, and local property values. This segment of I-17 also has numerous physical features and constraints that must be considered, including steep rock slopes, severe terrain, existing utilities, and existing bridges.

Table 28 lists all of the original alignment alternatives that were developed for this segment of I-17. These alternatives are illustrated in Figure 6.

TABLE 28 – ORIGINAL 2007 ALTERNATIVES

| | ALTERNA |
|---------|--|
| No Buil | d No improvements to existing I-17 roadways |
| А | Mainline widening |
| В | New east alignment from 0.5 mile south of the E |
| С | New east alignment from 0.5 mile north of the B |
| D | New middle alignment in the median, from 0.5 n Sunset Point TI |
| D-1 | New middle alignment with a series of tunnels, f of the Sunset Point TI |
| E | New middle alignment west of southbound I-17, of the Sunset Point TI |
| F | New west alignment from 0.5 mile north of the E |
| G | New west alignment from 0.5 mile north of the E |
| Н | New west alignment from 0.5 north of the Black |
| | |

TIVE DESCRIPTION

Black Canyon City TI to 1 mile south of the Sunset Point TI Black Canyon City TI to 1 mile south of the Sunset Point TI nile north of the Black Canyon City TI to 1 mile south of the from 0.5 mile north of Black Canyon City TI to 1 mile south , from 0.5 north of the Black Canyon City TI to 1 mile south Black Canyon City TI to 1 mile south of the Sunset Point TI Black Canyon City TI to the Badger Springs TI Canyon City TI to 1 mile south of the Bloody Basin TI



The evaluation criteria included design, environmental, and socioeconomic considerations that were developed during the agency and public involvement process. These criteria were used to determine the viability of the alternatives and evaluate the alternatives against the purpose and need of the project. The criteria used in the initial screening process included:

- Improve traffic operations •
- Improve incident management on Black Canyon Hill
- Constructability
- Earthwork/geotechnical
- Impacts to traffic during construction
- Estimated construction costs
- Structure and retaining wall construction
- Impacts to utilities and maintenance of facilities
- Maintain connectivity and access to crossroads
- Minimize environmental and socioeconomic impacts
- Minimize impacts to existing structures
- Minimize ROW acquisition
- Public comment

The assessment of alternatives also addressed factors such as land use and ownership, jurisdiction, water resources, biological impacts, visual resources, air quality, noise, hazardous materials, and cultural resources.

3.3.1 Alternatives Considered but Eliminated from Further Study – Long-term Solutions

As documented in the Alternative Selection Report, the alternatives discussed in this section were evaluated and eliminated from further consideration. The alternatives were originally developed to satisfy higher projected levels of population and employment growth and correspondingly higher projected traffic volumes; the descriptions that follow have been updated to reflect the current recommended number of lanes.

Alternative A, Mainline Widening

Alternative A consists of widening the existing northbound and southbound alignments from MP 244.5 to MP 262. This alignment would consist of adding one lane and additional shoulder width in both directions. A climbing lane would be added in the northbound direction from MP 244.65 to 250.40.

This alternative would consist of a combination of widening to the inside and outside of the existing roadways. Modifications to the existing horizontal geometry would be incorporated with the widening construction. The existing horizontal and stopping sight distance would be increased by cutting back slopes at key locations and flattening the sharp curves. There are also a number of existing curves where the superelevation does not meet current design criteria. The existing pavement would be reconstructed where it does not meet current criteria. This alternative would not change the existing maximum grades of 6% and design exceptions would be required.

Maintaining traffic during construction to improve the existing roadways would be a difficult and expensive undertaking. Construction would be very disruptive to existing I-17 traffic and prolonged because of high existing traffic volumes and because there is no alternate route to carry traffic during construction. In addition, earthwork operations, including blasting and mitigation of rockfall hazards, would require complete closures of both lanes in at least one direction and possibly both directions depending on the proximity of the traffic to construction activity.



Alternative A was eliminated from further consideration as a standalone alternative because:

- Traffic must be maintained during construction. No alternate route would be available during construction along the six-mile segment of I-17 on the Black Canyon Hill as part of this proposed alternative. Therefore, construction at this location would be expensive and difficult and the duration lengthy due to heavy existing high-speed traffic.
- lanes in one direction.
- Grades exceed the maximum 5% in mountainous terrain allowable by AASHTO and ADOT's Roadway Design Guidelines for a rural highway from MP 244.5 to 250.5.
- Widening of the northbound roadway could possibly impact the Agua Fria National Monument. Four mining claims would also be affected.

Alternative B. New East Alignment

In this alternative, a new alignment east of the existing I-17 corridor would be constructed. This alignment would consist of three lanes in both directions with a possible climbing lane in areas of sustained uphill grade. It would depart from the existing highway 0.5 mile south of the Black Canyon TI, near the Agua Fria River Bridge. The alignment would travel along a canyon within the AFNM to the top of Black Mesa. Several large structures may be required for the alignment to cross from one side of the canyon to the other. Once at the top of Black Mesa, the alignment would parallel the existing I-17 corridor for 1.5 mile until it ties back into the existing highway one mile south of the Sunset Point TI. Once the alignment ties back in with the existing I-17 alignment, the alternative would consist of widening the existing northbound and southbound alignments north to the project limit.

The proposed roadway profile would have a sustained grade of 5% for approximately 4.5 miles. Landings or interruptions of the maximum sustained grade could be provided by additional earthwork or by allowing a steeper grade. At the top of Black Mesa, the grade would be relatively level until it ties back in with existing I-17.

Bumble Bee Road could be connected to the new alignment by constructing a new TI east of existing I-17 on the mesa. This would be accomplished with a two-mile long crossroad that would cross west from the new alignment down a steep canyon to connect to the existing Bumble Bee Road.

This alternative was eliminated from further consideration because:

- The area near the Black Canyon City TI proposed for the new alignment has various residential and commercial developments. This alternative would require the displacement of approximately 50 single family residences, 6 apartment buildings, and other outbuildings.
- The new alignment would be located on private land and within the Agua Fria National Monument. A large amount of ROW acquisition would be required.
- hazards in areas with high slopes.
- Roadway foundation conditions are poor to fair, with a moderate potential for expansive soils in the southern portion of the alignment.
- There is a high impact probability to wildlife and wildlife habitat. The new alignment would fragment pronghorn habitat and fawning areas, have potential impacts to riparian habitat where major drainages are crossed, and potentially encroach on the Agua Fria River floodplain.
- The new alignment is not consistent with the BLM Resource Management Plan. There would be direct impacts to the Agua Fria National Monument. It would impact recreational experiences by severing existing trails and highly affecting visual quality.

Blasting and rockfall mitigation in close proximity to existing I-17 would require complete closures of both

• It would require extensive earthwork and there is a moderate to high risk of slope instability and rockfall

- AFNM cultural resources would be highly impacted.
- Constructing a crossroad to connect Bumble Bee road to the new alignment would require steep grades and extensive earthwork.
- It had low public and agency support.

Alternative C, New East Alignment

Alternative C also proposed a new alignment east of the existing I-17 corridor. This alignment would consist of three lanes in both directions with a possible climbing lane in areas of sustained uphill grade. It would begin 0.5 miles north of the Black Canyon City TI and proceed northeast, east of existing I-17. The new alignment would climb steep canyons within the AFNM to the top of Black Mesa. The corridor would then parallel existing I-17 for approximately one mile until it ties back into the existing I-17 alignment south of the Sunset Point TI. Once the alignment ties back in with the existing I-17 alignment, the alternative would consist of widening the existing northbound and southbound alignments north to the project limits.

The proposed profile would have an initial sustained grade of 10% for several miles north of Black Canyon City because the alternative must rapidly ascend the face of the Black Mesa. At the top of Black Mesa, the roadway grade would be relatively flat until it ties back in with the existing I-17 roadways south of Sunset Point TI.

Bumble Bee Road could be connected to the new alignment by constructing a new TI east of existing I-17 on Black Mesa. This would be accomplished with a two-mile long crossroad that would cross west from the new alignment down a steep canyon to connect to the existing Bumble Bee Road.

This alternative was eliminated from further consideration because:

- The 10% grade would exceed the maximum grade allowed by AASHTO and ADOT's RDG, which is 5% maximum in mountainous terrain.
- The new alignment would be located on private land and within the Agua Fria National Monument. A large amount of ROW acquisition would be required.
- It would require extensive earthwork and there is a moderate to high risk of slope instability and rockfall hazards in areas with high slopes.
- Roadway foundation conditions are poor to fair, with a moderate potential for expansive soils in southern portion of alignment.
- There is a high impact probability to wildlife and wildlife habitat. The new alignment would fragment pronghorn habitat and fawning areas, have potential impacts to riparian habitat where major drainages are crossed, and potentially encroach on the Agua Fria floodplain.
- The new alignment is not consistent with the BLM Resource Management Plan. There would be direct impacts to the Agua Fria National Monument. It would impact recreational experiences by severing existing trails and highly affecting visual quality.
- AFNM cultural resources would be highly impacted.
- Constructing a crossroad to connect Bumble Bee road to the new alignment would require steep grades and • extensive earthwork.
- The alternative would affect one mining claim and two grazing allotments.
- It has low public and agency support.

Alternative D-1, New Middle Alignment

Alternative D-1 consists of a new roadway alignment to be developed near the existing highway. The alternative would provide three lanes in both directions with a possible climbing lane in areas of sustained uphill grade. The new alignment would begin 0.5 mile north of the Black Canyon City TI. It would proceed north, utilizing the ROW between the existing northbound and southbound I-17 roadways and by using a series of tunnels to navigate the mountainous terrain. Using tunnels would result in a simple horizontal alignment with grades between 1% and 5%.

At its south end, the alignment would begin parallel to the existing northbound I-17 alignment. It would then cross over the existing southbound I-17 alignment and continue along its west side. The first tunnels would be constructed just south of the existing Bumble Bee TI; these tunnels would be just over a mile in length. The new alignment would tunnel under the existing southbound I-17 roadway once and existing northbound I-17 roadway twice, as well as under existing Bumble Bee Road. The parallel tunnels would daylight just north of existing Bumble Bee Road and the alignment would be aboveground for approximately one mile before entering another tunnel. The final series of mile-long tunnels would surface at the top of Black Mesa. From here, the alignment would tie back into the existing highway just south of the Sunset Point TI. Once the alignment ties back in with the existing I-17 alignment, the alternative would consist of widening the existing northbound and southbound alignments north to the project limits.

A new TI approximately 2000 feet north of the existing Bumble Bee TI could be constructed to connect the new alignment to Bumble Bee Road.

This alternative was eliminated from further consideration because:

- Preliminary geotechnical analysis has determined that the soil conditions in the area are unfavorable for tunnel construction. There is also a high risk of slope instability and rockfall hazards in areas with high slopes.
- Constructability would be difficult, earthwork would be extensive, and tunnel costs would be prohibitively high, estimates for tunnel construction could range from \$50,000 to \$70,000 per linear foot of tunnel (2007 estimate).
- Construction would be disruptive to existing I-17 traffic. Blasting and rockfall mitigation in close proximity to I-17 may require complete closures of both lanes in one direction.
- Hazardous cargo may not be permitted to pass through tunnels. Therefore, one of the existing I-17 roadways would need to be retained or another acceptable route be established for hazardous cargo transport.
- There would be medium impacts to existing utilities.
- Four mining claims would be affected.

Alternative F, New West Alignment

In this alternative, a new alignment west of the existing I-17 corridor would be constructed. This alternative would provide three lanes in both directions with a possible climbing lane in areas of sustained uphill grade. It would begin 0.5 miles north of the Black Canyon City TI, cross over the existing southbound I-17 alignment, and continue in a north to northwest direction. The new alignment would follow alongside the existing Maggie Mine Road and Crown King Road (Old Route 69) alignments. It would then travel east up the face of Black Mesa toward the existing I-17 roadway and would connect back to the existing I-17 alignment one mile south of the Sunset Point TI. Once the alignment ties back in with the existing I-17 alignment, the alternative would consist of widening the existing northbound and southbound alignments north to the project limits.

The southern segment for this alternative consists of borderline mountainous and rolling terrain. The climb to the top of Black Mesa would consist of a 5% grade followed by a 10% grade to traverse the steep face of Black I-17, ANTHEM WAY T.I. TO JCT, SR 69

Mesa without extensive cuts. At the top of Black Mesa, the profile grade would be relatively flat to its tie-in with the existing I-17 profile.

This alternative was eliminated from further consideration because:

- The 10% grade for 1.2 miles would exceed the maximum grade allowed by AASHTO and ADOT's RDG, which is 5% maximum in mountainous terrain.
- ROW acquisition requirements are medium to high.
- It would require extensive earthwork and there is a moderate to high risk of slope instability and rockfall hazards in areas with high slopes.
- There is a high impact probability to wildlife and wildlife habitat.
- The new alignment is not consistent with the BLM Resource Management Plan. It would impact recreational experiences by severing existing trails and highly impacting visual quality.
- There would be medium to high impacts to existing utilities and 17 mining claims would be affected.

Alternative G, New West Alignment

Alternative G also would construct a new alignment west of the existing I-17 corridor. This alternative would provide three lanes in both directions with a possible climbing lane in areas of sustained uphill grade. It would begin 0.5 miles north of the Black Canyon City TI and follow the same alignment as Alternative F south of the existing Bumble Bee TI. North of Bumble Bee Road. Alternative G would closely follow the existing Crown King Road alignment, passing just east of Bumble Bee Ranch. By staying along the bottom and the side of Black Canyon and crossing the entrance of Alkali canyon, this new alignment would climb gradually and connect with existing I-17 near the Badger Springs Road TI. Once the alignment ties back in with the existing I-17 alignment, the alternative would consist of widening the existing northbound and southbound alignments north to the project limits.

The southern segment for this alternative would cross borderline mountainous and rolling terrain of approximately 1% to 5% grade. The alignment would then ascend at a 5% grade for several miles. Due to the skew of the roadway up the side of Black Canyon and crossing the entrance of Alkali Canyon as it ascends to Badger Springs Road, several sections of deep cut and long fill slopes are anticipated.

This alternative was eliminated from further consideration because:

- A large amount of ROW acquisition would be required.
- There is a high impact probability to wildlife and wildlife habitat. With eleven stream crossings, it has the potential to impact riparian habitat as well as the AGFD's northern wildlife water catchment.
- The new alignment is not consistent with the BLM Resource Management Plan. It would impact recreational experiences by severing existing trails and impacting visual quality.
- There will be medium to high impacts to existing utilities.
- Seventeen mining claims and four BLM grazing allotments would be affected.
- Because of the elevation difference, access to the Sunset Point TI and rest area may not be possible.
- Terrain would make the connection back into I-17 north difficult. •

Alternative H, New Far West Alignment

Alternative H consists of a new alignment beginning approximately one mile north of the Black Canyon City TI and ending at approximately one mile south of the Bloody Basin TI. Three lanes would be provided in both directions; a climbing lane would be considered in areas of sustained uphill grades. The current Alternative H

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alignment was modified from the original version presented to the public in 2007. The revised alignment avoids more of the riparian area and bypasses locations that were identified as being environmentally sensitive during the data collection and technical studies phase of this study.

The southern segment of the Alternative H alignment would be similar to Alternative E. The new alignment would proceed northward until passing Maggie Mine to the east, then would begin to turn in a northwesterly direction across the valley to the opposing hillside. The new alignment would proceed westward and cross over Arrastre Creek. The alignment would pass to the east of Gillespie Mine, pass between two other mines, and then turn northward along the western face of Black Canyon. A range of hills would separate the new alignment from the existing I-17 alignments. Alternative H would run parallel to the existing Crown King Road along the west, crossing over Crown King Road several times to accommodate the terrain.

As Alternative H approaches the valley floor south of Bumble Bee Ranch, the alignment would turn to the east over Sheep Gulch. The alignment would then continue its course north on the hillside of Black Mesa for three miles, maintaining distance from the floodplain, as well as creating a physical nature barrier between the roadway and a view from the valley floor. The alignment would bridge over Alkali Canyon and resume its climb up the hillside to reach the top of Black Mesa and connect with existing I-17 south of the Bloody Basin Road TI. Once the alignment connects to existing I-17, the alternative would widen the existing northbound and southbound roadways north to the project limit.

The profile for Alternative H from the south would consist of an upgrade of 5% for the first mile, then level out for the next half mile. As the alignment crosses to the opposing hillside, it would climb at a grade of 4.5% for approximately 1.5 mile. The profile over the next eight miles ranges from a downgrade of 1.5% to an upgrade of 3.8%. Where the roadway travels up the hillside to reach the top of the mesa, the grades would increase to 5% for approximately three miles.

New structures would bridge rough terrain or span locations where fills are greater than 60 feet.

Because Alternative H is west of and much lower in elevation than the existing I-17, it would not provide access to the Sunset Point TI or rest area or the Badger Springs TI.

Although it was recommended for further study in the Alternative Selection Report, this alternative has since been eliminated from further consideration because:

- A large amount of new right-of-way would be required.
- The new alignment would not be consistent with the BLM's recently amended Resource Management Plan transportation/utility corridor.
- Eleven mining claims and four BLM grazing allotments would be affected.
- Foraging yellow-billed cuckoos, a US Fish and Wildlife threatened species, would potentially be impacted • where the new alignment parallels riparian habitat along Black Canyon and Bumble Bee creeks.
- Alternative H would have an adverse effect on three historic properties recommended or determined eligible of 1966, which protects historic properties of federal, state, or local significance.
- The new alignment of Alternative H would not provide access to Bumble Bee Road, the Sunset Point TI, the Sunset Point Rest Area, or the Badger Springs TI.
- Alternative H received low public and agency support.

because it would not conform to BLM's recreation management and visual quality objectives. In addition, approximately 50 percent of the alignment would be located outside BLM's designated multi-use

for listing in the National Register of Historic Places that would be avoided by Alternatives D and E. Thus, Alternative H would not comply with the requirements of Section 4(f) of the Department of Transportation Act

3.3.2 Alternatives Recommended for Further Study – Long-term Solutions

The alternatives discussed below were originally defined in the Alternative Selection Report. Based on favorable preliminary evaluations, they were developed further.

No Build Alternative

The No Build Alternative assumes that no major improvements would be made to I-17 from the Black Canyon City TI to Cordes Junction. Under the No Build Alternative, traffic flow within the study area would continue to deteriorate due to increasing congestion. This congestion would intensify in future years from traffic growth generated by ongoing land development and urbanization. The No Build Alternative would not fulfill the purpose of the project of reducing traffic congestion and improving the capacity and traffic operational characteristics of the route for regional traffic.

Alternative D

As in the other alternatives, Alternative D would extend the three-lane section in each direction (with revised traffic projections) recommended by the DCR to the south of the Black Canyon City TI. Alternative D consists of a new alignment constructed primarily in the median area between the existing northbound and southbound roadways where topography and spacing permit. The alternative alignment begins approximately 0.5 mile north of the Black Canyon City TI and ends approximately one mile south of the Sunset Point TI. Once the alignment ties back in with the existing I-17 alignment near Sunset Point, the alternative would consist of widening the existing northbound and southbound roadways north to the project limit. Four lanes would be provided in the northbound direction on the existing roadways by using the two existing northbound lanes and converting the two southbound lanes into northbound lanes and three lanes provided in the southbound direction on a new alignment from Black Canyon City to Sunset Point Rest Area. North of Sunset Point, three lanes would be provided in both directions.

South of the existing Bumble Bee TI, the new alignment would cross over the existing southbound alignment and Bumble Bee Road. From there, the new alignment would follow along the west side of the existing northbound alignment within the existing median and tie back in to the existing southbound roadway south of the Sunset Point TI. From this point to the northern project limit, the existing roadways would be widened to three lanes.

The vertical profile for the new alignment would consist of 4% to 5% grades to the top of Black Mesa. Once at the top of Black Mesa, the grade would be relatively level as the highway follows the terrain to connect with the existing I-17 profile.

Five new structures would be required for this alternative. Two structures would be necessary to cross over southbound I-17. Another bridge would be located at the existing Bumble Bee TI over the existing crossroad. The remaining locations would bridge rough terrain, deep valleys, and an existing underground gas line. Bridges spanning deep valleys that do not have elements such as utilities, roadways, or significant water crossings have been minimized to reduce cost due to the expected availability of large amounts of suitable fill material within the project limits. Bridge structures would range from 250 feet to 590 feet in length. In addition, the two existing overpass structures at the Sunset Point TI are recommended for widening and the existing overpass structures at Badger Springs TI and Bloody Basin TI should be replaced to accommodate the roadway widening. The existing Bumble Bee TI structures are not impacted by this alternative.

Conversion of the existing southbound I-17 roadway to allow northbound traffic to use it would require removing the existing ramps at the Bumble Bee TI, removing and replacing existing signs and protection devices, and correcting adverse crown.

<u>Alternative D Connection to Bumble Bee Road:</u> Alternative D crosses well above Bumble Bee Road because of topography and required bridge clearance over I-17. The horizontal alignment for Alternative D is between and close to both the existing northbound and southbound roadways at Bumble Bee Road. The close proximity to the existing roadways does not provide adequate space for new ramp connections to Bumble Bee Road. The new ramps would have very steep grades, ranging from 9% to 18%, which far exceed allowable ramp grades per the RDG.

The steep ramp grades eliminated southbound access options to Bumble Bee for Alternative D. However, Alternative D would provide northbound and southbound access to the Black Canyon City TI and the Sunset Point Rest Area and TI.

Alternative E

Alternative E consists of a new alignment generally to the west of the existing southbound I-17 roadway, beginning approximately 0.5 mile north of the Black Canyon City TI and ending approximately one mile south of the Sunset Point TI. Four lanes would be provided in the northbound direction on the existing roadways and three lanes would be provided in the southbound direction on a new alignment from Black Canyon City to Sunset Point. North of Sunset Point, three lanes would be provided in both directions north to Cordes Junction. Widening would consist of adding lanes to the inside of the existing roadways, the outside, or a combination of both.

At the south end of the project, the new alignment follows the existing southbound alignment. The new roadway would turn westward to cross over Arrastre Creek. Proceeding north, Alternative E would cross over a realigned section of Bumble Bee Road west of the existing TI. The new alignment stays west of and roughly parallel to the existing southbound roadway from Bumble Bee Road north to its tie-in at Sunset Point.

The vertical profile for Alternative E would consist of grades ranging from 0.5% to 5% from Black Canyon City to the top of Black Mesa. Once at the top of Black Mesa, grades would be relatively flat as Alternative E follows the terrain until it ties back in with the existing I-17 roadways.

Alternative E would require a total of six new structures, ranging from 140 feet to 1460 feet in length. The structures would bridge rough terrain, deep valleys, and existing underground gas and fiber optic lines. Bridges spanning deep valleys that do not have elements such as utilities, roadways, or substantial water crossings were minimized to reduce cost because of the expected availability of large amounts of suitable fill material within the project limits. One mainline structure and one ramp structure would be necessary to cross above the realigned segment of the Bumble Bee crossroad west of the existing traffic interchange.

Two existing overpass structures at the Sunset Point TI would be widened and the existing overpass structures at Badger Springs TI and Bloody Basin would be replaced to accommodate the roadway widening. The existing Bumble Bee TI structures are not impacted by this alternative.

<u>Alternative E Connection of Southbound I-17 to Bumble Bee Road:</u> Reasonable ramp horizontal alignments and grades can be provided with Alternative E.

Two TI configurations were considered to find a good solution to connect southbound I-17 to Bumble Bee Road with an acceptable exit ramp grade and length: a Loop Alternative and a Half Diamond (western half) Alternative. The loop configuration was rejected because it potentially could be confusing to drivers and encourage wrong-way movements. In addition, the loop configuration is not consistent with driver expectancy for the rest of the traffic interchanges in the corridor and it requires additional right-of-way.

The diamond alternative would require a new connector road to access existing Bumble Bee Road. The location of the TI allows a flatter grade on the southbound exit ramp. The initial grade for the southbound exit ramp would

be 5%, then reduced to 1% for the last 800 feet of the ramp. The entrance ramp has an upgrade of 3.3% before matching the mainline downgrade of 1.5%. A parallel entrance ramp is recommended to allow trucks to gain speed before merging into the main flow of traffic.

While more complicated to construct with two added structures and road connector, the diamond TI was recommended as the more desirable configuration.

Figures 7 and 8 below illustrate the connections from Alternatives D and E to existing I-17 near Black Canyon City ('South End') and Sunset Point ('North End').





FIGURE 8 – ALTERNATIVE E CONNECTION LAYOUTS AT SOUTH AND NORTH TERMINI



SOUTH END

3.3.3 Alternatives Considered but Eliminated from Further Study – Near-term Solutions

The alternatives with new roadways on new alignments are costly to construct. Because of limited funding availability, less expensive, nearer-term alternatives were developed that may not satisfy the traffic capacity needs in the design year 2040 but would improve current operations at a lower cost than the long-term alternatives on new alignment.

One- and two-lane flex lane alternatives were developed. The one-lane flex lane alternative has been eliminated from further consideration.

Flex Roadway - One Lane

Flex traffic lanes add peak-direction capacity to a two-way facility and decrease congestion by providing additional lane capacity for the peak direction. This alternative would retain the two southbound lanes on the existing southbound roadway and the two northbound lanes on the existing northbound roadway and add a barrier-separated one-lane flex roadway alongside the southbound lanes between Black Canyon City and Sunset Point.



NORTH END



I-17 Typical Section Flex Lane Alternative

To add the flex lane adjacent to the southbound lanes, a 42" concrete barrier would be added next to the inside shoulder with a two-foot shy distance on both sides. A new twelve-foot lane with eight-foot shoulders would carry northbound traffic during peak northbound hours (e.g., Friday and Saturday) and would carry southbound traffic during peak southbound hours (e.g., Sunday and holiday weekends). The traffic direction could be changed if needed due to crashes or maintenance.

Signing will be required to direct both directions of traffic. Breakaway posts will need to accommodate bidirectional traffic. Guardrail ends and attenuators will be fitted for approaches in both directions.

Because the flex lane would be barrier separated from the southbound lanes for the length of the Black Canyon Hill, no access to or from the Bumble Bee TI would be possible for traffic on the flex lane. Southbound traffic entering I-17 from the Sunset Point TI would not be able to access the flex lane because of limited distance between the Sunset Point TI entrance ramp and the top of the downgrade. A short section of temporary or moveable concrete barrier could be included to provide emergency access for this traffic. Several emergency access gates should be included for use by first responders.

The flex lane would connect to the existing northbound and southbound roadways near Black Canyon City and Sunset Point via slip ramps meeting ADOT design criteria for entrance and exit ramps. Dynamic message signs in advance of the flex lane entries would be added south of Black Canyon City (northbound) and north of Sunset Point (southbound) to alert drivers to the status of the flex lane.

Entry to the flex lane would be controlled by gates or a moveable barrier system. The series of gates at the entry points would be designed to prevent cars from going the wrong way. If a recent Florida project were used as an example, the initial gates should be well marked, with large, orange "Do Not Enter" signs suspended from the arm before a final steel arm. Even if a driver were to ignore the digital signs preceding the gates and crash through several of them, the final steel arm would prevent the driver from entering the flex lanes going in the wrong direction. Should the computer system fail, the gates would remain locked down in whatever position they were in last to prevent head-on collisions.

A sweep by operations personnel or a check of cameras would be required prior to switching the direction of traffic in the flex lanes.

This alternative would require approximately 1.5 acres of new ROW associated with two areas of rock cut slopes and associated access to the top of the cuts. An additional 2.8 acres of new drainage easement is required for improvements near MP 251.

This alternative was eliminated from further consideration because:

- The additional costs to create a flex two-lane facility are relatively nominal compared to the benefits of having two travel lanes.
- ADOT District staff indicated that having two lanes for northbound traffic is strongly preferred for future traffic control when northbound construction occurs on the Black Canyon Hill.

3.3.4 Alternatives Recommended for Further Study – Near-term Solutions

Because of limited funding availability, less expensive nearer-term alternatives were developed that focus on improving capacity and incident management options on the Black Canyon Hill between Black Canyon City and Sunset Point (MP 245-252). Three build alternatives were considered:

- Northbound climbing lane
- Two-lane flex roadway
- Part-time shoulder lane

Northbound Climbing Lane

This alternative would retain the two southbound lanes on the existing southbound roadway and add a northbound climbing lane to the existing two-lane northbound roadway.

The climbing lane would be twelve feet wide. Inside and outside shoulder widths desirably would be increased to twelve feet (per RDG Table 302.4); however, the minimum inside shoulder width is four feet and the minimum outside shoulder width is ten feet for a climbing lane. A design exception would be required from FHWA for a four-foot inside shoulder where the third lane (climbing lane) would be provided.



Operationally, the climbing lane would provide additional northbound capacity in the direction of slow-moving vehicles and trucks. It would provide flexibility and extra width for traffic to travel around partial closures; however, it would not provide additional southbound capacity or incident management flexibility for full closures. Access to and from the existing TIs would not change.

The proposed northbound climbing lane between Black Canyon City and Sunset Point would require widening of the northbound roadway from two to three lanes at the Bumble Bee TI. Since the Bumble Bee TI OP NB is considered "Functionally Obsolete" with a 15'-0" vertical clearance, bridge replacement is recommended over widening. ADOT is currently leading the design for this bridge. Construction funding is in ADOT's five-year plan in fiscal year 2020.

| Varies | Exst R/W |
|---|----------|
| WIDENING 22' TO EXISTING INSIDE 38' ROADWAY | |
| 12'' 12' 12' 12'' Shidr Lane Lane Shidr | |
| | |
| FARTHWORK | |
This alternative would require approximately three acres of new ROW.

Flex Roadway - Two Lanes

This alternative resembles the one-lane flex roadway alternative detailed in Section 3.3.3. It would retain the two southbound lanes on the existing southbound roadway and the two northbound lanes on the existing northbound roadway and add a barrier-separated two-lane reversible roadway alongside the southbound lanes between Black Canyon City and Sunset Point.



To add the flex lanes adjacent to the southbound lanes, a 42-inch concrete barrier would be added next to the inside shoulder. A glare screen on the concrete barrier should be considered as it may be helpful to drivers when the flex lanes are being used in the northbound direction. Two new twelve-foot lanes with a four-foot inside shoulder and a ten-foot outside shoulder would carry northbound traffic during peak northbound hours (e.g., Friday and Saturday) and would carry southbound traffic during peak southbound hours (e.g., Sunday and holiday weekends). The traffic direction could be changed if needed due to crashes or maintenance.

Operational features, access constraints, and entry into the flex lanes would be the same as described for the one-lane flex alternative.

This alternative would require approximately 1.8 acres of new ROW associated with two areas of rock cut slopes and associated access to the top of the cuts. An additional 2.8 acres of new drainage easement is required for improvements near MP 251.

Part-Time Shoulder Lane

Part-time shoulder use is a transportation system management and operation strategy that allows use of the left or right shoulder as a travel lane during some, but not all, hours of the day and days of the week. This section is a summary of a project memo entitled "Part-Time Shoulder Use Feasibility."

The I-17 traffic volumes fluctuate by day of week and are particularly influenced by rural/recreational traffic. I-17 traffic has a unique characteristic where the Friday, Saturday, and Sunday traffic volumes consistently exceed Monday through Thursday traffic. Furthermore, it is Friday afternoons, Saturday mornings, and Sunday afternoons that are the heaviest, again corresponding to the public traveling to or from recreational destinations.

Part-time shoulder operations in other states have varied, including dynamically opening shoulders when certain congestion thresholds are reached or statically opening shoulders during specified historical peak periods. Dynamic shoulder use is defined as regular or constant monitoring of the corridor and opening the shoulders for

use based on traffic demand. Static shoulder use is defined as opening the shoulder only on given days and hours that are consistent week-to-week, typically based on historical traffic volumes.

Because of the regular and predictable congestion cycles on the I-17 Black Canyon Hill, a static part-time shoulder would be recommended. The regular schedule could be adjusted during certain holidays (Memorial Day, Independence Day, Labor Day) by extending hours and/or days of operation. These adjustments could be made with temporary variable message signs and media coverage.

Part-time shoulder use operations may use the left or right shoulder, depending on several considerations, including driver expectations, striping and operations at traffic interchanges, truck operations, and available lane and shoulder widths.

The primary disadvantage of a right-side shoulder is that slow moving vehicles (trucks and RVs) would use it since it would be the right-most travel lane during peak periods. Without roadway widening, the part-time shoulder lane would be narrow (11-foot lane and 1-foot shoulder) to minimize roadway widening and earthwork costs. If trucks and RVs did not use the right-side part-time shoulder, cars would pass trucks on the right side, which is undesirable. The primary advantage of the right-side shoulder is that the right shoulder would be used for disabled vehicles when closed to through traffic, which is common and is expected by drivers. Because of the heavy truck volumes on I-17, particularly slow-moving truck traffic traveling northbound up steep grades, a left-side part-time shoulder, both northbound and southbound, would be recommended. With this recommendation, clear and descriptive signing advising off-peak drivers to move crashes and broken-down vehicles to the left shoulder will be particularly important.

Given the constrained roadway geometry and high construction costs associated with widening I-17 in this corridor, minimum lane and shoulder widths are recommended to implement the part-time shoulders. These dimensions are compatible with the existing 38-foot northbound and southbound roadway widths.

Left Shoulder (inside): 1' – a striped shoulder is recommended to give shy distance to guardrail during shoulder use. All travel lanes: 11' – FHWA requirement.

Right shoulder: 4' – FHWA requirement.

The widths listed above are absolute minimums and would require exception approval from FHWA. Northbound commercial trucks are currently confined to the right lane on the Black Canyon Hill; heavy trucks should be restricted from using the part-time shoulder lane because of the narrow shoulder.

Any surplus roadway width throughout the corridor should be utilized as lane width, particularly for the right travel lane utilized by commercial trucks. The typical section shown below illustrates the proposed left-side shoulder opened for peak period operations, as well as normal operations with the left shoulder closed to traffic.







Refuge areas for disabled vehicles should be located approximately every half-mile along a facility with static or dynamic shoulder use. The refuge area should be long enough to enable a tow truck to park and load a brokendown vehicle. The availability of space in this corridor to provide any refuge areas is limited by terrain. Building refuge areas to supplement the part-time shoulder lane may require rock excavation in places and new, large embankments and fill slopes in other areas. There are flat areas available along the right side of I-17 northbound approximately every half mile. However, none of the available flat areas along I-17 northbound or southbound can accommodate refuge areas of the recommended size; earthwork operations would be required to construct pullouts along I-17.

3.4 Evaluation of Alternatives

3.4.1 Evaluation Criteria

Criteria used to evaluate the potential impacts of widening between Anthem Way and Black Canyon City include connectivity at ramps, ROW acquisition, and any other major differentiators that could impact construction cost.

Criteria used to evaluate the potential impacts of the Black Canyon City to Cordes Junction long-term and nearterm alternatives include traffic operations, access to traffic interchanges, ROW acquisition, and estimated construction cost.

3.5 Evaluation – Anthem Way to Black Canyon City Near-Term Alternatives

The No Build Alternative and Inside, Outside, and Centered Widening Alternatives evaluated against these criteria. The criteria were weighted equally.

The results of the evaluation are summarized in Table 29. The alternatives with the most favorable characteristics for each criterion are identified in the 'Advantage' column. If more than one alternative was determined to have similar favorable characteristics, the alternatives are listed with an 'or' to indicate that they rank equally for that criterion. If the No Build alternative was ranked highest for a certain criterion, the most favorable build alternative(s) was also listed because the No Build alternative does not satisfy the purpose and need for the project. Regardless of its ranking, the No Build Alternative will be carried through the NEPA process.

3.6 Evaluation – Black Canyon City to Cordes Junction, Long-Term Alternatives

The No Build Alternative and Alternatives D and E were evaluated against these criteria. The criteria were weighted equally.

The results of the evaluation are summarized in Table 30. The alternatives with the most favorable characteristics for each criterion are identified in the 'Advantage' column. If more than one alternative was determined to have similar favorable characteristics, the alternatives are listed with an 'or' to indicate that they rank equally for that criterion. If the No Build alternative was ranked highest for a certain criterion, the most favorable build alternative(s) was also listed because the No Build alternative does not satisfy the purpose and need for the project. Regardless of its ranking, the No Build Alternative will be carried through the NEPA process.

3.7 Evaluation – Black Canyon City to Cordes Junction, Near-Term Alternatives

The No Build Alternative and the climbing, flex lane, and part-time shoulder lane alternatives were evaluated against similar criteria. The criteria were weighted equally.

The results of the evaluation are summarized in Table 31. The alternatives with the most favorable characteristics for each criterion are identified in the 'Advantage' column. If more than one alternative was determined to have similar favorable characteristics, the alternatives are listed with an 'or' to indicate that they rank equally for that criterion. If the No Build alternative was ranked highest for a certain criterion, the most favorable build alternative(s) was also listed because the No Build alternative does not satisfy the purpose and need for the project. Regardless of its ranking, the No Build Alternative will be carried through the NEPA process.

| Criterion | No Build Alternative | Inside Widening | Outside Widening | Centered Widening | Advantage |
|---|------------------------------------|--|--|---|---|
| Lane Designation Legend ↓ = Existing lane direction of travel ↓ = Proposed lane direction of travel | ↓↓ ↑↑ | ↓↓↓ ↑↑↑ | ↓↓↓ ↑↑↑ | ↓↓↓ ↑↑↑ | |
| Typical Section | No change to existing roadways. | Existing 10-ft outside shoulders to remain. Existing 12-ft travel lanes to remain. Existing 4-ft inside shoulders removed. Add one 12-ft travel lane in each direction on inside. Add one 10-ft inside shoulder in each direction. | Existing 10-ft outside shoulders removed. Existing 12-ft travel lanes to remain. Widen 4-ft existing inside shoulders to 10 feet. Add one 12-ft travel lane in each direction on outside. | Remove part of existing shoulders. Existing 12-ft travel lanes to remain. Widen 4-ft existing inside shoulders to 10 feet. Add one 12-ft travel lane in each direction centered. | |
| Connectivity at Ramps | No change to existing connections. | No change to existing connections. | Changes to ramps required. | Changes to ramps required. | No Build, Inside |
| | | Anthem to New River Parallel alignments accommodate future inside widening. Aligns with lanes south of Anthem. Barrier required as median width is less than 75 feet. <u>New River to Table Mesa</u> Northbound : Fits within right-of-way. Southbound : Requires less earthwork. | Anthem to New River Frontage roads conflict with outside widening. <u>New River to Table Mesa</u> Northbound : New River floodplain conflicts with outside widening. Right- of-way impacts likely. Southbound : Requires more earthwork. | Anthem to New River Frontage roads conflict with centered widening. Barrier required as median width is less than 75 feet. <u>New River to Table Mesa</u> Northbound : New River floodplain conflicted with centered widening. Southbound : Construction on both sides is undesirable because of impacts to traffic. | Anthem to New River Inside <u>New River to Table Mesa</u> Northbound : Inside Southbound : Inside |
| Major Differentiators | N/A | <u>Table Mesa to Rock Springs</u> Northbound : Requires less earthwork. Southbound : Does not match widened Little Squaw Creek bridge. Requires more earthwork. | Table Mesa to Rock Springs Northbound: Requires more earthwork. Southbound: Matches widened Little Squaw Creek bridge. Requires less earthwork. | <u>Table Mesa to Rock Springs</u> Northbound : Construction on both sides is undesirable because of impacts to traffic. Southbound : Does not match widened Little Squaw Creek bridge. | <u>Table Mesa to Rock Springs</u> Northbound: Inside Southbound: Outside |
| | | Rock Springs to Black Canyon City Parallel alignments accommodate future inside widening. Barrier required as median width is less than 75 feet. | Rock Springs to Black Canyon City Right-of-way constraints on outside. | Rock Springs to Black Canyon City Right-of-way constraints on outside. Construction on both sides is undesirable because of impacts to traffic. Barrier required as median width is less than 75 feet. | Rock Springs to Black Canyon <u>City</u> Inside |

TABLE 29 – EVALUATION MATRIX, ANTHEM WAY TI TO BLACK CANYON CITY TI (MP 229.1 TO MP 244.5) NEAR-TERM ALTERNATIVES

| Criterion | No Build Alternative | Alternative D | Alternative E | Advantage |
|---|---|---|---|-------------|
| Lane Designation Legend ↓ = Existing lane direction of travel ↓ = Proposed lane direction of travel | ↓↓ ↑↑ | $\downarrow\downarrow\downarrow\downarrow$ $\uparrow\uparrow$ $\uparrow\uparrow$ | $\downarrow\downarrow\downarrow\downarrow$ $\uparrow\uparrow$ $\uparrow\uparrow$ | |
| Traffic Operations / Geometrics | | | | |
| Typical Section | No change to existing roadways. | On Black Canyon Hill: 3 SB lanes on new alignment west of and between exst NB & SB rdwys; 2 NB lanes on existing SB rdwy, 2 NB lanes on existing NB rdwy North of Sunset Pt, widen existing to 3 lanes each direction. | On Black Canyon Hill: 3 SB lanes on new alignment mostly west of existing I-17; 2 NB lanes on existing SB rdwy 2 NB lanes on existing NB rdwy North of Sunset Pt, widen existing to 3 lanes each direction. | |
| Traffic Operations | Provides LOS F in design year 2040 | Provides LOS C in design year 2040 | Provides LOS C in design year 2040 | Alt. D or E |
| Traffic Operations – Truck Route | Trucks on 6% NB grade, 6% SB grade. | Trucks on 6% NB grade, new 5% SB grade. | Trucks on 6% NB grade, new 5% SB grade. | Alt. D or E |
| Maintenance of Facilities (Full or Partial Closures during ADOT maintenance or DPS crash-related activities) Incident Management on Black Canyon Hill (All build alternatives are equal north of Sunset Point TI) | Full Closures – NB Full Closures – SB No new opportunities for managing incidents. | Partial closures in segment with alternative route – NB Full Closures – SB NB traffic can be shifted to the clear roadway at locations where the profiles line up vertically (Black Cyn City TI and Bumble Bee TI). | Partial closures in segment with alternative route – NB Full Closures – SB NB traffic can be shifted to the clear roadway at locations where the profiles line up vertically (Black Cyn City TI and Bumble Bee TI). | Alt. D or E |
| Resolve Geometric Deficiencies / Design Exceptions | No improvements to existing geometrics; numerous design exceptions will be required. | Improves horizontal alignment and superelevation (separate cost); 6% grades remain on existing roadway (3 segments above 6% in NB direction). North of Sunset Pt, Grades greater than 4% remaining in rolling terrain: 4 segments in SB direction (5.2% to 4.0%); 6 segments in NB direction (5.0% to 4.3%) | Improves horizontal alignment and superelevation (separate cost); 6% grades remain on existing roadway (3 segments above 6% in NB direction). North of Sunset Pt, Grades greater than 4% remaining in rolling terrain: 4 segments in SB direction (5.2% to 4.0%); 6 segments in NB direction (5.0% to 4.3%) | Alt. D or E |

TABLE 30 – EVALUATION MATRIX, BLACK CANYON CITY TI TO SUNSET POINT TI (MP 244.5 TO MP 252.5), LONG-TERM ALTERNATIVES

| Criterion | No Build Alternative | Alternative D | Alternative E | Advantage |
|--|------------------------------------|--|---|------------------|
| Lane Designation Legend ↓ = Existing lane direction of travel ↓ = Proposed lane direction of travel | ↓↓ ↑↑ | $\downarrow\downarrow\downarrow$ $\uparrow\uparrow$ $\uparrow\uparrow$ | $\downarrow\downarrow\downarrow\downarrow$ 11 11 | , |
| Connectivity / Access | | | | |
| Connectivity at Bumble Bee Crossroad | No change to existing connections. | Retain connection from existing NB roadway. Remove existing Bumble Bee SB ramps due to directional conversion from SB to NB (=no NB connection to Bumble Bee from exst SB rdwy after conversion to NB). No connection to Bumble Bee TI from new SB alignment because required ramp grades of 9% and 18% exceed 6% maximum allowable grade. | Retain connection from existing NB roadway. Remove existing Bumble Bee SB ramps due to directional conversion from SB to NB (=no NB connection to Bumble Bee from exst SB rdwy after conversion to NB). Construct new ramp connections to Bumble Bee from new SB alignment. | No Build, Alt. E |
| Routes (NB and SB) Provide Access or Motorist Must Decide Which Route Is Required (Full Access or Decision) | | | | |
| Black Canyon City TI | NB & SB - Full Access | NB & SB - Full Access | NB & SB-Full Access | |
| Bumble Bee TI | NB & SB - Full Access | NB – Decision SB – No Access | NB - Decision | No Build, Alt. E |
| Sunset Point TI | NB & SB - Full Access | NB & SB - Full Access | NB & SB - Full Access | |
| ROW Acquisition (Acres) – all public land managed by BLM | 0 | 262 | 344 | No Build, Alt. D |
| Estimated Costs | | | | |
| Estimated Construction Cost (SE = Superelevation) | N/A | \$ 255,900,000 BCC to Sunset Pt <u>\$ 71,600,000 Sunset Pt to Jct. SR 69</u> \$ 327,500,000 BCC to Jct. SR 69 + \$90,200,000 SE Imprvmts BCC to Jct. SR 69 (+4 acres ROW) | \$ 286,000,000 BCC to Sunset Pt <u>\$ 71,600,000 Sunset Pt to Jct. SR 69</u> \$ 357,600,000 BCC to Jct. SR 69 + \$90,200,000 SE Imprvmts BCC to Jct. SR 69 (+4 acres ROW) | No Build, Alt. D |

| Criterion | No Build Alternative | NB Climbing Lane (Alt. CL) | (Two) Flex Lanes (Alt. FL) | Part-Time Shoulder Lane (PTSL) | Advantage |
|--|---|--|--|---|-------------------------|
| Lane Designation Legend ↓ = Existing lane direction of travel ↓ = Proposed lane direction of travel | ↓↓ ↑↑ | ↓↓ ↑↑↑ | ↓↓\$\$ ↑↑ | ↓↓↓ ↑↑↑ | |
| Typical Section | No change to existing roadways. | On Black Canyon Hill: 2 SB lanes on existing SB rdwy; 2+1 NB lanes on existing NB rdwy No added lanes south of Black Cyn City or north of Sunset Pt. | On Black Canyon Hill: 2 SB lanes on existing SB rdwy plus barrier-separated <u>two-lane</u> flex roadway; 2 NB lanes on existing NB rdwy No added lanes south of Black Cyn City or north of Sunset Pt. | On Black Canyon Hill: 2+1 part-time SB lanes on existing SB rdwy; 2+1 part-time NB lanes on existing NB rdwy No added lanes south of Black Cyn City or north of Sunset Pt. | |
| Traffic Operations | Provides LOS F in design year 2040 | Provides NB LOS E in design year 2040. SB LOS remains at LOS F. | Provides peak LOS C on flex facility in design year 2040. LOS B-D in peak direction on mainline. LOS D- F in non-peak direction on mainline. | Similar to No Build Alternative during non-peak periods. Similar results to one-lane flex facility during peak periods; however, crashes or vehicle breakdowns would not have shoulder width for refuge. | Alt. FL |
| Maintenance of Facilities (Full or Partial Closures during ADOT maintenance or DPS crash-related activities) Incident Management on Black Canyon Hill | Full Closures – NB Full Closures – SB No new opportunities for managing incidents. | Full Closures – NB Full Closures – SB No new opportunities for managing incidents. | Partial closures in segment with alternative route – NB or SB The flex roadway can be used during peak period or (depending on ease of reversing) to route traffic around incidents as needed. | Using the part-time shoulders would be difficult during incidents the shoulders may provide the only way for emergency response vehicles to get to the scene of an accident. | Alt. FL |
| Resolve Geometric Deficiencies / Design Exceptions | No improvements to existing geometrics; numerous design exceptions will be required. | No improvements to existing geometrics; numerous design exceptions will be required. | No improvements to existing geometrics; numerous design exceptions will be required. | No improvements to existing geometrics; numerous design exceptions will be required. | |
| Routes (NB and SB) Provide Access or Decision of Route Required (Full Access or Decision) Black Canyon City TI Bumble Bee TI Sunset Point TI | NB & SB - Full Access NB & SB - Full Access NB & SB - Full Access | NB & SB - Full Access NB & SB - Full Access NB & SB - Full Access | Existing NB & SB – Full access NB & SB - Full Access NB & SB - No Access NB - Full Access SB - Emergency access only | NB & SB - Full Access NB & SB - Full Access NB & SB - Full Access | No Build, Alt. CL, PTSL |

TABLE 31 – EVALUATION MATRIX, BLACK CANYON CITY TI TO SUNSET POINT TI (MP 244.5 TO MP 252.5), NEAR-TERM ALTERNATIVES

| Criterion | No Build Alternative | NB Climbing Lane (Alt. CL) | (Two) Flex Lanes (Alt. FL) | Part-Time Shoulder Lane (PTSL) | Advantage |
|---|----------------------|---|--|---|-------------------------|
| Lane Designation Legend \downarrow = Existing lane direction of travel \downarrow = Proposed lane direction of travel | ↓↓↑↑ | ↓↓ ↑↑↑ | ↓↓\$\$ ↑↑ | ↓↓↓ ↑↑↑ | 33 - |
| ROW Acquisition (Acres) (All public land managed by BLM) | 0 | 3.0 | 1.8 | 0 | - |
| Estimated Construction Cost | N/A | \$34,200,000 | \$106,300,000 | Some construction costs to construct emergency turnouts. Other costs for guardrail, signing, pavement marking, rumble strips, and asphalt rubber also required. | No Build, Alt. CL, PTSL |
| Structures / Retaining Walls | No change. | Replace NB I-17 bridge over Bumble Bee Rd. Construct five walls to contain slopes in ROW. | Replace Bumble Bee Rd bridge over SB I-17. Construct three walls to contain slopes in ROW. | No change. | No Build, PTSL |

Recommended Alternative – Anthem Way to Black Canyon City, Near-Term 3.8

The Anthem Way to Black Canyon City widening is identified as a Recommended Near-Term Alternative for the following reasons:

- Improved LOS compared to the existing condition •
- Provides connectivity to all existing TIs •
- Matches I-17 widening from Carefree Highway to Anthem Way •
- Implement inside and outside widening as recommended to avoid conflicts and minimize construction costs

Recommended Alternative – Black Canyon City to Cordes Junction, Long-Term 3.9

Alternative E is identified as the Recommended Long-Term Alternative for the following reasons:

- Improved LOS compared to the existing condition •
- Provides connectivity to all existing TIs •
- Alternative alignment provides opportunity for horizontal curvature and superelevation elements to be • improved on existing northbound and southbound roadways

If the near-term alternatives are constructed, Alternative E may need to be re-evaluated. Alternative E assumes a new three-lane facility for southbound I-17; the four existing travel lanes would be used for northbound with a total of seven lanes. If Alternative FL is constructed, there would be a total of six existing travel lanes, potentially leaving a long-term need of one additional lane. Capacity needs should be re-evaluated if a long-term alternative is selected.

Recommended Alternative – Black Canyon City to Cordes Junction, Near-Term 3.10

The Two-Lane Flex Roadway Alternative (FL) is identified as the Recommended Near-Term Alternative for the following reasons:

- Improved LOS in both directions compared to the existing condition and other near-term alternatives
- Best flexibility for incident management

3.11 Developing the Near-Term Alternatives

The Near-Term Alternatives are recommended for development for the following reasons:

- Current funding cannot accommodate Alternative E
- Short-term alternatives meet current traffic volume demands •
- sooner, especially for incident management on the Black Canyon Hill

The next chapters of this report focus on the recommended Anthem Way to Black Canyon City widening and Alternative FL, flex lanes on the Black Canyon Hill.

Length of construction is much shorter with short-term alternatives, thus offering the traveling public relief

4.0 Major Design Features of the Recommended Alternative

4.1 Introduction

This chapter will discuss the major design features associated with the Near-Term Recommended Alternatives – Anthem Way to Black Canyon City widening and Alternative FL, flex lanes from Black Canyon City to Sunset Point.

4.2 Design Controls

Much of the I-17 project will match existing horizontal and vertical geometry and superelevation. Where new crossover lanes are provided, they will be designed to meet ADOT design criteria and follow AASHTO guidelines. The proposed typical section for the new roadways will consist of 12-foot travel lanes and 10-foot inside and outside shoulders for typical sections with more than two lanes. For the flex lanes, a 4-foot inside (west) shoulder and a 10-foot outside (east) shoulder with a 2-foot offset to barrier are recommended. Glare screen should be considered on the flex lane barrier. Table 32 presents the preliminary design criteria for the new roadways and mainline widening. "**" is shown where the improvements will match existing geometry that doesn't meet minimum design criteria.

TABLE 32 - PRELIMINARY ROADWAY DESIGN CRITERIA

| DESCRIPTION OF CRITERION | VALUE FOR DESIGN |
|---|--|
| Design Year: | 2040 |
| AADT: | 52,100 – 58,900 |
| Level of Service: Level Terrain (MP 229 – 232) | C/D (See Section 2.1.3) |
| Rolling Terrain (MP 232 – 244 | C/D (See Section 2.1.3 + context-sensitive considerations such as mountainous terrain, rural surroundings) |
| Mountainous Terrain (MP 244.5 to 252) | C (See Section 2.1.3) |
| Elevation Range: | 1,900 ft. to 3,800 ft. |
| Lane Width: | 12 ft. (RDG, Section 301.3) |
| Shoulder Width: Inside and Outside | (RDG, Table 302.4) 10 ft. + 2' offset to barrier (3-lane section) |
| Barrier-Side (Flex Roadway) | 4 ft. |
| Median-Side (Flex Roadway) | 10 ft. + 2' offset to barrier |
| Median Width: | 84 ft. desirable (50 ft. minimum) (RDG, Section 304.1, Figure 306.2) |
| Existing and Normal Cross Slope: | ** 2.0% (RDG Section 301.2) |

| DESCRIPTION OF CRITERION | |
|--|--|
| Superelevation: | |
| MP 229 to 252 | ** e _{max} =0.10 4000 ft) |
| Median Barrier | Required: 1.) If media 2.) If media direction |
| Design Speed: Mainline: | |
| (MP 229.0 to 244.5) (Controlled Access Highway, level/rolling terrain) (MP 244.5 to 250.5) (Controlled Access Highway, mountainous terrain) | 75 mph 65 mph |
| Ramp Exit at Mainline Gore: Taper-Type | Mainline de |
| Parallel-Type | Mainline de |
| Ramp Entrance: | Mainline de |
| Ramp Body: | 50 mph (R |
| Ramp Terminus: | 35 mph (R |
| Crossroad: | 40 mph, but the intercha |
| Minimum Horizontal Curve Length: MP 229.0 to 244.5 MP 244 5 to 250 5 | 15 x desigr ** 1125 |
| Maximum Degree of Curve: | 0101 |
| MP 229.0 to 244.5 | ** 2°54' (R |
| MP 244.5 to 250.5 | ** 4°16' (R |
| Maximum Gradient: Mainline: | |
| MP 229.0 to 232.0 | 3%; match |
| MP 232.0 to 244.5 | ** 4%; mate |
| MP 244.5 to 250.5 | ** 5%; mate |
| Upgrade Downgrade | 4% desirab |
| Side Slope: | ADOT Star cut slope m to eliminate |
| Minimum Vertical Curve Length: | 1000 ft (RD |
| Taper Rate (Lane Drop): MP 229.0 to 244.5 MP 244.5 to 250.5 | Design spe 75:1 |
| Taper Rate (Lane Addition): MP 229.0 to 252.0 | 25:1 |
| Design Vehicle: | WB-67 |
| Minimum Vertical Clearance (new structure): | (RDG, Sec |
| Underpass | 10.5 It. ** 16.5 ft |
| | 10.0 10 |

VALUE FOR DESIGN 0 ft./ft. (RDG, Table 202.1A, Rural Highway, Elevation < (RDG, Section 304.4) an width ≤ 50 ft., or an width \leq 75 ft. and there are 3 or more lanes in each esign speed minus 10 mph (RDG, Section 503.3) esign speed minus 5 mph (RDG, Section 503.3) esign speed minus 10 mph (RDG, Section 503.3) RDG, Section 503.3) (DG, Section 503.3) ut not less than design speed of crossroad approaches to ange speed (mph): (RDG, Section 203.5) ft. ft. DG, Table 202.3D) DG, Table 202.3D) existing vertical alignment (RDG, Table 204.3) ch existing vertical alignment (RDG, Table 204.3) ch existing vertical alignment (RDG, Table 204.3) ble, 6% maximum (RDG, Section 504.1) ble, 6% maximum (RDG, Section 504.1) ndard C-02.10 (RDG, Figure 306.2) plus, when applicable, nodifications for rockfall containment and fill slope flattening the need for roadside guardrail OG, Table 204.4) eed (mph) to one: (RDG, Section 207) tion 206.4)

4.3 Horizontal and Vertical Alignments

4.3.1 Anthem Way TI to Black Canyon City TI

Existing horizontal alignments control I-17 northbound widening from Anthem Way to Black Canyon City. All northbound widening in this section is to the inside; employing the existing alignment works well as the centerline will remain on a lane line between the outside two lanes, which is standard design procedure and matches the design on I-17 from Carefree Highway to Anthem Way.

For southbound I-17 from Anthem Way to Black Canyon City, the existing horizontal alignment will be used for inside widening and a new construction centerline will be established for outside widening. The new centerline will be offset 15 feet to the outside from the existing alignment. New horizontal curves were defined for transitions from inside to outside widening. Table 33 summarizes areas of southbound inside and outside widening.

| Start MP | End MP | Widening Direction |
|----------|--------|--------------------|
| 229.1 | 237.0 | Inside |
| 237.0 | 237.4 | Transition |
| 237.4 | 240.6 | Outside |
| 240.6 | 240.8 | Transition |
| 240.8 | 245.0 | Inside |

TABLE 33 – SOUTHBOUND WIDENING MP 229 – 245

Existing vertical alignments will be followed for northbound and southbound widening from Anthem Way to Black Canyon City. Widening will be accomplished by sawcutting and widening using the existing cross slope.

Sawcutting/Widening: Based on a review of the record drawings, the structural section for the shoulder matched the mainline during the initial construction. However, since the initial construction, I-17 has had one or more mill and overlays on the mainline, but not the shoulder. The difference in the pavement section thickness between the mainline and the shoulder from the overlays is variable across the project length as the shoulder has been paved with rubberized asphalt in some areas, but not others. Rubberized asphalt is proposed for the mainline travel lanes and both shoulders as shown in the typical sections in Appendix A.

When considering reusing the existing shoulder as part of the future travel lanes, other considerations include the existing condition/age of the pavement and the required design (i.e., structural number) to support future traffic for the 20-year design life. The existing pavement was constructed in the 1960s and 1970s with minimal maintenance other than fog coats, according to the as-built information.

To be conservative, shoulder reconstruction is recommended. Where inside widening is proposed, the existing 4-foot shoulder will be removed. Where widening to the outside is proposed, the existing 10-foot shoulder will be removed.

A segment of southbound I-17 at approximately MP 241.2 has been the site of crashes for which wet road conditions were cited. The final designer should review the roadway geometry, cross slope through the curve, and the Rock Springs TI southbound entrance ramp merge to identify geometric or roadway drainage elements that may be contributing to crashes at this location.

4.3.2 Black Canyon City TI to Sunset Point TI

The flex lanes generally follow the existing I-17 southbound horizontal and vertical alignments except at the north and south crossovers, which will be used by northbound vehicles to access the flex lanes adjacent to the southbound roadway when permitted. The crossovers are approximately one-half mile long and have two horizontal curves, each with a radius of 9,550 feet. The final designer may consider increasing separation or adding barrier to discourage wrong-way movements.

The flex lanes will be controlled vertically by the existing I-17 southbound vertical alignment; the southbound roadway will be sawcut and widened at the existing freeway cross slope, with two exceptions: The first exception is at the south crossover where northbound traffic uses the crossover to enter the flex lanes just north of Black Canyon City. Existing southbound I-17 in this area is lower in elevation than northbound I-17; therefore, a new vertical alignment will be created for the flex lanes to resolve the elevation differences for the crossover. The crossover alignment is approximately 3,700 feet long.

A new vertical alignment also is required at the north crossover near Sunset Point. The existing northbound and southbound grades in this area are relatively flat at 0.7% and the terrain between them is also flat, enabling a new 1,000 feet long vertical alignment without any vertical curves.

Consideration was given to modifying the flex lanes' superelevation to meet current standards rather than extending the cross slope from the southbound lanes to the flex lanes. However, that option is not recommended because of the difficulty controlling the vertical alignment, determining

a pivot point, aligning the barrier between the two facilities, and the long-term impact if the flex lane facility were to be converted to a southbound-only roadway in the future.

Cape Horn: Widening to the west should be evaluated in this area (MP 247.0 to MP 248.5, south of Bumble Bee TI) during final design to respond to concerns about movement in the slope on the east side of I-17. Widening to the west would result in the need for new ROW unless substantial retaining walls are constructed. Retaining walls and side slopes of 2:1 and 3:1 should be considered in terms of aesthetics, maintenance, right-of-way, and cost.

Plan sheets for the recommended alternatives are presented in Appendix B. The 1"=200' scale plans provide preliminary horizontal design for the recommended alternatives. Geometric data is shown for the existing and modified mainline I-17 curves.



4.3.3 Mapping and Grid Adjustment Factor

Detailed topographic mapping was prepared for this project from MP 229 to MP 252. Additional mapping may be needed during final design at cut and fill slope limits and for new signs north of the Sunset Point TI. Supplemental mapping may also be needed in order to evaluate widening to the west for the flex lanes near the Cape Horn area south of the Bumble Bee TI.

A grid adjustment factor of 1.00016 was selected, which matches record drawings for most of the project area. Right-of-way plans for ADOT projects H6368 and H5059 indicate a grid adjustment factor of 1.00026298 from MP 249 to MP 252. Grid adjustment factors are used to adjust horizontal lengths to match the topography of the earth. During final design, a single grid adjustment factor may be used for simplicity, or the project could be divided into two in order to more accurately measure horizontal lengths in the area from MP 249 to MP 252.

44 Access

I-17 is an access-controlled facility. Modifications to existing access for the recommended alternative should be coordinated with ADOT and FHWA to determine whether a Change of Access Report is required.

Official ADOT crossovers on the existing alignments are located at MP 231.21, 233.98, 235.63, 236.45 (Table Mesa TI), 240.75/242.55 (Rock Springs TI), 245.00, and 251.46 (Sunset Point Rest Area). The crossovers at MP 245.00 and 251.46 will be removed because they conflict with the flex lane crossovers.

South of Sunset Point at approximately Station 2623+00, a primitive road departs from the southbound I-17 roadway. The road is used by AGFD to access a wildlife water catchment. This access point is not impacted by the addition of the flex lanes.

4.4.1 Moores Gulch Grader Road

South of Black Canyon City at approximately MP 238.4, ADOT currently provides access to approximately 700 acres of private property east of I-17 near Moores Gulch. During the original construction of I-17 in the mid-1960s, access to this area was created by a circuitous route departing from the west side of I-17 at Table Mesa Road, proceeding in a north/northwest direction for approximately three miles, then crossing east via a grader road under the northbound and southbound I-17 bridges at Moores Gulch to a point on the east side of I-17. Approximately 2,800 feet of the grader road is part of the State Highway System within ADOT's right-of-way. Maintenance responsibility is ADOT's. Maintenance has proven difficult because of flooding events, which have had the effect of damaging the road within the Gulch. One of the private property owners has performed maintenance activities on the grader road. Although Forest Road 41 connects Table Mesa Road and Moores Gulch on the east side of I-17, the road is rugged and impassable for most vehicles.

ADOT considered long-term solutions to the existing grader road and associated maintenance issues. The solutions included the following:

- constructing a frontage road,
- raising the elevation of the grader road within Moores Gulch, ٠
- constructing a full or partial traffic interchange, •
- purchasing the private property to eliminate the need for access, or
- taking no action.

The recommended solution is to raise the grader road approximately two feet. ADOT Environmental Planning worked with USGS to analyze high water flows at Moores Gulch. The grader road should be relocated to an elevation above the high water elevation. USGS has noted that Moores Gulch had one of the highest flow rates in Arizona during a recent storm event. Elevating or relocating the grader road could be accomplished by rerouting the road to keep it on the south side of the wash near its intersection with northbound I-17.

Right-of-Way 4.5

Approximately 4.5 acres of new right-of-way (ROW) and 2.9 acres of drainage easement are required for the Anthem to Black Canyon City widening along northbound and southbound, as well as for the flex lanes. This right-of-way is needed for rock cut slopes and access to the top of the rock cuts during construction. Drainage easements are also required to construct new pipe and box extensions and associated outfall protection.

TABLE 34 – NEW RIGHT-OF-WAY AND DRAINAGE EASEMENT REQUIREMENTS

| Station | Area Required (sq. ft.) | Туре |
|--------------|-------------------------|-------------------|
| 1965+00 (SB) | 11,930 | New ROW |
| 1970+00 (NB) | 1,240 | Drainage easement |
| 1995+00 (NB) | 5,150 | New ROW |
| 2020+00 (NB) | 49,500 | New ROW |
| 2050+00 (NB(| 1,250 | Drainage easement |
| 2054+00 (NB) | 3,220 | Drainage easement |
| 2065+00 (NB) | 12,780 | New ROW |
| 2085+00 (NB) | 30,660 | New ROW |
| 2090+00 (NB) | 7,410 | New ROW |
| 2566+00 (SB) | 13,200 | New ROW |
| 2587+00 (SB) | 66,300 | New ROW |
| 2627+00 (SB) | 118,930 | Drainage easement |
| TOTAL | 321,570 | |

All required right-of-way and easements are managed by the Bureau of Land Management.

Existing permitted access should be evaluated during final design.

New right-of-way lines shown on the plan sheets in the appendices are based on limits of disturbance identified by the conceptual design layout and do not indicate the final right-of-way requirements or easements necessary for construction. Actual limits will be influenced by final geotechnical slope recommendations and will be established during the final design process.

For the new right-of-way, a steeper rock cut slope or retaining wall could be used to limit needed right-of-way, as well as various slope treatments such as stacking rocks or slope paving. ADOT Materials has indicated that from a long-term and maintenance perspective, acquiring new right-of-way is more desirable than maintenanceintensive retaining wall and slope treatment options. The drainage easements are primarily needed for grading and outlet protection and increases in backwater near adjacent culverts.

There are a number of section corners in the project area which are in or near the roadway. The monuments shall be preserved or replaced if disturbed by construction.

4.6 Drainage Considerations

Drainage design criteria as related to hydrology, hydraulics, and scour were considered at each offsite drainage facility. For existing culverts, the estimated runoff discharges were compared to the culverts' hydraulic capacity to

evaluate the adequacy of the existing facilities. New roadway culverts will be designed to convey the 50-year peak discharge following the design procedures outlined in the ADOT *Highway Drainage Design Manual, Hydraulics,* and the RDG.

Offsite drainage improvements for sections of existing roadway will consist of extending existing culverts, erosion protection, relocating roadside ditches, and relocation of cut slope crown ditches.

New onsite drainage facilities will include barrier catch basins with storm drain outfalls, area-type inlets, spillways, down drains, and roadside ditches. In the vicinity

of new guardrail installations, curb may be required to intercept roadway sheet flow and convey the discharges to new spillways and/or new down drains. Onsite drainage facilities will be designed for the 10-year rainfall event.

Additional drainage analyses necessary to present drainage solutions to existing issues and preliminary sizes of new drainage elements for the recommended alternative were included in the Preliminary Drainage Report for this project.

Anthem Way TI to Black Canyon City

Most of the drainage improvements along I-17 from the Anthem Way TI to Black Canyon City are associated with the extension of either reinforced concrete box culverts or pipe culverts. These extensions were made with consideration to clear zone requirements. The lengths of the required extensions were based on the greater of the appropriate clear zone or the width of the roadway widening at each location.

The northbound and southbound lanes of I-17 closely parallel each other from Anthem Way to just north of the New River interchange. The median area between northbound and southbound lanes is currently drained by median catch basins connected to small-diameter pipes. These pipes convey flow under either the northbound or southbound lanes to an outfall channel. The median inlets will continue to be utilized but may need to be adjusted to account for changes created by the new slopes.

The analysis of culverts within this section showed that several of the existing culverts do not meet hydraulic design requirements. An additional culvert is proposed at these locations to meet the design requirements. Table 35 lists the culverts that do not meet hydraulic requirements and the proposed culvert improvements.

Some culvert extensions will require permanent drainage easements or acquisition of right-of-way. Approximately five culverts between the Table Mesa TI and the Rock Springs TI will likely require an easement or right-of-way to accomplish the necessary improvements.

TABLE 35 - UNDERSIZED CULVERTS, ANTHEM WAY TO BLACK CANYON CITY

| Culvert Station | Existing Culvert | Proposed Size |
|-----------------|------------------|---------------|
| 2072+54 SB | 1-30" CMP | 2-30" CMP |
| 2099+17 NB | 1-24" CMP | 2-24" CMP |
| 2136+23 SB | 1-30" CMP | 2-30" CMP |
| 2270+10 SB | 1-30" CMP | 2-30" CMP |
| 2273+10 SB | 1-30" CMP | 2-30" CMP |
| 2606+56 SB | 1-36" CMP | 2-36" CMP |

Black Canyon City to Sunset Point TI

Drainage improvements along I-17 from the Black Canyon City TI to the Sunset Point TI are associated with the extension of either reinforced concrete box culverts or pipe culverts and onsite improvements to handle runoff that would be collected and conveyed along the barrier between the existing and proposed lanes.

The roadway improvements will occur along the inside of the existing southbound lanes. In many instances, the proposed improvements require excavation in steep rock slopes along the existing roadway. A ditch will collect runoff from the proposed roadway widening at the base of the rock slopes. The existing culverts will be extended to the proposed ditch bottom. Because of the amount of rock excavation, the ditch bottom was not extended to a point that would place the culvert extension outlets outside of the clear zone. The culverts that fall into this category are circular culverts that are less than 60 inches in diameter. These culverts will have a safety end section to allow them to terminate within the clear zone. Additional culverts that terminate within the clear zone are protected by proposed guardrail.

Several existing culverts do not meet hydraulic design requirements. An additional culvert is being proposed at these locations to meet the design requirements. Table 36 lists the culverts that do not meet hydraulic requirements and the proposed culvert improvements. Some of the culverts that do not meet the HW/D<1.5 requirement are not being augmented with an additional culvert to meet this requirement because the ponding is within existing right-of-way and it is localized at the inlet.

TABLE 36 – UNDERSIZED CULVERTS, BLA

| Culvert Station | Existing Culvert | Proposed Size |
|------------------------|------------------|----------------------|
| 2349+20 SB | 1-54" CMP | 2-54" CMP |
| 2383+94 SB | 1-24" CMP | 2-24" CMP |
| 2426+30 SB | 1-30" CMP | 2-30" CMP |
| 2562+26 SB | 1-24" CMP | 2-24" CMP |
| 2598+08 SB | 1-48" CMP | 1-48", 1-36" CMP |
| 2606+56 SB | 1-36" CMP | 2-36" CMP |



| ACK CANYON CITY TO SUNSET POINT |
|---------------------------------|
|---------------------------------|

There is an existing culvert under the northbound and southbound lanes at the southern flex lane crossover at approximately northbound Sta 2332+59 and southbound Sta 2332+09. The crossover pavement will cover the outlet of the northbound culvert and the inlet of the southbound culvert. The culverts are not aligned along the same skew across the existing roadway, making connecting the two culverts an undesirable option. Therefore, a new culvert is recommended that will extend under both the northbound and southbound lanes and will be aligned with the upstream and downstream wash flow lines.

The roadway improvements within this section will require onsite drainage improvements to collect drainage that concentrates along the roadway against the proposed barrier between the existing and proposed lanes. The roadway is superelevated through the horizontal curves. Depending on the superelevation direction, runoff from the roadway will collect along the barrier on either the existing or proposed roadway side. A four- to six-foot shoulder is proposed on both sides of the barrier. Runoff can be conveyed along the barrier within the shoulder. When the capacity of the shoulder is exceeded, inlets will be placed to collect flow and convey it via a storm drain off the roadway. Barrier inlets with slotted drain are proposed with inlet design based on the ten-year storm event. In most instances, the storm drains that drain the inlets will be directed under the proposed roadway to outfall.

Section 404 of the Clean Water Act 4.7

Coordination with the COE during project design will be necessary to ascertain the need for any nationwide or individual permits required under Section 404 of the Clean Water Act. Any deposition of fill material or excavation below the ordinary high water mark will require a permit. Construction activities that will require permits include, but are not limited to, bridge pier construction, culvert installations, replacements and/or extensions requiring excavation and placement of fill material, and roadway embankment widening.

4.8 **Floodplain Considerations**

The following areas have been identified by FEMA as either floodplains or floodways and have been delineated on a Flood Insurance Rate Map (FIRM):

- Black Wash •
- New River
- Moores Gulch
- Little Squaw Creek
- Agua Fria River

Within the vicinity of Black Canyon City, the Agua Fria River has been mapped as Flood Zone AE, with an associated floodway. The remaining portion of the Agua Fria River has been mapped as Flood Zone A.

Applications for Conditional Letter of Map Revision(s) (CLOMR) may be required by FEMA as a result of possible encroachments into a designated floodplain.

Geotechnical, Pavement, and Earthwork Considerations 4.9

The recommended mainline alternatives will match the existing I-17 roadway profile. Approximate earthwork requirements are presented in Table 37. Earthwork estimates are approximate and should be verified during final design.

TABLE 37 – EARTHW

| LOCATION | ROADWAY EXCAVATION (CU. YDS.) | ROCK EXCAVATION (CU. YDS.) | EMBANKMENT WITH 15% SWELL (CU. YDS.) | WASTE VOLUME (CU. YDS.) |
|--|-------------------------------------|----------------------------------|--|----------------------------|
| Anthem Way to Black Canyon City Northbound | 240,000 | 485,000 | 225,000 | 500,000 |
| Anthem Way to Black Canyon City Southbound | 445,000 | 295,000 | 235,000 | 505,000 |
| Black Canyon City to Sunset Pt Flex Lanes | 340,000 | 1,580,000 | 140,000 | 1,780,000 |
| TOTAL | 1,025,000 | 2,360,000 | 600,000 | 2,785,000 |

The preferred alternative is expected to produce excess material. Some of this waste material can be used onsite in fill slopes where feasible.

Consideration should be given during final design to construction methods and contractor access to tall cut and fill slopes. Benching will likely be required to allow access for large earthmoving equipment. Sliver cuts and fills should be avoided. Tables 38 and 39 summarize approximate cut and fill heights throughout the project.

TABLE 38 – ANTHEM TO BLACK CANYON CITY CUT/FILL HEIGHTS

| Location | Length (ft) | Fill – Max Height (ft) | Cut – Max Height (ft) |
|--------------------------------|-------------|------------------------|-----------------------|
| Sta 1496+00 to 1648+00 (SB/NB) | 15,200 | N/A (median ditch) | N/A (median ditch) |
| Sta 1648+00 to 1658+00 (SB) | 1,000 | 10 | 0 |
| Sta 1658+00 to 1668+00 (SB) | 1,000 | 0 | 10 |
| Sta 1668+00 to 1677+00 (SB) | 900 | 30 | 0 |
| Sta 1677+00 to 1702+00 (SB) | 2,500 | 0 | 15 |
| Sta 1702+00 to 1712+00 (SB) | 1,000 | 35 | 0 |
| Sta 1712+00 to 1737+00 (SB | 2,500 | 0 | 20 |
| Sta 1737+00 to 1749+00 (SB) | 1,200 | 35 | 5 |
| Sta 1749+00 to 1772+00 (SB) | 2,300 | 0 | 55 |
| Sta 1772+00 to 1781+00 (SB) | 900 | 40 | 0 |
| Sta 1781+00 to 1796+00 (SB) | 1,500 | 0 | 25 |
| Sta 1796+00 to 1801+50 (SB) | 550 | 35 | 0 |
| Sta 1801+50 to 1814+50 (SB) | 1,300 | 0 | 5 |
| Sta 1814+50 to 1852+50 (SB) | 3,800 | 55 | 10 |

| VORK SUMMARY |
|--------------|
|--------------|

| Location | Length (ft) | Fill – Max Height (ft) | Cut – Max Height (ft) |
|--------------------------------|-------------|------------------------|-----------------------|
| Sta 1852+50 to 1865+50 (SB) | 1,300 | 0 | 40 |
| Sta 1865+50 to 1878+00 (SB) | 1,250 | 25 | 0 |
| Sta 1878+00 to 1892+00 (SB) | 1,400 | 0 | 55 |
| Sta 1892+00 to 1911+50 (SB) | 1,600 | 20 | 25 |
| Sta 1911+50 to 1916+00 (SB) | 450 | 0 | 25 |
| Sta 1916+00 to 1932+50 (SB) | 1,650 | 65 | 80 |
| Sta 1932+50 to 1946+00 (SB) | 1,350 | 0 | 55 |
| Sta 1946+00 to 1961+50 (SB) | 1,550 | 10 | 5 |
| Sta 1961+50 to 1971+50 (SB) | 1,000 | 0 | 80 |
| Sta 1971+50 to 1977+00 (SB) | 550 | 25 | 0 |
| Sta 1977+00 to 1997+00 (SB) | 2,000 | 0 | 25 |
| Sta 1997+00 to 2006+50 (SB) | 950 | 25 | 0 |
| Sta 2006+50 to 2025+50 (SB) | 1,900 | 25 | 10 |
| Sta 2025+50 to 2065+50 (SB) | 4,000 | 40 | 50 |
| Sta 2065+50 to 2074+50 (SB) | 900 | 10 | 0 |
| Sta 2074+50 to 2087+00 (SB) | 1,250 | 15 | 30 |
| Sta 2087+00 to 2114+50 (SB) | 2,750 | 35 | 20 |
| Sta 2114+50 to 2126+00 (SB) | 1,150 | 0 | 45 |
| Sta 2126+00 to 2187+00 (SB) | 8,050 | 10 | 40 |
| Sta 2187+00 to 2327+00 (SB/NB) | 14,000 | N/A (median ditch) | N/A (median ditch) |
| Sta 1648+00 to 1673+50 (NB) | 2,550 | 25 | 10 |
| Sta 1673+50 to 1742+00 (NB) | 7,050 | 15 | 55 |
| Sta 1742+00 to 1751+50 (NB) | 950 | 15 | 0 |
| Sta 1751+50 to 1798+00 (NB) | 4,650 | 25 | 35 |
| Sta 1798+00 to 1835+50 (NB) | 3,750 | 5 | 50 |
| Sta 1835+50 to 1871+00 (NB) | 3,550 | 15 | 35 |
| Sta 1871+00 to 1889+00 (NB) | 1,800 | 40 | 15 |
| Sta 1889+00 to 1895+50 (NB) | 650 | 15 | 60 |
| Sta 1895+50 to 1911+00 (NB) | 1,550 | 45 | 15 |
| Sta 1911+00 to 1915+50 (NB) | 450 | 0 | 50 |
| Sta 1915+50 to 1926+50 (NB) | 1,100 | 60 | 0 |
| Sta 1926+50 to 1935+50 (NB) | 900 | 5 | 30 |
| Sta 1935+50 to 1958+00 (NB) | 2,250 | 40 | 15 |
| Sta 1958+00 to 1968+00 (NB) | 1,000 | 0 | 25 |
| Sta 1968+00 to 1988+00 (NB) | 2,000 | 45 | 5 |
| Sta 1988+00 to 1992+50 (NB) | 450 | 0 | 30 |
| Sta 1992+50 to 1997+00 (NB) | 450 | 35 | 0 |
| Sta 1997+00 to 2030+00 (NB) | 3,300 | 5 | 45 |
| Sta 2030+00 to 2034+50 (NB) | 450 | 60 | 0 |
| Sta 2034+50 to 2047+00 (NB) | 1,250 | 0 | 25 |
| Sta 2047+00 to 2064+50 (NB) | 1,750 | 40 | 0 |
| Sta 2064+50 to 2087+00 (NB) | 2,250 | 0 | 35 |
| Sta 2087+00 to 2115+50 (NB) | 2,850 | 35 | 20 |
| Sta 2115+50 to 2123+50 (NB) | 800 | 5 | 110 |
| Sta 2123+50 to 2141+50 (NB) | 1,800 | 40 | 5 |

| Location | Length (ft) | Fill – Max Height (ft) | Cut – Max Height (ft) |
|-----------------------------|-------------|------------------------|-----------------------|
| Sta 2141+50 to 2145+00 (NB) | 350 | 0 | 50 |
| Sta 2145+00 to 2151+00 (NB) | 600 | 45 | 0 |
| Sta 2151+00 to 2156+00 (NB) | 500 | 0 | 110 |
| Sta 2156+00 to 2175+50 (NB) | 1,950 | 25 | 0 |
| Sta 2175+50 to 2187+00 (NB) | 2,450 | 0 | 25 |
| Sta 2327+00 to 2348+00 (NB) | 2,100 | 0 | 60 |
| Sta 2348+00 to 2357+50 (NB) | 950 | 20 | 0 |

TABLE 39 – BLACK CANYON CITY TO SUNSET POINT CUT/FILL HEIGHTS

| Location | Length (ft) | Fill – Max Height (ft) | Cut – Max Height (ft) |
|------------------------|-------------|------------------------|-----------------------|
| Sta 2327+00 to 2345+00 | 1,800 | 0 | 30 |
| Sta 2345+00 to 2354+00 | 900 | 10 | 10 |
| Sta 2354+00 to 2356+50 | 250 | 20 | 0 |
| Sta 2356+50 to 2386+00 | 2,950 | 5 | 90 |
| Sta 2386+00 to 2391+00 | 500 | 10 | 0 |
| Sta 2391+00 to 2466+00 | 7,500 | 5 | 125 |
| Sta 2466+00 to 2470+00 | 400 | 5 | 15 |
| Sta 2470+00 to 2501+00 | 3,100 | 10 | 85 |
| Sta 2501+00 to 2508+00 | 700 | 35 | 0 |
| Sta 2508+00 to 2549+50 | 4,150 | 5 | 55 |
| Sta 2549+50 to 2553+00 | 350 | 5 | 0 |
| Sta 2553+00 to 2579+50 | 2,650 | 0 | 135 |
| Sta 2579+50 to 2596+00 | 1,650 | 5 | 170 |
| Sta 2596+00 to 2599+50 | 350 | 70 | 0 |
| Sta 2599+50 to 2623+50 | 2,400 | 0 | 75 |
| Sta 2623+50 to 2630+50 | 700 | 35 | 0 |
| Sta 2630+50 to 2641+50 | 1,100 | 0 | 10 |
| Sta 2641+50 to 2652+50 | 950 | 5 | 5 |
| Sta 2652+50 to 2676+00 | 2,350 | 5 | 5 |

4.9.1 Earthwork Factors

Estimated earthwork factors for the geologic units within the project corridor are as follows:

TABLE 40 – ESTIMATED EARTHWORK FACTORS

| GEOLOGIC UNIT | EARTHWORK FACTOR | |
|------------------------------------|------------------|--|
| Native soils (Quaternary deposits) | 5 to 10% shrink | |
| Existing embankment | Even | |
| Hickey Formation basalt | 20% swell | |
| Tertiary sediments | Even to 5% swell | |

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| GEOLOGIC UNIT | EARTHWORK FACTOR | |
|---|------------------|--|
| Metavolcanic and other Precambrian rock | 10% swell | |

The swell potential will be influenced by the methods of excavation, the final particle size, and the amount of blending with other soils and/or borrow materials.

Ground compaction during the construction of the roadway embankments will most likely occur within the fine-grained, young sediments deposited on the basin floors and the fine-grained alluvial fans of the lower piedmonts. On average, soils within the project corridor will experience 0.2 feet of ground compaction prior to earthwork activities.

For purposes of preliminary planning, it is estimated that 75 gallons of water will be required per cubic yard of material.

4.9.2 Conditions Along Alternative Alignments

The following subsections provide more detailed descriptions of the geotechnical conditions anticipated along each of the alternative alignments. The discussions are focused on the following geotechnical issues:

- General geologic conditions; •
- Pavement subgrade conditions; .
- Cut slope designs; ٠
- Fill slope designs;
- Use of excavated materials: ٠
- Bridge support systems; and ٠
- Geological and geotechnical constraints. •

4.9.3 General Geologic Conditions

Anthem Way to Black Canyon City - The generalized geologic units between approximate MPs 229 and 244.4 consist of Precambrian metavolcanic rocks and granite intrusions; interbedded sequence of Tertiary basalts, tuffs; Quaternary/Tertiary pediment deposits; and Quaternary surface deposits.

Black Canyon City to Sunset Point – The existing roadways are predominantly underlain by Tertiary sediments between approximate MPs 244.4 and 247, with a minor amount of metavolcanic rock located north of MP 246. Between approximately MPs 247 and 248, the existing roadway is predominantly underlain by Hickey Formation basalt. North of MP 248, the northbound lanes roughly follow the contact between Hickey Formation basalt and metavolcanic rock until the road tops out on Black Mesa at approximately MP 250. The southbound roadway is underlain by metavolcanic rock from approximately MP 248 until it tops out on Black Mesa at MP 250.5. The southbound and northbound roadways are then underlain by basalt to approximately MP 256.5. Old landslide deposits may also be present in the southernmost portion of the corridor.

4.9.4 Pavement Subgrade Conditions

Anthem Way to Sunset Point - Metavolcanic rock will provide suitable support for the roadway. This unit generally has moderate to high strengths and relatively low compressibility, although very localized zones of

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In general, it is anticipated that subgrade conditions will be suitable for most of the alignment. The preliminary investigation identified the following areas of poor subgrade:

- SB Sta 1877+50 to 1957+00 (~MP 236 to 238);
- NB and SB Sta 2289+00 to 2320+00 (~MP 244 to 245); and
- SB Sta 2625+00 to 2710+00 (~MP 251 to 252).

These areas and potentially others will require local treatment including overexcavation and replacement. The depth of overexcavation will be such that three feet below the bottom of the pavement has suitable subgrade soils.

4.9.5 Cut Slope Designs

The ADOT RDG includes several statements regarding the design of side slopes in Section 303.3 as follows:

Cut and fill slopes should initially be designed as shown in the ADOT Construction Standard Drawing C-02.10. Final slopes are then incorporated into the design and shown on the plans as required by the Project Geotechnical Report, Materials Design Report and other considerations such as slope flattening for elimination of barrier, cut widening to facilitate drainage, rockfall, landscape and vegetation establishment, and visual mitigation.

The preliminary recommended cut slope ratios provided below are based on observed site conditions and performance of existing cuts for the various geologic units.

TABLE 41 – RECOMMENDED CUT SLOPE RATIOS

| GEOLOGIC UNIT | SLOPE RATIO |
|--|-------------------|
| Precambrian rock units | 0.75H:1V |
| Tertiary Basalt (including Hickey Formation) | 0.75H:1V |
| Tertiary sediments and volcanic deposits | 0.75H:1V to 1H:1V |
| Quaternary sediments | 1H:1V |
| Notes: | |

- materials.
- 2) A preliminary slope ratio for the Precambrian units of up to 0.75H:1V can be used, however some local flattening may be necessary where other fractures have unfavorable orientations.
- 3) Quaternary deposits of intermediate terrace deposits (Qirn), middle and young intermediate 0.75H:1V in some areas.

The cut slope ratios presented above are considered maximum slope ratios; flatter slopes may be necessary. Site-specific conditions may require engineering controls to reduce rockfall potential. Higher cuts will

relatively softer fault gouge or sheared rock may be encountered within this unit. The Hickey Formation basalt

1) The slope ratio for Tertiary sediments will depend upon the competency (internal strength) of the

deposits, undivided (Qi), and old terrace deposits (Qorn) can have a preliminary slope ratio of

require rockfall containment ditches matched to the slope ratio and height. The following table represents the recommended slope containment ditch width relative to the cut slope ratio and cut slope height for preliminary design.

| | WIDTH of 6H:1V SIDESLOPE (ft) | | | |
|--------------------------|-------------------------------|---------------------------|-----------------|--|
| CUT SLOPE HEIGHT (ft) | CUT SLOPE 1:1 | CUT SLOPE 0.75:1 | CUT SLOPE 0.5:1 | |
| 10 – 20 | 15 feet o | or height of cut, whichev | er is lower | |
| 20 | 20 | 15 | 15 | |
| 40 | 25 | 19 | 15 | |
| 60 | 30 | 28 | 24 | |
| 80 | 40 | 37 | 26 | |
| 100 | 66 | 54 | 41 | |
| 120 | 70 | 58 | 44 | |
| 160 | 78 | 65 | 46 | |
| 200 | 85 | 68 | 49 | |

TABLE 42 – RECOMMENDED SLOPE CONTAINMENT GEOMETRY

Notes

1) Ditch not required for slopes less than 10 feet high.

Crown ditches are recommended on the top of proposed cuts that have exposed height of greater than 40 feet. The location of the crown ditches should be sufficiently far away from the cut slope face to provide stability and minimize erosion to the rock face.





Slope rounding is recommended per the ADOT construction standard drawings (C-02) in cuts that are not in solid rock. This rounding should be performed in the upper five feet of the cut. The slope rounding will minimize the dislodging of loose debris at the top of the cuts and will enhance the visual impacts of the cut by softening the hard edges of the top of the cut slope and better blend them into the hillside.

Additional issues which should be considered when designing cut slope ratios for the various alternatives are discussed below.

Existing Roadways – ADOT provided a Rock Hazard Rating System summary for existing cut slopes within the project corridor. The most recent survey available from ADOT was completed in 2004. The summary lists:

1) the starting and ending MPs of the cut, the direction of travel (N or S), and the side of the roadway (R or L) the cuts are located on; 2) the severity (degree of instability) of the slope ranked from 1 through 5 with 5 as the most severe; 3) the number of priority points (the higher the number the greater the perceived instability of the slope); and 4) field comments and/or recommendations. Cut slopes receiving severity ratings of 5 are summarized below.

|--|

| MILEPOST | | | GEVEDITY | PRIORITY | LAST DAY |
|----------|-------|-----------|-----------------|----------|------------|
| Start | End | DIRECTION | SEVERIIT | POINTS | SURVEYED |
| 248.4 | 248.2 | S | 5 | 462 | 02/11/2004 |
| 248.6 | 248.7 | N | 5 | 396 | 02/11/2004 |
| 248.8 | 248.9 | N-L | 5 | 300 | 02/11/2004 |
| 249.0 | 249.1 | N-L | 5 | 342 | 02/11/2004 |
| 249.1 | 249.1 | N | 5 | 507 | 09/19/1995 |
| 249.9 | 249.6 | S | 5 | 396 | 02/11/2004 |
| 249.9 | 250.2 | N-RL | 5 | 498 | 02/11/2004 |
| 255.6 | 255.8 | N-L | 5 | 432 | 02/11/2004 |

In general, the existing cut slopes are generating a considerable amount of rockfall, small slides were observed in the cut slopes, and the rockfall containment ditches generally are undersized. Site-specific conditions may require engineering controls to reduce the potential for rockfall, erosion, and small slides at the cut slopes. Engineering controls could include rock bolting, rock containment fencing, draped mesh, and other measures.

A Brugg rock containment fence has been installed on the right side of the road at approximately northbound MP 247.8 to protect the roadway from small slides and rockfall. Several other areas along existing northbound I-17 are signed as having a potential for small slides. A draped mesh has been installed on both sides of the rock cut on northbound I-17 just south of MP 250 to keep rocks from the basalt flow capping Black Mesa from rolling onto the roadway, and a chain-link fence has been installed on the east side of northbound I-17 near MP 250.

4.9.6 Fill Slope Designs

All non-stabilized fill slopes should be constructed no steeper than 2:1 in accordance with ADOT Standard Drawing C-02.10. Construction of fill slopes should be in accordance with Section 203-10 of the ADOT Standard Specifications. Should steeper slopes be required within drainages or near existing canal structures, use of mechanically-stabilized embankments is recommended.

In areas of potential excessive fill erosion, treatment of slopes with geosynthetics should be considered.

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4.9.7 Use of Excavated Materials

It is anticipated that embankment fills will be constructed using available materials from nearby rock cuts. In general, the geologic materials exposed by the alignments will be suitable for embankment, with the exception of high plasticity soils associated with the soil horizons separating flows in the Hickey Formation and the finegrained deposits of the Tertiary sediments. Staging and phasing of the required excavations will affect the nature of the fill materials. For example, cuts partly in lower density materials (such as the Tertiary sediments) and partly in more competent rock (basalt) will generate materials with different maximum dry densities and optimum moisture contents. Separation or blending of these materials in an embankment could affect the distribution of void spaces, and thus affect the fill densities and swell factors. Nesting of oversized boulders that may result from excavation of the Hickey Formation basalt flows should be avoided.

In general, the rock units are moderately to highly weathered and/or highly foliated and will not be suitable for use as coarse aggregate, mineral aggregate, or riprap. Some of the slightly weathered to unweathered materials, especially the basalt and to a lesser extent the Precambrian metavolcanic rocks, may be suitable for use as riprap. The basalt may locally meet the specifications for part of the coarse aggregate or mineral aggregate, but crushing and processing would be required.

4.9.8 Bridge Support Systems

Structures can be supported on conventional shallow spread-type footings in the harder Precambrian and basaltic rocks (Hickey Formation). Structures should be supported on either spread footings or deep foundations (drilled shafts) in the Tertiary sediments or in areas which may be exposed to scour.

Most of the existing bridge structures along the alignment are founded on spread footings. Many structures that cross waterways utilize driven H-piling.

4.9.9 Geological and Geotechnical Constraints

Several old landslide deposits have recently been mapped by the Arizona Geological Survey north of the Black Canyon City TI and south of Bumble Bee Road (Cape Horn area). A fault crosses southbound I-17 north of Black Canyon City (approx. MP 247.8). Movement of this fault, which may be attributed to a nearby landslide, has caused the need for increased roadway maintenance in this area. An existing fill slope serves as a buttress for the northbound lanes. Consideration should be given if cutting into this slope is required for construction of the flex lanes. Careful consideration should be given to designing appropriate slope ratios and rockfall containment ditches. Protective measures, such as rock catch fences or draped mesh, may be required at certain locations.

A number of existing cut slopes in the mountainous area between mileposts 248 and 250 have been rated by ADOT as a 5 on a severity scale of 1 through 5. The cut slope inventory identified existing cut slopes with rockfall and instability issues and/or rockfall containment ditches that are inadequate. Reducing (flattening) the slope ratio of selected cut slopes, and widening and/or deepening rockfall containment ditches adjacent to selected cut slopes, should be considered when improving the existing roadway.

Cut slope design through all new areas needs to include a rockfall containment ditch of suitable geometry based on exposed rock and cut slope angle.

4.10 Preliminary Pavement Design

A preliminary pavement design has been developed for this segment of I-17. The results of the analyses are summarized in Table 44.

Two pavement types considered for this project were asphalt concrete and Portland cement concrete pavement (PCCP). Based on the availability of materials and flexibility of placing traffic on the new surface during construction activities, a pavement section consisting of AC over AB to provide the required thickness to meet the required structural requirements is recommended. An asphalt rubber-asphaltic concrete friction course (AR-ACFC) surface course measuring ½ inch is also recommended.

The pavement sections provided in Table 44 apply only to the new lanes. In addition, there are some areas of poor subgrade (0 to 3 feet) that need to be removed from beneath the new lanes.

TABLE 44 – PAVEMENT DESIGN PARAMETERS

| PARAMETER | ANTHEM WAY TO NEW RIVER ROAD | NEW RIVER ROAD TO BLACK CANYON CITY | BLACK CANYON CITY TO SUNSET POINT |
|--|---------------------------------|---|---|
| Approximate Station Limits | 1490+00 to 1678+00 | 1678+00 to 2289+00 | 2289+00 to 2710+00 |
| Milepost | 229 to 232 | 232 to 244 | 244 to 252 |
| Design R Value | 30 | 30 | 30 |
| Regional Factor (Cordes Junction) | 2.6 | 2.6 | 2.6 |
| Resilient Modulus | 10,075 psi | 10,075 psi | 10,075 psi |
| Pavement Design Year ADT | 59,619 | 56,763 | 52,418 |
| Lane Factor (Four-Lane Road) | 0.70 | 0.70 | 0.70 |
| Direction Factor | 0.61 | 0.60 | 0.56 |
| Traffic: | | | |
| Automobiles | 88.4% | 75.9% | 73.9% |
| Commercial | 11.6% | 24.1% | 26.1% |
| Vehicle Equivalencies: | | | |
| Automobiles | 0.0008 | 0.0008 | 0.0008 |
| Commercial | 1.2000 | 1.2000 | 1.2000 |
| Equivalent 18-kip Single Axle Loadings | 23,480,353 | 44,736,277 | 39,940,961 |
| Level of Reliability | 99% | 99% | 99% |
| Overall Standard Error | 0.35 | 0.35 | 0.35 |
| Design Change in Serviceability (ΔPSI) | 1.2 | 1.2 | 1.2 |
| Minimum Structural Number Required | 6.09 | 6.65 | 6.55 |
| Pavement Section: | | | |
| Asphaltic Concrete | 11 | 11 | 11 |
| Aggregate Base | 11 | 14 | 14 |

4.11 Interchanges

4.11.1 Introduction

There are seven TIs within the study area:

- Anthem Way MP 229.1
- New River MP 232.0
- Table Mesa MP 236.0

- Rock Springs MP 242.2
- Black Canyon City MP 244.4
- Bumble Bee MP 248.4
- Sunset Point / Rest Area MP 252.5

The configuration of the TIs will not be impacted by the near-term alternatives, although access between three TIs (Black Canyon City, Bumble Bee, and Sunset Point) and the flex lanes will be limited.

Recent crash data was assembled and roadway segments with cluster of crashes were identified for Interactive Highway Safety Design Model (IHSDM) analysis, six of which were related to taper-type versus parallel-type ramps. Costs of crashes and injuries were estimated using FHWA criteria. The benefit to safety was compared to the costs of upgrading the roadway segment and the estimated years to return was presented for each segment. Based on the analysis results, modifying the northbound entrance ramp at the Table Mesa TI and all four ramps at the Black Canyon City TI from taper-type to parallel-type is recommended.

4.11.2 Anthem Way TI (MP 229.1)

The Anthem Way TI provides the northern access to the Anthem community and is the southern limit of the Anthem Way to Black Canyon City widening. The TI was reconstructed in 2000 and I-17 was widened in 2010. The existing pavement is wide enough for three northbound and southbound lanes, although striping will need to be adjusted to eliminate the northbound lane drop and connect to the southbound lanes. Vertical clearances meet current guidelines. The project construction begins approximately 500 feet north of the TI.

4.11.3 New River TI (MP 232.0)

The New River TI is a diamond TI that was constructed in 1968 and serves the community of New River to the east. Other than bridge widening, the TI and ramps will not be affected by the mainline widening to the inside in this area. The existing vertical clearances under the northbound and southbound I-17 bridges are 19.9 feet and 15.9 feet, respectively. A horizontal curve on northbound I-17 begins just south of the TI



that separates the northbound and southbound horizontal alignments.

4.11.4 Table Mesa TI (MP 236.0)

The Table Mesa TI is located at MP 236.0 on I-17, approximately four miles north of the town of New River. Table Mesa Road provides access for a small number of residences and businesses east and west of I-17, including a ranch property about one mile east of the TI. East of I-17, Table Mesa Road becomes Forest Service Road 41, which extends to the Seven Springs area. To the west, Table Mesa Road runs toward Lake Pleasant Park. Both roads are unpaved.



Constructed in 1968, the Table Mesa TI is a trumpet-type interchange with southbound I-17 traffic exiting via a loop ramp and with diamond ramps on the east side of I-17. Table Mesa Road crosses above the I-17 mainline via separate structures over the northbound and southbound lanes. The northbound and southbound mainline roadways, both 38 feet wide, are separated by a 175-foot median consisting primarily of rock. Horizontal and vertical control for the northbound and southbound roadways are independent. The roadway profiles differ by as much as five feet through the TI area.

The TI ramps are not impacted by the mainline widening because it is to the inside in this area; however, as noted above, the northbound entrance ramp will be modified from a taper-type to a parallel-type ramp. The existing bridges will remain in place with the proposed widening. Lateral clearance beneath the bridges is deficient by approximately three feet; the shy distance to the guardrail/barrier will be reduced to accommodate the three-lane section. The barriers will be within inches of the columns; an SD 1.02 barrier with a structural foundation will be required. A design exception for the shoulder widths/shy distance will be requested.

According to recent bridge inspections, southbound I-17 at Table Mesa Road has a vertical clearance of 16.1 feet. Inside widening using the existing southbound I-17 cross slope would reduce the vertical clearance to approximately 15.75 feet at the face of barrier. Geometric and bridge structure constraints limit options to reduce vertical clearance impacts at this location. These include: (1) the positioning of the existing lanes and limited span length restrict widening to the inside and high side of southbound I-17, (2) southbound I-17 is on a horizontal curve with low existing superelevation such that reducing the cross-slope of the new lane to increase vertical clearance is not desirable, and (3) the existing Table Mesa bridge superstructure is integral with the pier columns, making raising the superstructure impractical. The reduced vertical clearance would be limited to the inside lane and inside shoulder. Unless the existing pavement section is deep enough to allow a profile change or a break in the cross slope is added, major roadway or bridge reconstruction would be required to provide the desired 16-foot vertical clearance at this location. A design exception may be needed.

4.11.5 Rock Springs TI (MP 242.2)

The Rock Springs TI provides access to Black Canyon City and Rock Springs. The TI configuration is a modified diamond interchange with the mainline crossing under the crossroad; the southbound entrance ramp connects to the two-way west frontage road approximately 3,600 feet south of the crossroad. The southbound entrance ramp is at the southern end of a commercial area, where traffic has the option to enter southbound I-17 or enter the two-way frontage/circulation road and return to the crossroad to travel northbound.



The TI and ramps are not impacted by the mainline widening, which is to the inside in this area. The northbound and southbound horizontal alignments become parallel near the Rock Springs TI, at approximately MP 242.1. From this point north to the Black Canyon City TI, the alignments are parallel with a 76-foot median.

The existing bridges are adequate and do not require widening or replacement. The vertical clearance to the bridges would be decreased as the proposed widening at the bridges is on the high side of the roadways. A break in the cross slope is recommended for the northbound and southbound lane widening so that the vertical clearance is not reduced. A design exception for the northbound vertical clearance will be requested.

4.11.6 Black Canyon City TI (MP 244.4)



The Black Canyon City TI marks the northern limit of the mainline widening and the southern limit of the flex lanes. The TI and ramps are not impacted by the widening to the inside in this area; however, the bridges will be widened and all four ramps will be modified to parallel-type ramps. Existing vertical clearances to the two-lane roadway below are 14.3 feet northbound and 14.7 feet southbound. Widening the I-17 bridges will reduce the southbound vertical clearance by 0.33 feet unless the crossroad profile is modified.

The flex lane facility connects to existing southbound I-17 approximately 1,000 feet north of the southbound exit ramp at the Black Canyon City TI; southbound vehicles in the flex lanes may not exit at Black Canyon City. Signage will indicate that flex lane drivers may not

exit at the Black Canyon City TI; however, extension of the flex lanes farther south should be considered during final design to eliminate potential weaving. Rumble strips or other measures to discourage/prohibit weaving could be added to the off-ramp gore. The average daily traffic at the Black Canvon City TI southbound exit ramp is 402 vehicles per day (2018).

4.11.7 Bumble Bee TI (MP 248.8)

The existing Bumble Bee TI is located approximately halfway up the Black Canyon Hill. The northbound and southbound roadways are separated by 1,375 feet, measured along the crossroad. Bumble Bee Road crosses above the existing southbound I-17 roadway and below northbound I-17.

Access will not be provided to the TI from the flex lanes. Flex lane signage along southbound I-17 at the top of the Black Canyon Hill will need to notify motorists to avoid the flex lanes if they intend to exit at the Bumble Bee TI. Similar signage will be required along northbound I-17 near Black Canyon City to notify northbound traffic that there is no access to the Bumble Bee TI from the flex lanes.

A new bridge is proposed to span the southbound I-17 lanes and the proposed flex lanes. The new bridge will be approximately 30 feet longer and 2.5 feet deeper than the existing bridge. To provide adequate clearance above southbound I-17 and the flex lanes, Bumble Bee Road will be reconstructed approximately 600 feet on both sides of the bridge. The raised profile is shown on Figure 10.

New Southbound Bridge

The northbound I-17 bridge is programmed for rehabilitation under a separate project. The existing Bumble Bee Road SB UP (#1170) bridge crosses southbound I-17 at a 60-degree skew such that the existing 120-foot middle span over the roadway provides only 57 feet clear between pier columns normal to the roadway.

The barrier-separated flex lanes proposed at this location require a curb-to-curb width normal to I-17 of 84 feet, not including barriers. Allowing for space to maintain the existing drainage swales and provide clearance behind the barriers requires a new span of approximately 200 feet with the 60-degree skew. The desire for future lane flexibility prevents the placement of a span-shortening pier along the separation barrier between the existing southbound lanes and the new flex lanes.

The 200-foot span is beyond the capabilities of typical precast prestressed girders. While post-tensioned cast-inplace concrete can provide long spans, southbound I-17 traffic requirements and construction duration considerations suggest a steel plate girder superstructure or a post-tensioned spliced girder bridge with the splice situated toward the east end of the bridge would be less disruptive to traffic during construction.

Either option will result in a substantially deeper superstructure and would require raising the profile of Bumble Bee Road. Efforts should be made to economize on structure depth in final design; however, a structure depth increase of 2 1/2 to 3 feet from the existing 5 1/2 foot depth can be expected.

A two-span bridge with an inverted-T straddle bent over I-17 is also an economical option that may reduce the structure depth increase; however, significant construction activities for the straddle bent construction and girder tie-ins to the straddle would occur over I-17, complicating I-17 maintenance and protection of traffic.







Staged construction options for bridge replacement are limited by the existing three girder end spans. Overbuilding and alignment shifts would require a significant horizontal realignment and reconstruction of Bumble Bee Road and the tie-in to the I-17 southbound ramp. Closing this cross road to remove the existing and replace with the new bridge at the same location would allow for a shorter construction duration with no staging, while minimizing approach roadway horizontal realignment.

The crossroad traffic is light and if closed to traffic, the detour is approximately eight miles for vehicles desiring to exit or enter from northbound I-17. Short term closure of southbound I-17 would also be required while girders are set; however, this can be accomplished with overnight closures and traffic rerouted through the southbound off and on ramps. A girder bridge with precast concrete deck forms can minimize construction time, cross-road closures, and nighttime I-17 closures for overhead work.

4.11.8 Sunset Point TI / Rest Area (MP 252.5)

The existing Sunset Point TI provides access to the Sunset Point Rest Area. The TI configuration is a modified diamond interchange with the mainline crossing over the crossroad; however, the southbound entrance ramp is located roughly 4,800 feet from the crossroad. The southbound entrance ramp is at the southern end of the rest area, where traffic has the option to enter southbound I-17 just north of the descent down the Black Canyon Hill or enter the two-way frontage/circulation road and return to the crossroad to travel northbound. The TI will not be affected by the flex lane construction.

Because the north flex lanes crossover is located close to the northbound exit ramp at the Sunset Point TI, insufficient weaving length is available and access cannot be provided from the flex lanes to the northbound offramp. Signage will indicate that drivers may not use flex lanes to exit at the Sunset Point TI. Rumble strips or other measures could be added to this off-ramp gore to further discourage/prevent weaving. Southbound entrance ramp traffic will be unable to access the flex lanes as the ramp enters I-17 south of the flex lanes southbound entrance.



4.12 Structures

4.12.1 Bridge Locations

The recommended alternatives will require replacement bridges or modifications to existing bridges at all existing crossing locations.

Between Anthem and Sunset Point, the proposed improvements will require two bridge replacements, at Moores Gulch SB (by others) and Bumble Bee SB, and ten bridge overpass or water crossing widenings. The relatively new bridge at Little Squaw Creek SB and underpasses at Mud Springs and the Rock Springs TI have sufficient clearance to accommodate I-17 widening. The Table Mesa TI UP can accommodate the widening underneath with the installation of ADOT SD 1.02 barriers to protect the pier columns and a design exception for reduced shoulder width.

4.12.2 Bridge Improvement Considerations

Vertical Clearances

ADOT bridge design guidelines call for a minimum vertical clearance of 16'-6" for new bridges and 16'-0" for existing bridges. Bridge widening on the low side or widening the roadway underneath a bridge can negatively impact vertical clearances. Bridge widening should not reduce vertical clearances below 16'-0". Existing overpass bridges at the New River TI SB, Black Canyon City TI NB and SB, and the Bumble Bee TI NB have existing vertical clearances of less than 16 feet.

Where typical widening would reduce clearances to below 16 feet, mitigation such as widening with a shallower structure depth than the existing girder bridges, cross-slope adjustments, introducing a cross slope break between lanes, or milling or reprofiling the roadway underneath should be considered.

In most cases for bridges over waterways, I-17 widening is to the high side of the roadway and will not impact freeboard. A minor 0.4-foot freeboard reduction is anticipated at the Little Squaw Creek NB bridge. If needed, a reduction in structure girder depths for the widened portion can mitigate any freeboard impacts.

Construction Considerations

Minimizing traffic disruptions along the corridor is a key requirement. Widenings will require some existing bridge removal to tie in to the existing. Removals will be kept to a minimum and will likely include removing the deck overhang to the exterior girder.

Widening will be to one side, either inside or outside, except for the Little Squaw Creek NB bridge, to limit structure removal and construction impacts to one side where practical. Partial widening on both sides of the existing Little Squaw Creek NB bridge is recommended to avoid the need to shift the existing roadway horizontal curve and helped to reduce approach roadway reconstruction costs.

Cast-in-place concrete will be avoided except for in-kind concrete slab bridge widening to avoid falsework over traffic and the horizontal and vertical clearance reductions that accompany falsework. Accelerated construction techniques and precast and prefabricated bridge elements can reduce construction durations and the accompanying traffic constraints.

Replacement structures at Moores Gulch SB (by others) and Bumble Bee TI UP SB will be replaced on the existing alignments to avoid the need for right-of-way and to minimize approach roadway reconstruction.

Structure Types

Structure types for bridge widenings will be primarily in-kind widenings of the same or similar structure type. The widened sections will be designed independent of the existing structure. In some cases, girder bridges may need to be shallower than the existing to maintain vertical clearances. This can be accomplished with more efficient or compact girder designs and possibly closer girder spacing. This is not an option with the slab bridges which are already quite shallow in structure depth.

For the new bridges at Moores Gulch SB and Bumble Bee TI UP SB, structure type is site dependent. The predominant economical structure type used in Arizona is a precast concrete girder bridge. Cast-in-place reinforced and post-tensioned concrete is also used frequently; however, the falsework requirements are a detriment to construction over active waterways, I-17 lanes, or busy cross roads.

Additional Improvements and Rehabilitation

Widened bridges will receive current ADOT standard crash-tested barriers. In addition, non-conforming barriers on the non-widened side of overpasses at the New River TI and Moores Gulch NB will also be upgraded to current standards.

Bridge widenings on existing bridges at the New River NB and SB bridges, with substandard or excessive AC overlay thicknesses, will have the existing overlays removed, and the existing bare concrete deck surface will be inspected and repaired if needed. The full widened deck surface will be sealed with penetrating deck sealant and re-overlaid with an appropriate asphaltic overlay.

Widened waterway crossings will require a reassessment of existing bank and scour protection measures in the design phase to determine if improvements or additional mitigation measures are warranted.

All existing concrete that will be removed or connected will need to be tested for asbestos. Steel girder bridges that are to be removed or repainted will need to be tested for lead paint.

4.12.3 Bridge Recommendations

The proposed improvements to the existing structures are summarized in the following tables:

TABLE 45 – ANTHEM WAY TO BLACK CANYON CITY OVERPASSES

| STR NO | l-17 MP | BRIDGE NAME | PROP RDWY WIDTH (Ft) | PROP DECK WIDTH (Ft) | EXIST RDWY WIDTH (Ft) | EXIST DECK WIDTH (Ft) | HORIZ CLEARANCE SURPLUS/ (SHORTAGE) | PROP BRIDGE IMPROV- MENTS | NEW BRIDGE AREA (SF) |
|-----------|------------|--------------------------------|-------------------------------|-------------------------------|--------------------------------|--------------------------------|--|------------------------------------|-------------------------------|
| 1290 | 231.4 | New River Bridge NB | 60.0 | 63.0 | 42.0 | 45.2 | (17.8) | Widen | 7,290 |
| 1291 | 231.4 | New River Bridge SB | 60.0 | 63.0 | 42.0 | 45.2 | (17.8) | Widen | 7,290 |
| 1292 | 232.0 | New River TI OP NB | 60.0 | 63.0 | 38.0 | 40.6 | (22.4) | Widen | 3,900 |
| 1293 | 232.0 | New River TI OP SB | 60.0 | 63.0 | 38.0 | 40.6 | (22.4) | Widen | 3,560 |
| 0967 | 238.2 | Moores Gulch Br NB | 60.0 | 63.0 | 38.0 | 40.6 | (22.4) | Widen | 4,980 |
| 0339 | 238.6 | Moores Gulch Br SB (by others) | 76.0 | 79.0 | 31.8 | 35.0 | (44.0) | Replace (by others) | 15,010 |
| 0968 | 239.2 | Little Squaw Creek Br NB | 60.0 | 63.0 | 32.5 | 35.6 | (27.4) | Widen | 11,820 |
| 2965 | 239.6 | Little Squaw Creek Br SB | 60.0 | 63.0 | 62.0 | 64.8 | 1.8 | None | 0 |
| 1807 | 243.3 | Agua Fria River Br NB | 60.0 | 63.0 | 42.0 | 45.2 | (17.8) | Widen | 7,990 |
| 1808 | 243.3 | Agua Fria River Br SB | 60.0 | 63.0 | 42.0 | 45.2 | (17.8) | Widen | 7,990 |
| 0764 | 244.4 | Black Cyn City TI OP NB | 60.0 | 63.0 | 38.0 | 43.2 | (19.8) | Widen | 2,240 |
| 0765 | 244.4 | Black Cyn City TI OP SB | 60.0 | 63.0 | 38.0 | 43.2 | (19.8) | Widen | 2,240 |

TABLE 46 – ANTHEM WAY TO BLACK CANYON CITY UNDERPASSES

| STR NO | I-17 MP | BRIDGE NAME | PROP RDWY WIDTH (Ft) | PROP WIDTH (Ft) | EXIST CLEAR WIDTH (Ft) | EXIST CLEAR LANE- STRUCT | PROP CLEAR LANE- STRUCT | HORIZ CLEARANCE SURPLUS/ (SHORTAGE) | PROP BRIDGE IMPROV- MENTS | NEW BRIDGE AREA (SF) |
|-----------|------------|--------------------------|-------------------------------|-----------------------|---------------------------------|-----------------------------------|----------------------------------|--|------------------------------------|-------------------------------|
| 2537 | 229.0 | Anthem Way TI UP | 60.0 | 63.0 | 90.5 | 24.8 (SB (Inside) | 22.5 (NB Inside) | 27.5 | None | 0 |
| 1294 | 235.9 | Table Mesa TI UP SB | 54.6* | 57.6* | 57.6 | 13.8 (Outside) | 7.8 (Inside) | 0.0 | None | 0 |
| 1295 | 235.9 | Table Mesa TI UP NB | 54.6* | 57.6* | 57.6 | 13.8 (Outside) | 7.8 (Inside) | 0.0 | None | 0 |
| 0969 | 242.2 | Rock Springs TI UP NB | 60.0 | 63.0 | 65.0 | 39.8 (Inside) | 27.8 (Inside) | 2.0 | None | 0 |
| 0970 | 242.2 | Rock Springs TI UP SB | 60.0 | 63.0 | 63.0 | 34.7 (Outside) | 33.0 (Inside) | 0.0 | None | 0 |
| 0863 | 243.0 | Mud Springs UP | 60.0 | 63.0 | 82.0 | 41.0 (Inside) | 29.0 (Inside) | 19.0 | None | 0 |

* Roadway shoulders and barrier offsets reduced to clear existing bridge columns. Roadway design exception is required.

TABLE 47 – BLACK CANYON CITY TO SUNSET POINT

| STR NO | l-17 MP | BRIDGE NAME | PROP RDWY WIDTH (Ft) | PROP DECK WIDTH (Ft) | EXIST CLEAR WIDTH (Ft) | EXIST RDWY WIDTH (Ft) | EXIST DECK WIDTH (Ft) | HORIZ CLEARANCE SURPLUS/ (SHORTAGE) | PROP BRIDGE IMPROV- MENTS | NEW BRIDGE AREA (SF) |
|-----------|------------|------------------------|-------------------------------|-------------------------------|---------------------------------|--------------------------------|--------------------------------|--|------------------------------------|-------------------------------|
| 1170 | 248.4 | Bumble Bee TI UP SB | 84.0 | 87.0 | 57.0 | NA | NA | (30.0) | Replace | 7,000 |
| 1171 | 248.4 | Bumble Bee TI OP NB | 38.0 | 40.3 | NA | 38.0 | 40.3 | NA | N/A | 0 |

4.12.4 New Bridges

New replacement bridges are recommended at the existing Moores Gulch SB (MP 238.6) (by others) and Bumble Bee TI UP SB (MP 248.4). The Bumble Bee bridge was addressed in a previous section.

Moores Gulch SB (#00339) (by others)

Replacement of the Moores Gulch SB bridge is currently in the ADOT five-year program, programmed for 2022 under a separate project. ADOT is using an outside consultant to design the bridge.

The existing southbound bridge at Moores Gulch was built in 1950, has only 32 feet clear width across the bridge for two existing freeway lanes, and has a low HS 16 Inventory Load Rating. The bridge also has an Operating Load rating of 49 tons which limits heavier permit vehicles access. To accommodate the added through lane, it would need to be widened 28 feet. These factors and the low current bridge Sufficiency Rating of 70.2 make it impractical and undesirable to widen the existing bridge.

Full bridge replacement is recommended. The intent is for the southbound I-17 widening to follow the existing I-17 alignment at this location. This requires a new bridge to be built at essentially the same location as the existing.

To maintain southbound I-17 traffic during construction the new bridge will need to be overbuilt, i.e., built wider than it needs to be for the final condition. While traffic is on the existing bridge, approximately 35 feet of the new bridge will be built alongside the existing. Once the first stage is complete, traffic can be shifted to the new bridge while the existing bridge is demolished and the remainder of the new bridge is constructed. This will require building a new bridge approximately 75 feet wide, or about 12 feet wider than required for the final condition.

A multi-span steel or precast prestressed concrete girder bridge would be appropriate for the southbound Moores Gulch crossing. Precast prestressed side-by-side boxes should also be considered as an approach to accelerate construction, although this type typically costs more. Cast-in-place concrete is generally not desirable for waterway crossings because of the need for falsework, even if the waterway is typically dry.

It is anticipated the new bridge span configuration would be similar to the existing, with a slightly longer threespan bridge length of approximately 190 feet. New substructure elements would be shifted from the existing to avoid conflicts with existing bridge piles left in-place. A detailed hydraulic analysis will confirm waterway opening requirements and may lead to adjustments of this configuration.

4.12.5 Retaining Walls

One retaining wall is anticipated for the Anthem Way to Black Canyon City segment, along with bridge abutment wingwalls associated with bridge widenings or replacements. A proposed retaining wall for the flex lanes is also

listed in Table 48. The retaining walls in the table are independent of bridge crossings. Bridge abutment wingwalls, required at each bridge abutment, are typical of each bridge and are not listed separately.

Key to the length and height of retaining walls is the close proximity of adjacent roadways with appreciably different profiles.

TABLE 48 – BLACK CANYON CITY TO SUNSET POINT WALLS

| STATION | LOCATION DESCRIPTION | LENGTH (FT) |
|--|---|-------------|
| 2295+00 – 2308+00 (Black Canyon City TI, NB Entrance Ramp) | Contain cut slope in ROW, support eroding cut slope and erosion. Additional flattening of the slope above the wall may be needed to increase stability. | 1,200 |
| 2330+00 - 2364+00 | Vertically separate flex lane facility and existing SB lanes | 3,400 |

4.13 ITS / Incident Management

ADOT's Intelligent Transportation Systems (ITS) requirements are outlined in its report, ITS Concepts for Rural Corridor Management, September 2007, and are now incorporated in the Statewide ITS Architecture. Section 3.1.5 outlines the Prescott District's main traffic management concerns [note that District lines were re-drawn; the project is now in the Northwest District]. These include interagency communications, real-time traffic monitoring for the I-17 corridor, traveler information systems, and weather forecasting to give the driver real-time accurate information. Section 3.2, Table 4, "Districts Needs Matrix," details what ITS components are identified as significant or minor needs. Mentioned, but not covered under the types of devices, was the District's desired installation of wildlife detection and monitoring systems.

The specific needs identified by the Northwest District that relate to the I-17 corridor are:

- Real Time Traffic Monitoring of I-17
- CCTV Monitoring
- Budgetary Funding for ITS Maintenance
- Wildlife Presence Detection
- Additional Roadway Weather Information Sites
- Flood Detection Sensors •
- Bridge Deck Icing Monitors
- Additional Dynamic Message Sign Locations ٠
- Portable DMS
- Good DMS Maintenance Service
- Multiple Agency Coordination for Traveler Information and Incident Response
- District-Wide Communications (Radio, Cell, Satellite Coverage)
- Improved Traveler Information
- Comprehensive AZ 511 System •
- Portable Speed Display Trailers and Photo Enforcement Programs •
- Highway Advisory Radio for Work Zones •
- Motorist Assist Patrols for Major Construction Projects

While many of these ITS needs are beyond the scope of this DCR, it is important to include a description or vision of the fully evolved ITS system so that ITS infrastructure elements can be included in future projects that will contribute to the long-term traffic management goals of the Department.

4.13.1 Recommended ITS Elements

The recommended ITS elements for the corridor are based on the ITS needs identified by ADOT Transportation Systems Management and Operations (TSM&O) Group and the Northwest District. The primary elements include:

- Real Time Traffic Monitoring
- CCTV Monitoring •
- Dynamic Message Signs •
- ITS Communications System and Power Distribution •
- Flex Lanes •
- Traveler Information Systems

Real Time Traffic Monitoring

Real time traffic monitoring is an important ITS element for incident detection and travel time data. Vehicle detection technology has evolved considerably over the past 20 years with the increased use of video, radar, and other non-intrusive detection devices. Some of these detection technologies have not proven to be as accurate as loop detectors under certain conditions. Other in-pavement or under pavement detection devices have also been tested by ADOT. Some of these technologies include wireless communications from the detector to the cabinet and from the cabinet to a communications hub. Other detection systems have been developed that use inductance footprint matching that can track vehicles throughout a corridor to provide very accurate travel time information, as well as the traditional spot speed and density data. Some private vendors have also developed systems that can report travel time data using a large pool of probe vehicles.

ADOT is currently getting real time traffic information through INRIX and this is envisioned by ADOT to be the primary traffic data source within the corridor going forward. The INRIX data will be supplemented by loop detectors at key locations between Black Canyon City and Sunset Point. The key locations are envisioned to include a location in advance of the flex lanes, as well as within the flex lane crossover areas for both the northbound and southbound directions.

CCTV Monitoring

CCTV cameras will be an important ITS element for accurate verification of incident location and type. This information is critical for appropriate and timely incident response. CCTV cameras should be installed to provide full coverage of the corridor within the project limits. CCTV cameras are typically installed at one mile spacing within the urban freeway corridors. For estimating purposes, camera spacing of approximately one mile has been assumed between Anthem Way and Black Canyon City. An additional eight cameras have been added to provide CCTVs on both northbound and southbound roadways where the roadways are bifurcated. There may be portions of the corridor between Anthem Way and Black Canyon City where power is not readily available to power cameras with a #2 AWG wire or smaller; within this portion of the corridor, larger spacings between CCTV would be acceptable.

Between Black Canyon City and Sunset Point, it is assumed that the southbound camera spacing will need to be one-half mile or less within the flex lane limits. The closer spacing of cameras within the flex lane limits is required to provide continuous coverage and clearance capability within the flex lanes. Cameras should be located at the flex lane entrances and exits north of the Black Canyon City TI and south of the Sunset Point TI.

The signing concept for the two flex lanes includes one additional DMS in each direction. The DMS are integrated with the advance static signing leading into the transition to the flex lane entrances. The DMS sign locations will allow the driver to select which lanes to use based on the latest travel time and incident information.

In the ultimate development of widening I-17 all the way to Cordes Junction, one DMS should also be located on northbound I-17 on the approach to Cordes Junction. Six to ten additional DMS should also be located outside the project limits to redirect traffic from the I-17 corridor to other routes such as SR 69, SR 87, SR 260, SR 89, US 93, and US 60 when road closures or long delay conditions occur along the I-17 corridor.

ITS Communications System and Power Distribution

DIRECTION

I-17 NB

I-17 SB

The ITS infrastructure should be a comprehensive communications system that is comprised of a combination of fiber optic cable, cell phone, and radio communications systems. The system should provide communications from all field equipment to the ADOT Traffic Operations Center via fiber communications, as well as to the Northwest District Maintenance Facility in Prescott Valley via radio communications or other wireless means.

The backbone of this system will be 3-3" conduits throughout the project corridor. The fiber optic backbone should consist of 144 strand fiber optic cables on each side of I-17 between Anthem Way and Black Canvon City and one 144 strand fiber optic cable along the southbound flex lane between Black Canyon City and Sunset Point. New communications nodes should be located near the New River TI, the Sunset Point Rest Area, and near the Cordes Junction TI. ADOT is starting to deploy communications nodes along rural corridors with a 20-25 mile spacing to accommodate future ADOT and DPS communications needs. The concept for the rural nodes is still under development internally between ADOT and DPS, but nodes may need to include towers for wireless

TABLE 49 – EXISTING DMS LOCATIONS

ADOT typically uses pan-tilt-zoom cameras with lowering devices powered by an AC power source. Electrical service is available at the Black Canyon City TI and the Sunset Point Rest Area. However, the availability of AC power throughout the corridor is problematic and larger wire sizes may be required to power all of the CCTV cameras within the flex lanes portion of the corridor. The power demand of the camera controls (pan/tilt/zoom) and communications equipment (ethernet switches, radios, and controllers) currently being used is at the upper range or higher than can be provided with standard ADOT solar power installations. This will be particularly important for the northbound I-17 CCTV locations, where the final design will have to rely solely on solar power since a conduit system will not be constructed along northbound I-17. Camera type, communications needs, power sources, solar panel size, battery storage, etc. will need to be carefully evaluated during the final design stage to identify the best CCTV camera and power source solutions for this segment of the corridor.

Dynamic Message Signs

Dynamic message signs (DMS) are an important Traveler Information System device to support incident management and communicate travel time information to the public. DMS have been installed along the I-17 corridor over the years, with the most recent installation occurring in 2017. Current DMS locations are listed in the table below.

is personnel to view the merge-diverge areas and the ns that provide full coverage of the corridor should be -17 between Black Canyon City, camera spacing has

| MILEPOST |
|----------------------------|
| 235.50, 242.71, and 251.90 |
| 252.83, 261.70, and 264.70 |



communications if existing DPS coverage is not available in that area, or if ADOT determines there is a wireless communication need that would require such a tower.

The wireless communications infrastructure within the limits of the flex lane installation is envisioned to provide point to point communications from each CCTV and detector location along northbound I-17 to a counterpart device located along the flex lanes, where the northbound devices will be tied into the fiber optic backbone. The fiber and wireless components should be a part of the flex lane project construction to ensure the communications with CCTV and detector stations are integrated with the field devices that are directly connected to fiber. For example, the CCTV and detectors along the new flex lane alignment are anticipated to be connected directly to the fiber communications network while most of the CCTV and detector stations along the existing northbound I-17 alignment are anticipated to be wireless links back to the fiber optic backbone. The ADOT TSM&O Group has expressed the desire that all devices in the corridor be IP addressable. The final communications system design should be developed for the entire corridor, taking into consideration phased construction of the projects within the corridor.

Flex Lanes

The flex lanes would connect to the existing northbound and southbound roadways near Black Canyon City and Sunset Point via slip ramps meeting ADOT design criteria for entrance and exit ramps. Dynamic message signs in advance of the flex lane entries would be added near Black Canyon City (northbound) and near Sunset Point (southbound) to alert drivers to the status of the flex lanes. See signing concept in Figure 11.

If current traffic patterns continue, the flex lanes would likely be used to carry northbound traffic on Fridays and Saturdays and southbound traffic on Sundays and holiday weekends. The lanes could be closed Monday through Thursday or they could remain open in the northbound direction to assist with accommodating higher traffic flows in the climbing section of the corridor. It is not envisioned that the direction of flow would be reversed on a frequent basis during the week unless construction activities or crashes warrant reversing the flow. The system would need to be flexible enough to be reversed in a relatively short amount of time if required.

Ideally, clearing the flex lanes for reversing the direction of flow would be an automated process. Gate open/closed positions would be changed automatically from the Traffic Operations Center and the flex lanes could be visually cleared by using CCTV cameras that provide continuous coverage of the entire flex lane length. If flow reversals happen during night time hours because of crashes, the roadway may need to be physically checked to make sure traffic is clear and there are no vehicles parked on the shoulder before switching directions.

The flex lanes will require ITS infrastructure above and beyond the requirements of the typical urban or rural ITS/FMS corridor in order to monitor and control the operation of equipment required to operate the flex lanes and meet the operational objectives for the flex lane.

ADOT TSM&O personnel have indicated their desire to have a robust ITS system within the area of the flex lanes. This robust ITS system is envisioned to include an automated gate control system at the entry to the flex lanes at Black Canyon City and Sunset Point TI, as well as numerous detector stations and CCTV cameras to assist with the clearance verification process when the lanes are being switched from one direction of travel to the other. Variable speed limit signs approaching and within the limits of the flex lanes could be used to adjust the posted speed limit based on monitored traffic conditions and speeds to promote a safer travel environment. The goal is to operate and clear the flex lanes with technology that is monitored at the ADOT Traffic Operations Center (TOC) rather than by manual/personnel-intensive methodologies (driving the corridor) due to the relative remoteness of the northbound and southbound entry locations from the Phoenix metropolitan area.

Gate control systems typically consist of four or more gates in each direction that allow the flex lane to be closed in one direction, cleared, and then reopened to traffic in the opposing direction. Typically, the first few gates have

fairly lightweight gate arms as they are more prone to being struck. The series of gates at the entry points would be designed to prevent cars from going the wrong way. Using a recent Florida project as an example, the initial gates should be well marked, with large, orange "Do Not Enter" signs suspended from the arm before the final steel gate arm. The last one or more gates are "hardened" gates designed to prevent traffic from entering the flex lanes and traveling in the wrong direction. Should the central control system or communications fail, the gates would remain locked in their position prior to the failure to prevent head-on collisions.

Clearance of the flex lanes can occur manually by having ADOT or DPS personnel drive the flex lane shortly after it is closed in one direction to visually confirm that there are no disabled vehicles within the flex lane limits. This is a time and labor intense process and an ongoing operational cost that would occur every time the direction of flow is reversed, and is therefore not viewed as the preferred operational concept, even though it would be expected to provide the highest degree of confidence that the flex lane is clear.

By contrast, clearance can be achieved through technology by using a combination of CCTV cameras and detector technology. These solutions require a robust communications network to be installed along the flex lane alignment such that the control cabinets can be connected to a fiber optic communications network. ADOT has begun designing fiber installations along interstates in rural locations (e.g., I-10 between Casa Grande and Picacho Peak) and ADOT TSM&O personnel have indicated a desire to ultimately have fiber along one side of I-17 all the way from Anthem Way to SR 69. It is expected that the fiber backbone will be constructed in phases as projects are developed.

The use of CCTV cameras to visually clear the flex lanes is one aspect of technology that is expected to be deployed. Full 100% visual confirmation of the flex lane corridor is desired by TSM&O personnel. The existing terrain and horizontal curvature would significantly increase the number of CCTV cameras required to provide full coverage. In addition, cameras are an essential component of the automated gate system for verification of gate closure, as well as in advance of each DMS location for message verification. There are several key constructability concerns with deploying a significant number of CCTV cameras along the flex lanes, primarily the lack of available power sources along the corridor, as well as the subsurface soil conditions at the CCTV locations. Additional geotechnical investigation and special CCTV foundation designs will likely be required at some CCTV locations within the flex lane section.

Other types of technology such as license plate recognition systems, similar to what are used on tolling systems, could also be considered for clearance. Final selection of technology will be determined during final design, as new, more reliable technologies could be developed by the time the flex lanes are designed and constructed.

Traveler Information Systems

Traveler information systems come in many forms. It is envisioned that one or more of the ITS capabilities included in the recommended project will require an expansion and refinement of the ADOT Traveler Information System including extensive use of the AZ 511 System, connected vehicle applications such as dedicated shortrange communications, improved travel information distributed to television and local radio stations, and especially to traffic conditions and navigation apps on mobile devices. The ADOT Communications office, which is responsible for public and media outreach, is a good resource to assist with the preparation of clear and concise messages. These systems will be particularly important during the construction phases of the various projects in this corridor.

4.13.2 Incident Management

The following sections describe the incident management scenarios that are anticipated based on assumed incident locations within the corridor.

Anthem Way to Black Canyon City

Scenario 1: For incidents between Anthem Way TI and New River TI, northbound and southbound traffic would be rerouted to the Anthem Way TI or the New River Road TI via the frontage road. Traffic trapped between the Anthem Way TI and the New River TI would remain until allowed to pass the incident safely under the direction and traffic control measures by ADOT and DPS. The wider proposed roadway would provide the width to bypass many incidents with 56 feet (3-12 foot lanes, 2-10 foot shoulders) of pavement.

Scenario 2: For incidents north of the New River TI, the traffic would not be rerouted but would remain until allowed to pass the incident safely under the direction and traffic control measures by ADOT and DPS. The wider proposed roadway would provide the width to bypass many incidents with 56 feet (3-12 foot lanes, 2-10 foot shoulders) of pavement.

Black Canyon City to Sunset Point

I-17 from the Black Canyon City TI to Sunset Point is a steep roadway that travels up the Black Canyon Hill. Incidents on this segment have been responsible for many hours of delay to the traveling public because of crashes and the lack of alternate routes on which to reroute traffic around incidents and maintenance activities. The existing northbound and southbound alignments are bifurcated with substantial elevation differences.

The current two-lane roadway configuration does not provide flexibility for routing traffic around crashes. Crossing traffic over to the opposing lanes, then back again past an incident is not possible. The reduction from two lanes to one lane in the direction opposite to the incident causes operations on that segment of roadway to fail as well. A full road closure is frequently required for hazardous material incidents or a fatal crash that blocks the roadway.

Sample incident management scenarios have been developed to address how traffic could be routed around incidents within specific roadway segments.

Potential Scenarios and Responses - Black Canyon City to Sunset Point (Flex Lanes) Scenario 1: An incident occurs in the northbound direction on the existing northbound roadway. Traffic would begin to queue on the Black Canyon Hill. ADOT's traffic monitoring system would measure a slowing of traffic speed, alerting ADOT of a problem. After video verification and confirmation from DPS, the Traffic Operations Center would direct approaching northbound traffic by posting a message on the dynamic message sign south of Black Canyon City to stay left and use the northbound flex lanes.

Scenario 1A: Incidents in the northbound direction on the existing northbound roadway north of the Bumble Bee TI would follow a similar strategy except traffic could be turned around at Bumble Bee TI and rerouted south to the Black Canyon City TI, where the traffic would turn around and proceed northbound using the northbound flex lanes under traffic control measures by ADOT and DPS. Traffic trapped between the Bumble Bee interchange and the incident would remain until it was allowed to pass the incident safely.

Scenario 1B: Incidents in the northbound direction on the existing northbound roadway south of the Bumble Bee TI would require that northbound traffic be routed to the northbound flex lanes at Black Canvon City. Traffic trapped between the Black Canyon City interchange and the incident would remain until it was allowed to pass the incident safely. Motorists who desire to access Bumble Bee Road would be routed north to the Sunset Point TI, where they would turn around and proceed south to the Bumble Bee TI.

Scenario 2: An incident occurs in the southbound direction on the existing southbound roadway. Traffic would begin to queue on the Black Canyon Hill. ADOT's traffic monitoring system would measure a slowing of traffic speed, alerting ADOT of a problem. After video verification and confirmation from DPS, the Traffic Operations

Center would direct approaching southbound traffic by posting a message on the dynamic message sign north of Sunset Point to stay left and use the southbound flex lanes.

Scenario 2A: Incidents in the southbound direction on the existing southbound roadway south of the Bumble Bee TI would follow a similar strategy except traffic could be turned around at Bumble Bee TI and rerouted north to the Badger Springs Road TI, where the traffic would turn around and proceed southbound using the southbound flex lanes under traffic control measures by ADOT and DPS. Traffic trapped between the Bumble Bee interchange and the incident would remain until it was allowed to pass the incident safely.

Scenario 2B: Incidents in the southbound direction on the existing southbound roadway north of the Bumble Bee TI would require that southbound traffic be routed to the southbound flex lanes at Sunset Point. Traffic trapped between the Sunset Point interchange and the incident would remain until it was allowed to pass the incident safely. Motorists who desire to access Bumble Bee Road would be routed south to the Black Canyon City TI, where they would turn around and proceed north to the Bumble Bee TI.

Scenario 3: For incidents within the new flex lanes alignment, existing northbound or southbound traffic would not be rerouted but would remain until allowed to pass the incident safely under the direction of and traffic control measures by ADOT and DPS.

The final designer should consider whether there are opportunities to provide emergency access through the barrier between the southbound lanes and flex lanes to allow evacuation of the lanes or to provide access to emergency vehicles.

4.14 Constructability and Traffic Control

4.14.1 General

Existing highway movements and access must be maintained during construction. Because there are no convenient alternate routes, closure of Interstate 17 will not be allowed other than for short periods of time. Final construction sequencing/phasing will be determined during final design. Traffic will be managed using detailed traffic control plans and by procedures and guidelines specified in the current edition of the Manual on Uniform Traffic Control Devices and the current ADOT Traffic Control Design Guidelines.

Major construction activities that disrupt traffic are to be performed during off-peak hours. Efforts to minimize the duration of construction should be made during final design. Existing freeway movements and access to and from TIs must be maintained during construction. Other methods of reducing traffic impacts during construction, such as phasing the improvements so the entire length of the project is not under construction at one time, will be evaluated during the final design phase of the project.

Contractual incentives should be considered to minimize closure durations and facilitate traffic flow during construction. Examples of methods used successfully on other projects include the following:

- Travel-time incentives
- Motorist assist patrol to help stranded motorists •
- Lane rental, with a higher cost for peak-hour closures
- Variable message signs
- Highway conditions reporting system
- Major public outreach campaign

The construction and phasing of the Anthem Way to Black Canyon City construction can likely be accomplished in one phase. This phase will include widening to the inside (or outside in one southbound segment) along the freeway. To maintain traffic during this phase of construction, the width of the inside shoulder may be reduced, but a useable (10-foot) right shoulder must be maintained. Temporary concrete barrier is recommended to protect the work area from freeway traffic.

Construction of the flex lanes could be a separate construction project or a separate phase of one overall project; the flex lanes will likely be constructed in one phase.

Replacement of the Bumble Bee TI UP bridge will require a detour and short-term southbound I-17 closures. Traffic can be detoured through the existing southbound ramps when required. The use of precast superstructure elements can limit the mainline closures and detours to primarily overnight closures. With a small shift in the Bumble Bee Road alignment over southbound I-17, staged bridge construction may allow for the maintenance of traffic on Bumble Bee Road and access to northbound I-17 except for short-term closures. Shifting the Bumble Bee Road alignment would be complicated by the mountainous terrain and large rock formations. If staged bridge construction or shifting the cross road alignment to maintain access during bridge reconstruction isn't feasible, northbound traffic accessing Bumble Bee Road will be detoured north to the Sunset Point TI and turned around. While this seven-mile detour would be inconvenient, traffic volumes are low at the Bumble Bee Road northbound exit at 147 vehicles per day (2018).

Constructability and traffic control issues have been identified for the recommended alternatives as follows:

Earthwork

 Earthwork haul routes can have a considerable impact on construction zone traffic control and to facilitate the hauling activities.

Bridge Construction

- One structure (Bumble Bee Road) would be re-constructed over an existing roadway; other during the closure.
- Table Mesa TI Underpass bridges provides a horizontal clearance of 57 to 58 feet. The proposed clearance to divert the two new flex lanes through the end span opening.

4.15 Utilities

During final design, each utility company will receive and review the preliminary design for this project and develop plans for any relocations and/or adjustments.

construction zone congestion. It may be beneficial to require the contractor to submit a haul route design tailored to their specific equipment and its capabilities. At locations where the haul route would use existing or proposed structures, the load capacity of the structure must be identified and adhered to by the haul vehicles. It may be necessary to design some of the new structures as overload structures

overcrossing structures will be widened. All of the crossings can be constructed in stages to maintain I-17 traffic with lane shifts and short-term mainline traffic diversions through the off/on ramps. Cross road closures can be limited to overnight using precast superstructure elements. Accelerated bridge construction (ABC) techniques have also been used successfully to deliver bridge replacement over the course of a weekend closure. This would require that mainline traffic be shifted to the off/on ramps

widening of the existing I-17 roadways will require a 63-foot horizontal clearance. Bumble Bee TI SB Underpass bridge will require 87 feet of horizontal clearance to accommodate the new flex lanes. The bridge currently provides 57 feet of clearance and the short end spans do not have adequate lateral

Based on as-built plans, plans supplied by the utility companies, and the conceptual plans developed for I-17 as references, it is anticipated that utility relocations and adjustments will be necessary. The table below summarizes various utility crossings, many of which will not be directly impacted, but they should be noted and conflicts determined during final design.

| Туре | Owner | Location | Disposition | Other |
|--------------------------------------|----------------------------|--|-------------------------------------|---|
| Gas | Southwest Gas | SB Sta 1656+00 NB Sta1657+00 | No impact likely | |
| Overhead Power | APS | SB Sta 1671+00 NB Sta 1671+00 | No impact likely | Vertical clearance approximately 25' |
| Overhead Power | APS | Along east side of NB NB Sta 1875+00 to Sta 1883+00 Crosses SB Sta 1883+00 | No impact likely | Vertical clearance approximately 25' |
| Gas | El Paso Natural Gas | NB Sta 2054+00 SB Sta 2012+50 | No impact likely | |
| Fiber Optic | ATT | NB Sta 2052+50 SB Sta 2011+50 | No impact likely | |
| Overhead Power | APS | Along west side of SB SB Sta 2065+00 to Sta 2165+00 | One pole impacted at Sta 2070+00 | |
| Overhead Power and Fiber Optic | APS/ATT | NB Sta 2201+75 SB Sta 2202+00 | No impact likely | Vertical clearance approximately 25' |
| Water | Black Canyon City Water | NB Sta 2201+75 SB Sta 2202+00 | No impact likely | Line is adequately deep, valves should be located during final design |
| Gas | El Paso Natural Gas | NB Sta 2204+50 SB Sta 2204+50 | No impact likely | |
| Water | Black Canyon City Water | NB Sta 2213+50 SB Sta 2213+50 | No impact likely | Line is adequately deep, valves should be located during final design |
| Water | Black Canyon City Water | NB Sta 2225+00 SB Sta 2223+75 | No impact likely | Line is adequately deep, valves should be located during final design |
| Water | Black Canyon City Water | NB Sta 2232+00 SB Sta 2232+00 | No impact likely | Line is adequately deep, valves should be located during final design |
| Overhead Power | APS | SB Sta 2429+75 | No impact likely | One pole 30' away from outside edge of pavement |
| Gas | El Paso Natural Gas | SB Sta 2430+00 | No impact likely | |

TABLE 50 – PRELIMINARY UTILITY CONFLICTS

No impacts are expected to any Western Area Power Administration 345 kV transmission lines or towers.

A 42-inch Transwestern natural gas pipeline runs along the west side of I-17 from Black Canyon City northwest through the Bumble Bee Valley, then northwesterly toward Prescott.

New roadway lighting will be designed at the south and north crossover points for the flex lanes. It is anticipated that existing lighting services will be modified/upgraded to accommodate the additional lighting that will be added.

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ITS electrical services will be needed to support ITS equipment installations throughout the entire flex lane corridor for DMS, CCTV, and detection. It is expected that new ITS electrical services will be required near the locations of the existing lighting load centers at the far west side of the Black Canyon City TI and within Sunset Point Rest Area. Additional electrical services and load centers would be desirable at one or more locations between MP 244 and MP 252 to decrease the conductor size that would be required to run power to ITS equipment within the corridor. There is a power line overcrossing north of MP 247 that may be a potential electrical service point. The power company will be contacted during design to determine if this or additional electrical service points are available along the corridor.

The 2017 Safety Improvements project installed new ITS electrical services for DMS along northbound I-17 south of Table Mesa Road (MP 235.50), and south of Black Canyon City (MP 242.71). New ITS electrical services for DMS were installed along southbound I-17 near MP 252.83.

4.16 Signing and Pavement Marking

The roadway widening between Anthem Way and Black Canyon City will require the relocation of any existing warning, marker, or regulatory sign impacted by the widening, as well as the installation of new pavement marking along both the southbound and northbound alignments due to proposed milling and replacing AR-ACFC. At the project termini, an existing lane line and edge line will need to be restriped to properly tie into the existing lane addition in the southbound direction and tie into the existing lane drop in the northbound direction. Where inside widening occurs along the northbound and southbound alignments a new lane line and inside edge line will need to be installed.

The two-lane flex roadway facility between Black Canyon City and Sunset Point will require the relocation of any existing warning, marker, regulatory or guide sign impacted, as well as the installation of new warning, marker, and regulatory signs along the median side of road for drivers traveling in either direction along the flex lane alignment. Signing to indicate which shoulder should be used for emergencies will be included on the flex lanes. The installation of new post-mounted warning signs and overhead guide signs mounted on sign structures will also be required at the north and south crossover areas to inform drivers of the flex lanes. A proposed signing concept for these signs is shown in Figure 11. The FLEX LANES ENTRANCE 1 MILE advance guide sign for the southbound direction is located north of Sunset Point Road. It is recommended that this sign be installed in the median between Station 2728+00 and 2735+00 to avoid potential conflict with culturally significant areas. No access to Bumble Bee Road will be provided for drivers within the flex lanes. Because of the proximity of the flex lane merge point with I-17 in relation to the Sunset Point and Black Canyon City exits, insufficient weaving lengths are available and access cannot be provided from the flex lanes to the adjacent ramps. Therefore, a "NEXT EXIT XX MILES" plaque will be added to the "FLEX LANES ENTRANCE 1 MILE" advance guide signs to inform the drivers entering the flex lanes that no exits are available within the flex lane section.

New pavement marking at the crossover areas in the form of edge lines, lane lines, gore lines, and skip stripes will need to be installed. The crossover areas should also utilize raised pavement markers (RPM) that maintain red reflective markings on the back side of the RPM, as well as wrong-way pavement arrows, to better inform drivers of the correct direction of travel. Due to the different possible directions of travel along the flex roadway, both edge lines should be solid white instead of maintaining a white and a vellow edge line.

All new signing and pavement marking will be designed in accordance to ADOT's Signing and Marking Standards.

4.17 Lighting

Existing continuous lighting along I-17 ends south of the project limits at the Carefree Highway TI (MP 224); therefore, continuous lighting along I-17 between Anthem Way and Sunset Point is not recommended.

The crossovers for the two-lane flex roadway facility between Black Canyon City and Sunset Point are unique conditions, not specifically addressed by the AASHTO Roadway Lighting Design Guide, October 2005, which provides information on roadway lighting warranting conditions for rural interchanges but does not specifically address the type of roadway geometry created with the introduction of a two-lane flex roadway facility. The Guide does indicate that the installation of a few lights at the point of on- or off-movements could contribute to driver ease by providing visual indications of the maneuver areas. Lighting also improves the drivers' ability to see roadway geometry and other vehicles at extended distances ahead. For this reason, partial interchange-type lighting system is recommended to illuminate the crossover merge and diverge areas just north of the Black Canyon City TI and south of the Sunset Point TI. The partial lighting should cover the travelled way from the beginning or ending point of taper on the mainline to a point between 50 feet and 150 feet beyond the back of gore as shown in Figure 15c of the ANSI/IES RP-8-14 Roadway Lighting guide. The average maintained horizontal illuminance should be a minimum of 0.6 foot-candles with an average to minimum uniformity ratio of 4.0:1 or better.

Between Anthem Way and Black Canyon City, the TIs at Anthem Way, New River Road, Rock Springs, and Black Canyon City employ partial lighting to illuminate the points of conflict where the ramps merge and diverge from I-17; however, the Table Mesa Road TI does not currently have any lighting. All proposed roadway widening at the interchanges between Anthem Way and Black Canyon City is to the inside of the existing roadway; therefore, the existing partial lighting along this project segment will not be impacted.

North of Black Canyon City, the TI at Sunset Point employs partial lighting to illuminate the points of conflict where the ramps merge and diverge from I-17; however, the Bumble Bee Road TI does not currently have any lighting. The partial lighting at the southbound entrance and northbound exit ramps for the Sunset Point TI may need to be modified due to the additional lighting for the north flex lane roadway crossover. If modification is necessary, the partial lighting should cover the travelled way from the beginning or ending point of taper on the mainline to a point between 50 feet and 150 feet beyond the back of gore as shown in Figure 15c of the ANSI/IES RP-8-14 Roadway Lighting guide. The average maintained horizontal illuminance should be a minimum of 0.6 foot-candles with an average to minimum uniformity ratio of 4.0:1 or better.

Light Emitting Diode (LED) luminaires with a correlated color temperature of 3,000k and zero uplight should be used on this project to be in accordance with the Dark Skies recommendations.

4.18 Landscape and Aesthetic Considerations

This section establishes design criteria for the landscape and aesthetics documents to be prepared by the final designer for the corridor to adequately address the impacts of the roadway improvements on these resources. Preparation of aesthetic and landscape concepts, plans, details and special provisions should be a collaborative effort involving ADOT technical disciplines, BLM, municipal stakeholders, and the final designer. The final design scope should consider the specific submittal requirements, approvals and processes with the objective to

mitigate undesirable impacts to the natural and visual quality of the I-17 project impacts using careful planning and design of ground treatments, native planting, structures rustication and paint, and slope treatments.

4.18.1 Guidelines and Predesign Resources

Landscape and aesthetics developed in final design should consider findings detailed in this DCR, mitigation measures, and supporting documents and reports. Additionally, previously-developed guidelines that are applicable to work within the project area such as the ADOT *Guidelines for Highways on Bureau of Land Management and Forest Service Lands* and *Supplement to Guidelines for Highways on Bureau of Land Management and Forest Service Lands* should be reviewed.

4.18.2 Planting Design: Objectives and Biozone Character Areas

Planting design themes should be developed through collaboration with ADOT Roadside Design Section (RDS) to develop Character Areas (CA) defining the plant palette(s), density requirements, and salvage and replanting objectives based on planting biozones. Broad objectives for the character areas should consider development growth patterns, vegetative buffers to screen views both from and to the roadway, strategic gaps to frame positive views, measures to blend disturbed areas into their surroundings, and transplant large saguaros, mature trees, and cacti to visually sensitive and critical roadway areas.

Plant Density: Urbanized planting density should be established at rates appropriate for the impacts caused by disturbance to the existing I-17 corridor, development growth patterns, and project goals as determined by ADOT and the final designer. Rural planting density should be determined by a review of the Native Plant Inventory of recommended salvageable plants by the final designer and ADOT RDS staff. The native plant density should be applied to the plantable disturbance acreage in determining the density requirements.

Soil Amendments and Agronomy Testing: The final designer should conduct agronomic soil fertility and nutrient soils testing throughout the project ROW to determine topsoil plating and prepared soil requirements. Soil sampling should occur for suitability as a planting medium for landscaping and native seeding to develop preliminary soil amendment recommendations. Samples should occur at one-mile increments within the project ROW in disturbance areas.

4.18.3 Native Plants and Seeding

The native plants surrounding the I-17 corridor are a significant resource that provide soil stabilization and wildlife habitat, and act as visual interest. During final design, efforts should be made in areas of disturbance to salvage and replant suitable species: young and healthy *Carnegia gigantea* (Saguaro 12-20 feet in height), *Ferocactus fishhook* (Barrel Cactus), and *Olneya tesota* (Ironwood), etc. Revegetation efforts in should consider the elevation of salvaged material when identifying disposition of replanted salvaged material.

Native Plant Inventory: Prepare a native plant inventory of all saguaros, barrel cactus, ocotillos, and all healthy native trees within the disturbance areas meeting the requirements of the ADOT Native Plant Salvage and Replanting Guidelines. A Salvage Operations Plan should detail all used processes, methods, equipment, and materials for plant salvage, nursery set-up and operation, and replanting of salvaged plants.

Native Seeding: All disturbed soils not paved, otherwise landscaped, or permanently stabilized by construction should be seeded using native species to the project vicinity. The various elevations, soil conditions, and drainage considerations may require that several seed mixes to be developed. Examples of project specific seed mixes includes Low Grass & Forbs, Tall Background, and Wash Seed Mixes. Additionally, clear zone and background seed mixes may be needed. The final designer should coordinate with ADOT RDS staff to prepare Seeding Special Provisions.

4.18.4 Noxious and Invasive Species Control Plan

A Noxious and Invasive Species Control Plan (NISCP) will be required to assist with controlling noxious and invasive plant species within the project area. The work under the NISCP shall consist of the detection and eradication of noxious and invasive plants. Proposed method(s) of noxious plant control include either manual eradication or herbicide application by recommended methods for each plant species identified in the NISCP and will be in accordance with NEPA and state statutes. The project area will be surveyed following rain events and during plant germination and growth periods prior to and during construction, as well as post-construction activities. Construction best management practices will include items of operation that may minimize the spread of noxious species. The NISCP shall also include post-construction measures to prevent invasive species seeds from leaving the site.

4.18.5 Irrigation System Design: Permanent and Temporary Systems

Permanent irrigation should be considered in urbanized areas planted with nursery and salvaged plants where potable water exists in adjacent municipal rights-of-way. Use of a temporary irrigation system should be considered for rural areas with salvaged and replanted landscaping and areas where no potable water exists. The final designer should coordinate with ADOT to develop performance criteria of temporary irrigation systems in the special provisions. No irrigation would be required for native seeding.

4.18.6 Aesthetics: Objectives and Corridor Aesthetic Areas

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The objectives for aesthetics should include minimizing the impact of structures on the viewers' attention through use of paint, rustication, and low-profile design of structures. The final designer should collaborate with ADOT RDS to establish Aesthetic Areas (AA) defining the aesthetic theming for each of the selected characteristics occurring within the I-17 corridor. Each AA should define the paint palette(s), rustication requirements, and aesthetic concepts and patterns.

Structures Rustication: The final designer should coordinate with ADOT RDS to develop rustication designs that may vary from Hohokam symbols and patterns to simulated rock that resembles the strata and fracture qualities of the native rock. Drainage structures and headwalls are exempt from rustication. Structure elements that should be considered for rustication include:

New Bridges:

- Abutment/Wingwalls
- Barriers (non-traffic side) Light Blisters

- Walls:
- Noise Barrier

Piers

- Lightweight Noise Barrier
- Retaining

Fencing and Guardrail: Refer to ADOT *Guidelines for Highways on Bureau of Land Management and Forest Service Lands* and *Supplement to Guidelines for Highways on Bureau of Land Management and Forest Service Lands* and Special Provisions in final design for requirements for fencing and guardrails treatments.

Paint/Color Treatment: Paint all new and modified structures and walls to blend with the surrounding native vegetation and landscape. Assess existing structures to determine if existing conditions meet the AA objectives. Color selection should be coordinated with ADOT during Final Design and may include separate colors for each AA.

4.18.7 Slope Stabilization, Erosion, Sediment, and Stormwater Quality Control

Stabilization Goals: Minimizing dust and erosion of soils by wind and water and weed control are the primary goals of stabilization. Stabilization in urban areas is intended to enhance back-of-curb roadway areas with consistent color and gradation of rock for a clean, weed free appearance. For rural areas the salvaged surface soils is intended to blend with existing background and minimize the impact of the roadway disturbance. Inert materials plans should be identified during final design to document the placement locations, types, and colors of granite mulch, decomposed granite, and salvaged soils throughout the project area within the limits of disturbance.

Inert Materials and Salvaged Surface Soils:

Urbanized Areas: Inert materials consisting of granite mulch, 1 ¹/₄" minus. Color(s) should be determined by CA in Final Design.

Rural Areas: Salvaged surface soils approximately the native desert ground color found in adjacent undisturbed areas. The final designer should inventory the existing conditions within areas to be disturbed to determine the types of desert pavements that could be matched or reused within the project area. If used, salvaged soils should be taken from onsite source(s) prior to roadway construction activities, stored, and then placed in geographic regions similar to the location where the material was harvested.

Rock and Slope Treatments and Techniques: The final designer and ADOT will develop a strategy to mitigate the visual impacts to rock cut slopes. It will be necessary to review the Geotechnical reports, roadway design, and right-of-way plans to determine the appropriate measures on a case by case basis. Provide the selected rock treatment techniques in the landscape details.

Techniques for rock slope mitigation include:

- rock sculpting,
- cut and fill slope warping,
- slope rounding,
- varied slope ratios,
- false cuts,
- rock staining.

Erosion, Sediment and Stormwater Quality Control: Both construction and post construction erosion control measures should be prepared by the final designer and coordinated with ADOT to establish the plan requirements for the erosion control plans that serve as part of the stormwater pollution prevention plan.

4.19 Transit Considerations

In 2010, ADOT prepared a statewide transportation plan that formulated and evaluated roadway, public transit, and rail improvements. The resulting BQAZ Statewide Transportation Planning Framework Program is a vision for the State of Arizona that recommends a comprehensive 2050 transportation scenario.

The BQAZ plan recommends I-17 as a route for intercity buses. Because of the steep terrain in the project area, with four to six percent existing and proposed roadway grades on the Black Canyon Hill, passenger rail facilities between Phoenix and Flagstaff would be precluded from utilizing the I-17 corridor and instead would be routed along gentler terrain to the west. The BQAZ plan recommends that passenger rail be routed from Phoenix to

Wickenburg, northward following an existing railroad route west of Prescott to Ash Fork, then east to Williams and Flagstaff.

4.20 Recommendations from Other Studies

Recommendations from the May 2007 Road Safety Audit, I-17 Southbound Black Canyon Hill, Sunset Point to Black Canyon TI, should be implemented where feasible. Some of these recommendations were implemented with the I-17 Black Canyon Hill (SB) project (017 YV 245 H6368 01C; IM-HES-017-B(007)A); others may be included in this project. Recommendations include improvements to sight distance, adding rumble strips and delineators, replacing guardrail with 42-inch tall concrete barrier, and improving/increasing signs and pavement markings.

ADOT prepared a planning-level Corridor Profile Study for Interstate 17 in 2017, extending from SR 101L in Phoenix to I-40 in Flagstaff. The recommendations were identified based on pavement, bridge, mobility, safety, and freight; several of the corridor profile study's high-priority recommendations coincide with the recommendations in this DCR.

4.21 Design Exceptions

Non-conforming features will be upgraded as part of this project to meet current standards as noted in Chapter 5. Design exceptions and design variances will be requested for the remaining non-conforming features.

The existing roadway geometry includes horizontal curves with limited sight distance. Modifications to the existing horizontal geometry are generally not recommended because of funding limitations and impacts to traffic during construction.

There are a number of existing curves where the superelevation does not meet current design criteria. Modifications to the existing superelevation rates were evaluated but are generally not recommended as detailed in the following section and the design exception request letter.

4.22 Safety Study

A safety study was completed for I-17 from Anthem Way to Sunset Point. The purpose of the study was to analyze crash data to determine crash patterns by location, type of crash, roadway characteristics, interchange type, and circumstance of the crash which would lead to potential countermeasure identification. The limits for the study included I-17 from MP 229 to MP 245, both northbound and southbound, and from MP 245 to MP 253, southbound only.

Safety data is subject to the provisions of 23 USC § 409. Any intentional or inadvertent release of this material, or any data derived from its use, does not constitute a waiver of privilege pursuant to 23 USC § 409.

Five years of crash data was collected for I-17 within the study limits from January 1, 2013 to December 31, 2017. In the northbound direction between MP 229 and MP 245, a total of 412 crashes occurred. These crashes are summarized based on crash severity and manner of collision in Table 51 and Table 52, respectively. In the southbound direction between MP 229 and MP 253, a total of 615 crashes occurred. These crashes are summarized based on crash severity and manner of collision in Table 53 and Table 54, respectively.

| Crash Severity | 2013 | 2014 | 2015 | 2016 | 2017 | Grand Total | Percentage |
|--------------------------|------|------|------|------|------|----------------|------------|
| Fatal | 1 | 1 | - | 2 | 1 | 5 | 1.2% |
| No Injury | 48 | 41 | 63 | 51 | 78 | 281 | 68.2% |
| Possible Injury | 9 | 8 | 9 | 8 | 12 | 46 | 11.2% |
| Suspected Minor Injury | 10 | 10 | 14 | 16 | 12 | 62 | 15.0% |
| Suspected Serious Injury | 5 | 2 | 3 | 3 | 5 | 18 | 4.4% |
| Total | 73 | 62 | 89 | 80 | 108 | 412 | 100.0% |

Table 52 – Northbound MP 229 to MP 245, Crashes by Collision Manner

| Collision Manner | 2013 | 2014 | 2015 | 2016 | 2017 | Grand Total | Percentage |
|--|------|------|------|------|------|----------------|------------|
| Angle (Front to side) (Other than left turn) | 1 | - | - | - | - | 1 | 0.2% |
| Head On | - | 1 | 1 | 1 | - | 3 | 0.7% |
| Other | 1 | 1 | 1 | 1 | 3 | 7 | 1.7% |
| Rear End | 19 | 18 | 29 | 23 | 47 | 136 | 33.0% |
| Sideswipe (Opposite Direction) | 1 | - | 1 | 1 | - | 3 | 0.7% |
| Sideswipe (Same Direction) | 8 | 6 | 7 | 13 | 12 | 46 | 11.2% |
| Single Vehicle | 43 | 36 | 50 | 41 | 46 | 216 | 52.4% |
| Total | 73 | 62 | 89 | 80 | 108 | 412 | 100.0% |

Table 53 – Southbound MP 229 to MP 253, Crashes by Severity

| Crash Severity | 2013 | 2014 | 2015 | 2016 | 2017 | Grand Total | Percentage |
|--------------------------|------|------|------|------|------|----------------|------------|
| Fatal | 3 | 3 | 2 | 1 | 2 | 11 | 1.8% |
| No Injury | 50 | 62 | 76 | 106 | 114 | 408 | 66.3% |
| Possible Injury | 15 | 17 | 12 | 18 | 15 | 77 | 12.5% |
| Suspected Minor Injury | 14 | 18 | 22 | 20 | 22 | 96 | 15.6% |
| Suspected Serious Injury | 5 | 5 | 2 | 5 | 6 | 23 | 3.7% |
| Total | 87 | 105 | 114 | 150 | 159 | 615 | 100.0% |

| Collision Manner | 2013 | 2014 | 2015 | 2016 | 2017 | Grand Total | Percentage |
|--|------|------|------|------|------|----------------|------------|
| Angle (Front to side) (Other than left turn) | 1 | - | - | 1 | - | 2 | 0.3% |
| Head On | 1 | 1 | - | - | 2 | 4 | 0.7% |
| Other | - | - | - | 1 | - | 1 | 0.16% |
| Rear End | 15 | 21 | 27 | 37 | 56 | 156 | 25.4% |
| Rear to Rear | - | - | - | - | 2 | 2 | 0.3% |
| Sideswipe (Opposite Direction) | 1 | - | - | - | - | 1 | 0.2% |
| Sideswipe (Same Direction) | 9 | 13 | 10 | 16 | 4 | 52 | 8.5% |
| Single Vehicle | 55 | 64 | 69 | 87 | 90 | 365 | 59.3% |
| Total | 87 | 105 | 114 | 150 | 159 | 615 | 100.0% |

Table 54 – Southbound MP 229 to MP 253, Crashes by Collision Manner

Crash rates for the entire project corridor were calculated using the following equations:

Total Crash Rate = 1,000,000 * # of crashes AADT * 365 * # of years * length of segment

100,000,000 * # of crashes involving one or more fatalities Fatal Crash Rate = AADT * 365 * # of years * length of segment

In the northbound direction, the total corridor crash rate is calculated to be 0.86 crashes per one million vehicle miles traveled and the fatal corridor crash rate is calculated to be 1.05 crashes per 100 million vehicle miles traveled. In the southbound direction, the total corridor crash rate is calculated to be 0.91 crashes per one million vehicle miles traveled (MVMT) and the fatal corridor crash rate is calculated to be 1.63 crashes per 100 million vehicle miles traveled.

The 2017 Arizona Motor Vehicle Crash Facts Report and the 2016 National Highway Traffic Safety Administration Traffic Safety Facts Report documented the following crash rates:

| Table 55 – | Arizona and | d US | Crash | Rates |
|------------|-------------|------|-------|-------|
|------------|-------------|------|-------|-------|

| | | | Urban | | Rural | |
|----------|--------------------------|------------------------------|--------------------------|---------------------------------|--------------------------|------------------------------|
| | Total Crash Rate/MVMT | Fatal Crash Rate/100 MVMT | Total Crash Rate/MVMT | Fatal Crash Rate/100 MVMT | Total Crash Rate/MVMT | Fatal Crash Rate/100 MVMT |
| Arizona | 1.95 | 1.41 | 2.14 | 1.03 | 1.39 | 2.59 |
| National | 2.29 | 1.18 | * | 0.75 | * | 1.76 |

* There was not enough information provided within the 2016 National Highway Traffic Safety Administration Traffic Safety Facts Report to calculate total crash rates for urban and rural areas.

After analyzing the observed crash data on a project wide scale, I-17 was divided into analysis segments to determine areas along I-17 that required further analysis. The freeway was segmented based on roadway geometry related to the interchanges along I-17 as well as the areas within defined design exception limits in order to identify higher risk areas along the study corridor. The crossroads at the interchanges were considered segment boundaries in order to consider the areas where interchange ramps merge with or diverge from the freeway separately. Total and Fatal Crash rates were then calculated for each of these study segments. The study segments were analyzed on a macro scale by comparing them to both Arizona and National crash rates. The segments were also analyzed on a micro scale by comparing them to the project corridor crash rates.

Although there are areas that exceed the Arizona or National Fatal Crash Rates, these areas only experienced one fatal crash; however, the segment limits are small enough that the rate is calculated to be higher than average. None of the areas exceed the Arizona or National Total Crash Rates; therefore, it was determined that the study areas should be compared to the project corridor rates in order to determine higher risk areas that warrant the assessment of countermeasures.

Of the segments exhibiting higher observed crash rates than the project corridor, nine segments between MP 229 and MP 245 and eight segments between MP 245 and 253 were identified for modeling in the IHSDM. Two main improvement types were considered for the segments modeled in the IHSDM. For segments identified within traffic interchange ramp areas, IHSDM was utilized to predict the reduction in crashes that could be expected by transitioning the existing taper-type ramps to parallel-type ramps. For segments identified within horizontal or vertical design exception areas, the IHSDM, in addition to published crash modification factors, was utilized to predict the reduction in crashes that could be expected by correcting the variation between the existing and recommended superelevation or the difference between the existing and recommended vertical grade. These segments are listed below.

- Interchange Ramp-Related Improvements
 - Anthem Way (NB On Ramp)
 - New River TI (SB Ramps)
 - Table Mesa TI (SB Off Ramp)
 - Table Mesa TI (NB On Ramp)
 - Rock Springs TI (NB Ramps)
 - Black Canyon City TI (All Ramps)
- Horizontal and Vertical Design Exception Improvements
 - NB, MP 239.75 to 240.49 (Superelevation DE)
 - MP 242.14 to 242.45 (Superelevation DE)
 - NB, MP 244.34 to 244.68 (Superelevation DE)
 - NB, MP 244.81 to 245.00 (Superelevation DE)
 - SB, MP 236.70 to 237.03 (Superelevation DE)
 - SB, MP 237.85 to 238.42 (Superelevation DE)
 - SB, MP 239.57 to 240.06 (Superelevation DE)
 - SB, MP 244.33 to 244.69 (Superelevation DE)

- SB, MP 244.83 to 245.04 (Superelevation DE)
- SB, MP 246.04 to 246.32 (Max Grade and Superelevation DE)
- SB, MP 246.32 to 246.65 (Max Grade and Superelevation DE)
- SB, MP 249.15 to 249.47 (Superelevation DE)
- SB, MP 249.63 to 249.82 (Max Grade and Superelevation DE)
- SB, MP 249.82 to 250.01 (Max Grade and Superelevation DE)
- SB, MP 250.01 to 250.29 (Max Grade and Superelevation DE)
- SB, MP 250.29 to 250.64 (Max Grade and Superelevation DE)
- SB, MP 251.05 to 251.41 (Superelevation DE)

In addition to considering areas that exhibit higher than average crash rates, the impacts of different travel lane and shoulder widths along the proposed flex lane alignment were considered. For the purposes of the safety study, the "shoulder" was defined as the west-side shoulder of the flex lane alignment and the "emergency shoulder" was defined as the east-side shoulder of the flex lanes. The following comparisons were made using the modeling capabilities within the IHSDM.

- Flex Lane Cross Sections
 - o 10' to 11' Lane Width
 - o 11' to 12' Lane Width
 - o 6' to 8' Emergency Shoulder Width
 - o 8' to 10' Emergency Shoulder Width
 - o 4' to 2' Shoulder Width
 - o 6' to 4' Shoulder Width

Upon determining estimated reductions in predicted crashes, a cost-benefit analysis was conducted to determine the fiscal value to implementing the assessed countermeasures. The cost-benefit analysis was completed by first calculating an estimated annual cost savings based on the yearly reduction of crashes and the comprehensive costs associated with these crashes. Comprehensive crash costs are established to estimate the overall total cost of a crash based on severity. These costs include both monetary costs related to property damage, congestion and incurred delay, emergency services, legal costs, and medical care related to the crash as well as a cost associated with intangible impacts such as loss in quality of life. Table 56 provides the comprehensive crash costs associated with each crash type that were utilized for the cost-benefit analyses. The FHWA comprehensive crash costs were utilized as opposed to those published by Arizona because Arizona only reports crash costs for fatal and serious injury crashes.

Table 56 – Monetary Costs Based on Crash Severity

| Injury Severity | Comprehensive Crash Cost |
|--------------------|--------------------------|
| Fatal | \$11,295,400 |
| Incapacitating | \$655,000 |
| Non-Incapacitating | \$198,500 |
| Possible Injury | \$125,600 |
| No Injury | \$11,900 |

The cost savings were then compared to one-time construction costs estimated for the assumed improvement. A "years to return" value was calculated based on the amount of time it would take for the annual cost savings to equal the one-time construction cost. This value captured the amount of time required for the improvement to offset the cost based on estimated crashes. The-cost benefit analysis results are summarized in Tables 57 through 59.

Table 57 – Interchange Ramp Improvements Cost/Benefit Summary

| Location | Cost | Annual Benefit | Years to Return |
|----------------------------------|--------|----------------|-----------------|
| Anthem TI (NB On Ramp) | \$0.6M | \$12k | 50.0 |
| New River TI (SB Ramps) | \$1.2M | -\$45k | No Return |
| Table Mesa TI (SB Off Ramp) | \$3M | -\$1k | No Return |
| Table Mesa TI (NB On Ramp) | \$0.6M | \$89k | 6.7 |
| Rock Springs TI (NB Ramps) | \$1.2M | \$47k | 25.5 |
| Black Canyon City TI (All Ramps) | \$2.4M | \$187k | 12.8 |

Table 58 – Superelevation Improvements Cost/Benefit Summary

| Location | Cost | Annual Benefit | Years to Return |
|---|--------|----------------|-----------------|
| NB, MP 239.75 to 240.49 (Super) | \$4.4M | \$130k | 33.8 |
| NB, MP 242.14 to 242.45 (Super) | \$2.9M | \$64k | 45.3 |
| NB, MP 244.34 to 244.68 (Super) | \$3.0M | \$122k | 24.6 |
| NB, MP 244.81 to 245.00 (Super) | \$1.1M | \$42k | 26.2 |
| SB, MP 236.70 to 237.03 (Super) | \$2.0M | \$27k | 74.1 |
| SB, MP 237.85 to 238.42 (Super) | \$3.4M | \$121k | 28.1 |
| SB, MP 239.57 to 240.06 (Super) | \$2.9M | \$99k | 29.3 |
| SB, MP 244.33 to 244.69 (Super) | \$3.2M | \$118k | 27.1 |
| SB, MP 244.83 to 245.04 (Super) | \$1.3M | \$48k | 27.1 |
| SB, MP 246.04 to 246.32 (Super & Grade) | \$4.2M | \$106k | 39.6 |

| Location | Cost | Annual Benefit | Years to Return |
|---|--------|----------------|-----------------|
| NB, MP 239.75 to 240.49 (Super) | \$4.4M | \$130k | 33.8 |
| NB, MP 242.14 to 242.45 (Super) | \$2.9M | \$64k | 45.3 |
| SB, MP 246.32 to 246.65 (Super & Grade) | \$5.0M | \$84k | 59.5 |
| SB, MP 249.15 to 249.47 (Super) | \$4.8M | \$79k | 60.8 |
| SB, MP 249.63 to 249.82 (Super & Grade) | \$2.8M | \$59k | 47.5 |
| SB, MP 249.82 to 250.01 (Super & Grade) | \$2.8M | \$40k | 70.0 |
| SB, MP 250.01 to 250.29 (Super & Grade) | \$4.2M | \$80k | 52.5 |
| SB, MP 250.29 to 250.64 (Super & Grade) | \$5.2M | \$39k | 133.3 |
| SB, MP 251.05 to 251.41 (Super) | \$5.4M | \$150k | 36.0 |

Table 59 – Flex Lane Cross Section Cost/Benefit Summary

| Location | Cost | Annual Benefit | Years to Return |
|------------------------------------|---------|----------------|-----------------|
| 10' to 11' Lane Width | \$4.5M | \$1.2M | 3.8 |
| 11' to 12' Lane Width | \$4.5M | \$1.0M | 4.5 |
| 6' to 8' Emergency Shoulder Width | \$4.5M | \$487k | 9.2 |
| 8' to 10' Emergency Shoulder Width | \$4.5M | \$446k | 10.1 |
| 4' to 2' Shoulder Width | -\$4.5M | \$147k | Immediate |
| 6' to 4' Shoulder Width | -\$4.5M | \$45k | Immediate |

The Arizona Highway Safety Improvement Program (HSIP) Manual (Appendix C), updated in March 2015, includes service life (in years) for specific types of roadway improvements. Based on the HSIP Manual, the expected service life for each improvement is as follows:

- Modifying Interchange Ramps from Taper-Type to Parallel-Type 20 years
- Correcting Superelevation Variations 20 years
- Correcting Vertical Grade 20 years

The expected years to return for the following segments is less than the service life; therefore, it is recommended that these improvements be implemented:

- Modifying the northbound on ramp at the Table Mesa TI from the existing taper-type configuration to a parallel-type configuration
- Modifying all of the interchange ramps at the Black Canyon City TI from the existing taper-type configuration to a parallel-type configuration

For the remaining interchange ramp or design exception related segments modeled using the IHSDM, the expected years to return exceeds the service life of the modeled roadway improvement; therefore, implementation of the improvements for these segments is not recommended.

Based on the analysis results, assumptions, and modeling limitations, it is recommended that the flex lanes provide a cross-section of a 4-foot shoulder, two 12-foot travel lanes, and a 10-foot emergency shoulder. The 12-foot travel lane width and 10-foot emergency shoulder width result in the lowest predicted total number of crashes. The 2-foot shoulder width results in a slightly lower predicted total number of crashes when compared to the 4-foot shoulder. However, reducing the shoulder width to 2' would negatively affect sight distance (based on engineering judgement; stopping sight distance is not considered by the model).

The segment in the northbound direction on I-17 between MP 237.58 and MP 238.52, locally referred to as U-Haul Hill, was identified as a higher risk location based on the existing crash trends. There are a notable number of overturn crashes in this area. Based on the reviewed crash reports, it appears that these crashes are related to high operating speeds and blowing winds. It was determined that the IHSDM software would not provide a beneficial analysis of these areas as the crash prediction module does not take into account posted speed limit or presence of warning signing. Warning signs currently exist to warn drivers of strong wind areas and the importance of maintaining lower operating speeds. It is recommended that the crashes be monitored in this area to determine the effectiveness of the existing signing and determine if additional signage is warranted.

4.23 Social, Economic, and Environmental Considerations

The environmental study begins at the Anthem Way TI at MP 228.5 on I-17 in Maricopa County and extends north to the Sunset Point TI at MP 252.0 in Yavapai County.

Work began on an Environmental Assessment in 2006 (MP 232 to MP 262); however, the scope of the environmental studies was reduced when FHWA/ADOT policies changed regarding the approval of environmental documents for projects that are not included in an approved transportation improvement program. A Planning and Environmental Linkages Checklist was prepared in 2015 to document the efforts completed to date (e.g., biological resources, cultural resources), document important issues identified during the study process, and provide a basis for identifying smaller projects which may accomplish improvements at a lower cost. Environmental technical studies and an environmental document for the near-term improvements will be complete in Spring 2019.

Specific mitigation measures will be included in the environmental document.

The Final Noise Analysis Technical Report, May 2018, recommended noise barriers in three locations:

TABLE 60 – RECOMMENDED NOISE BARRIERS

| Noise Barrier Description | Barrier Height Range, ft. | Length, ft. |
|---|---------------------------|-------------|
| Barrier S2 (Sta 1542+00 to Sta 1577+96) | 14-16 | 3,600 |
| Barrier N3 (Sta 1698+00 to Sta 1709+99) | 14 | 1,200 |
| Barrier S6 (Sta 2215+00 to Sta 2233+00) | 16-18 | 1,800 |

The possible incorporation of fire breaks and other fire prevention measures should be evaluated and coordinated with the Bureau of Land Management during final design.

5.0 AASHTO Controlling Design Criteria

Introduction 5.1

The existing features of I-17 between Anthem Way TI and Sunset Point TI (MP 229.1 to MP 252.5) were analyzed using the AASHTO Controlling Design Criteria outlined in A Policy on Geometric Design of Highways and Streets (2011 edition), also known as the AASHTO Green Book. A Policy on Design Standards - Interstate System (2016 edition) was also used.

This section describes the non-conforming AASHTO design elements of the existing highway which will not be upgraded as part of the project and for which design exceptions will be requested. The AASHTO analysis and list of proposed design exceptions will need to be updated during final design; the recommended alternative will be used to make this determination. A complete current analysis is available in the Initial AASHTO Controlling Design Criteria Report, I-17: SR 101L TI to Black Canyon City TI, TRACS No. 17 MA 215 H5162 01L, October 2000, and the I-17: Black Canyon City TI to Sunset Point TI, TRACS No. 17 MA 229 H6800 01L, August 2018. Horizontal and vertical data summaries for mainline I-17 are provided in Appendix A.

Lane and Shoulder Widths

The existing lane and shoulder widths along the mainline of the northbound and southbound I-17 in the study area meet AASHTO recommendations. However, two locations will not meet minimum inside shoulder width requirements when I-17 is widened.

The following locations where the inside shoulder width will be less than the recommended 10' are as follows:

- Southbound I-17 at Table Mesa TI UP (MP 235.9) 5.5' less than recommended.
- Northbound I-17 at Table Mesa TI UP (MP 235.9) 5.5' less than recommended.

Vertical Alignment and Stopping Sight Distance

The existing vertical stopping sight distance is less than the AASHTO recommendations at the following locations. Because the added lanes will match the existing profile grade, these crest vertical curve locations, which have been grade-adjusted, will require design exceptions:

- Northbound MP 232.0 to 232.2 -- 24' less than the required 832'
- Northbound MP 232.8 to 233.0 -- 42' less than the required 837' •
- Northbound MP 237.2 to 237.5 -- 149' less than the required 905' •
- Northbound MP 240.0 to 240.4 -- 82' less than the required 869' •
- Northbound MP 242.2 to 242.3 -- 38' less than the required 842' •
- Southbound MP 232.0 to 232.2 -- 57' less than the required 866'

- Southbound MP 233.5 to 233.7 -- 25' less than the required 835'
- Southbound MP 234.9 to 235.1 -- 11' less than the required 860'
- Southbound MP 235.7 to 236.0 -- 81' less than the required 866'

Horizontal Alignment and Stopping Sight Distance 5.4

A listing of the horizontal curve analysis is included in Appendix A. The existing horizontal curve superelevation is less than the AASHTO recommended minimum at the following locations:

- Northbound I-17 (MP 233.30 to MP 233.40) -- 0.038 '/ft less than the recommended 0.061 '/ft
- Northbound I-17 (MP 233.80 to MP 234.00) -- 0.025 '/ft less than the recommended 0.079 '/ft
- Northbound I-17 (MP 234.20 to MP 234.40) -- 0.038 '/ft less than the recommended 0.061 '/ft
- Northbound I-17 (MP 234.70 to MP 234.90) -- 0.016 '/ft less than the recommended 0.031 '/ft
- Northbound I-17 (MP 235.20 to MP 235.30) -- 0.038 '/ft less than the recommended 0.061 '/ft
- Northbound I-17 (MP 235.80 to MP 236.40) -- 0.032 '/ft less than the recommended 0.061 '/ft
- Northbound I-17 (MP 237.20 to MP 237.60) -- 0.026 '/ft less than the recommended 0.041 '/ft
- Northbound I-17 (MP 238.50 to MP 239.50) -- 0.016 '/ft less than the recommended 0.031 '/ft •
- Northbound I-17 (MP 239.60 to MP 240.40) -- 0.026 '/ft less than the recommended 0.041 '/ft
- Northbound I-17 (MP 242.10 to MP 242.50) -- 0.026 '/ft less than the recommended 0.041 '/ft •
- Northbound I-17 (MP 244.30 to MP 244.70) -- 0.048 '/ft less than the recommended 0.063 '/ft
- Southbound I-17 (MP 235.80 to MP 236.40) -- 0.060 '/ft less than the recommended 0.079 '/ft
- Southbound I-17 (MP 236.70 to MP 236.80) -- 0.026 '/ft less than the recommended 0.041 '/ft
- Southbound I-17 (MP 236.90 to MP 237.00) -- 0.026 '/ft less than the recommended 0.041 '/ft
- Southbound I-17 (MP 237.10 to MP 237.40) -- 0.038 '/ft less than the recommended 0.061 '/ft
- Southbound I-17 (MP 237.70 to MP 237.80) -- 0.026 '/ft less than the recommended 0.041 '/ft
- Southbound I-17 (MP 237.90 to MP 238.40) -- 0.036 '/ft less than the recommended 0.051 '/ft
- Southbound I-17 (MP 239.70 to MP 240.00) -- 0.038 '/ft less than the recommended 0.061 '/ft
- Southbound I-17 (MP 240.60 to MP 240.80) -- 0.025 '/ft less than the recommended 0.079 '/ft •
- Southbound I-17 (MP 240.90 to MP 241.80) -- 0.006 '/ft less than the recommended 0.021 '/ft
- Southbound I-17 (MP 243.50 to MP 244.00) -- 0.011 '/ft less than the recommended 0.061 '/ft
- Southbound I-17 (MP 244.30 to MP 244.70) -- 0.046 '/ft less than the recommended 0.061 '/ft
- Southbound I-17 (MP 244.81 to MP 245.13) -- 0.019 '/ft less than the recommended 0.034 '/ft •
- SB I-17 and flex lanes (MP 245.78 to MP 245.93) -- 0.047 '/ft less than the recommended 0.062 '/ft
- SB I-17 and flex lanes (MP 246.13 to MP 246.26) -- 0.057 '/ft less than the recommended 0.087 '/ft

- SB I-17 and flex lanes (MP 246.40 to MP 246.56) -- 0.028 '/ft less than the recommended 0.099 '/ft
- SB I-17 and flex lanes (MP 246.72 to MP 246.81) -- 0.028 '/ft less than the recommended 0.099 '/ft
- SB I-17 and flex lanes (MP 247.08 to MP 247.10) -- 0.016 '/ft less than the recommended 0.087 '/ft
- SB I-17 and flex lanes (MP 247.24 to MP 247.45) -- 0.028 '/ft less than the recommended 0.099 '/ft •
- SB I-17 and flex lanes (MP 247.60 to MP 247.92) -- 0.028 '/ft less than the recommended 0.099 '/ft
- SB I-17 and flex lanes (MP 248.07 to MP 248.47) -- 0.040 '/ft less than the recommended 0.055 '/ft .
- SB I-17 and flex lanes (MP 248.75 to MP 248.94) -- 0.018 '/ft less than the recommended 0.033 '/ft ٠
- SB I-17 and flex lanes (MP 249.23 to MP 249.35) -- 0.057 '/ft less than the recommended 0.087 '/ft
- SB I-17 and flex lanes (MP 249.58 to MP 249.69) -- 0.028 '/ft less than the recommended 0.099 '/ft
- SB I-17 and flex lanes (MP 249.85 to MP 249.89) -- 0.028 '/ft less than the recommended 0.099 '/ft
- SB I-17 and flex lanes (MP 250.04 to MP 250.08) -- 0.028 '/ft less than the recommended 0.099 '/ft •
- SB I-17 and flex lanes (MP 250.23 to MP 250.36) -- 0.028 '/ft less than the recommended 0.099 '/ft
- SB I-17 and flex lanes (MP 250.50 to MP 250.57) -- 0.016 '/ft less than the recommended 0.087 '/ft .
- SB I-17 and flex lanes (MP 250.72 to MP 250.91) -- 0.057 '/ft less than the recommended 0.087 '/ft
- SB I-17 and flex lanes (MP 251.05 to MP 251.38) -- 0.064 '/ft less than the recommended 0.079 '/ft

With the addition of the median barrier for the flex lanes between existing southbound lanes and the flex lanes, the following horizontal curves do not provide AASHTO-recommended minimum horizontal sight distance:

- SB MP 245.75 to MP 245.90, barrier side flex lane -- 85' less than the required 612' •
- SB MP 246.29 to MP 246.56, barrier side flex lane -- 209' less than the required 584'
- SB MP 247.15 to MP 247.55, barrier side flex lane -- 209' less than the required 584' •
- SB MP 247.99 to MP 248.42, barrier side flex lane -- 119' less than the required 682'
- SB MP 249.54 to MP 249.57, barrier side flex lane -- 209' less than the required 584'
- SB MP 249.79 to MP 249.92, barrier side flex lane -- 189' less than the required 584'
- SB MP 250.27 to MP 250.39, barrier side flex lane-- 151' less than the required 584'
- SB MP 250.97 to MP 251.37, barrier side flex lane -- 85' less than the required 612'
- SB MP 246.22 to MP 246.37, existing inside lane -- 298' less than the required 728'
- SB MP 246.73 to MP 246.96, existing inside lane -- 377' less than the required 728'
- SB MP 247.10 to MP 247.22, existing inside lane -- 240' less than the required 728'
- SB MP 247.61 to MP 248.05, existing inside lane -- 346' less than the required 728' •
- SB MP 249.23 to MP 249.48, existing inside lane -- 261' less than the required 682'
- SB MP 249.71 to MP 249.93, existing inside lane -- 305' less than the required 728'
- SB MP 250.10 to MP 250.34, existing inside lane -- 337' less than the required 728'

SB MP 250.73 to MP 251.01, existing inside lane -- 281' less than the required 728'

5.5 Design Speed

The route's classification, use, and terrain determine the appropriate design speed to be used to evaluate the existing and proposed roadway. Because the existing facility traverses rural surroundings on rolling and mountainous terrain, the AASHTO Green Book and ADOT RDG recommend design speeds of 65 and 75 mph as detailed below:

From MP 229.0 to MP 244.5, the AASHTO-recommended minimum design speed of the highway is 70 mph (rolling terrain, rural). Posted speeds in this section are 75 mph from MP 229.0 to MP 244.5.

From MP 244.5 to MP 250.5, the AASHTO-recommended minimum design speed for evaluation of the existing highway is 50-60 mph (mountainous terrain, rural). The posted speed in this section is 65 mph.

Design speeds of 65 mph in mountainous terrain and 75 mph in rolling terrain were used for developing the preferred alternatives and are recommended for final design.

5.6 Cross Slopes

Existing cross slopes of 1.5% to 2.0% conform to current design recommendations.

Grades 5.7

Because the recommended improvements match the existing profiles, design exceptions will be required for those existing grades in excess of AASHTO guideline recommendations.

The existing gradient is greater than the AASHTO recommended 4% maximum at the following locations:

Northbound I-17 (MP 237.49 to MP 238.19) – 1.0526% steeper than the maximum

The existing gradient is greater than the AASHTO recommended 5% maximum at the following locations:

- Southbound I-17 (MP 245.95 to MP 247.62) 0.7368% greater than the maximum
- Southbound I-17 (MP 248.78 to MP 249.18) 0.7143% greater than the maximum
- Southbound I-17 (MP 249.53 to MP 250.81) 1.1739% greater than the maximum

Vertical Clearance

With implementation of the project improvements, vertical clearances will conform to current design standards except at the following locations:

Northbound I-17, MP 242.1, Rock Springs TI UP (Str # 00969) -- 0'-1" less than the minimum 16'0"

5.9 Bridge Structures

The existing bridge structural capacity does not meet recommended AASHTO recommendations at the following location:

MP 248.40 Bumble Bee TI OP NB (#01171) – 1.7 less than the minimum HS 20.

5.10 Design Variances

Design variances were identified when reviewing proposed design elements compared to ADOT's Roadway Design Guidelines. Design variances have been requested in the following locations:

| Design Feature | Туре | Location | Discrepancy from Required Design Value |
|--|---------------|---|--|
| 1) Superelevation Transition Length, | ADOT Variance | MD 222 80 to MD 224 00 600' onized langth | 124' langer than the maximum La-476 |
| Northbound I-17 | ADO1 variance | MP 233.80 to MP 234.00, 600 spiral length | 124 longer than the maximum Ls=476 |
| | | MP 246.40 to MP 246.56, 400' spiral length | 63' longer than the maximum Ls=337' |
| | | MP 246.72 to MP 246.81, 400' spiral length | 63' longer than the maximum Ls=337' |
| | | MP 247.24 to MP 247.45, 400' spiral length | 63' longer than the maximum Ls=337' |
| Superalayation Transition Longth | | MP 247.60 to MP 247.92, 400' spiral length | 63' longer than the maximum Ls=337' |
| Supererevation Transition Length, | ADOT Variance | MP 249.23 to MP 249.35, 450' spiral length | 61' longer than the maximum Ls=389' |
| Soundound I-17 | | MP 249.58 to MP 249.69, 400' spiral length | 63' longer than the maximum Ls=337' |
| | | MP 249.85 to MP 249.89, 400' spiral length | 63' longer than the maximum Ls=337' |
| | | MP 250.04 to MP 250.08, 400' spiral length | 63' longer than the maximum Ls=337' |
| | | MP 250.23 to MP 250.36, 400' spiral length | 63' longer than the maximum Ls=337' |
| 2) Horizontal Align Coincident with Axis of Rotation, | ADOTTAL S | MP 237.0 to MP 240.8, Widened Pavement with new horizontal alignment uses | |
| Southbound I-17 | ADOT Variance | existing axis of rotation between two existing lanes (exst HCL). | 15' from existing HCL and PGL. |
| | | MP 233.30 to MP 233.40, Widened Pavement matches existing Ls=450.24', | 2°15' minimum DOC for spiral curves at 75mph |
| | | DOC= 1°30'03", DS=75mph | design speed |
| | | MP 233.80 to MP 234.00, Widened Pavement matches existing Ls=600', | 2°15' minimum DOC for spiral curves at 75mph |
| | | DOC= 2°00'00", DS=75mph | design speed |
| | | MP 234.20 to MP 234.40, Widened Pavement matches existing Ls=450', | 2°15' minimum DOC for spiral curves at 75mph |
| | | DOC= 1°30'00", DS=75mph | design speed |
| Use of Spiral Curves (emax=10%), | ADOT Variance | MP 234.69 to MP 234.88, Widened Pavement matches existing Ls=225', | 2°15' minimum DOC for spiral curves at 75mph |
| Northbound I-17 | ABOT Vallance | DOC= 0°45'00", DS=75mph | design speed |
| | | MP 235.80 to MP 236.40, Widened Pavement matches existing Ls=300', | 2°15' minimum DOC for spiral curves at 75mph |
| | | DOC= 1°30'00", DS=75mph | design speed |
| | | MP 243.51 to MP 244.02, Widened Pavement matches existing Ls=300', | 2°45' minimum DOC for spiral curves at 65mph |
| | | DOC= 1°28'45", DS=65mph | design speed |
| | | MP 244.30 to MP 244.70, Widened Pavement matches existing Ls=300', | 2°45' minimum DOC for spiral curves at 65mph |
| | | DOC= 2°02'18", DS=65mph | design speed |
| | | MP 235.80 to MP 236.40, Widened Pavement matches existing Ls=300', | 2°15' minimum DOC for spiral curves at 75mph |
| | | DOC= 2°00'00", DS=75mph | design speed |
| | | MP 236.70 to MP 236.80, Widened Pavement matches existing Ls=200 ⁷ , | 2°15' minimum DOC for spiral curves at 75mph |
| | | DOC= 1°00'00", DS=/5mph | design speed |
| | | MP 250.90 to MP 257.00, widened Pavement matches existing Ls=200, | 2°15 minimum DOC for spiral curves at 75mpn |
| Use of Spiral Curves (amov=10%) | | MD 227 70 to MD 227 80 Wildowed Deventent metakes existing Le-200? | design speed |
| Southbound L17 | ADOT Variance | $DOC = 1^{\circ}00^{\circ}00^{\circ}$ DS=75mpb | design speed |
| | | MP 237.00 to MP 238.40. Widened Payement matches existing L s=375' | 2°15' minimum DOC for spiral curves at 75mph |
| | | $DOC = 1^{\circ}15'00"$ DS=75mph | design speed |
| | | MP 243 50 to MP 244 00 Widened Pavement matches existing I s=300' | 2°15' minimum DOC for spiral curves at 75mph |
| | | $DOC = 1^{\circ}31'17"$, DS=75mph | design speed |
| | | MP 244.30 to MP 244.70. Widened Pavement matches existing Ls=300'. | 2°15' minimum DOC for spiral curves at 75mph |
| | | DOC= 1°57'47", DS=75mph | design speed |
| Use of Spiral Curves (emax=10%), Southbound I-17 Flex Lanes | ADOT Variance | MP 244.81 to MP 245.13. Widened Pavement matches existing Ls=300'. | 2°45' minimum DOC for spiral curves at 65mph |
| | | DOC= 1°12'00". DS=65mph | design speed |
| | | MP 248.07 to MP 248.47. Widened Pavement matches existing Ls=350'. | 2°45' minimum DOC for spiral curves at 65mph |
| | | DOC=1°45'00". DS=65mph | design speed |
| | | MP 251.05 to MP 251.38, Widened Pavement matches existing Ls=400'. | 2°45' minimum DOC for spiral curves at 65mph |
| | | DOC= 2°00'00", DS=65mph | design speed |
| 4) Maximum Grade Break Without a Vertical Curve. | ADOT Variance | MP 229.84, 1532+00.00, Grade Break of 0.2399% | 0.0399% more than 0.2000% maximum. |
| Northbound I-17 | | MP 234.65, 1788+00.00, Grade Break of 0.3239% | 0.1239% more than 0.2000% maximum. |
| | | MP 248.95, 2516+00.00, Grade Break of 0.5967% | 0.3967% more than 0.2000% maximum |
| Maximum Grade Break Without a Vertical Curve, | ADOT Variance | MP 249.76, 2567+00.00, Grade Break of 0.6739% | 0.4739% more than 0.2000% maximum |
| Southbound I-17 Flex Lanes | | MP 250.30, 2595+00.00, Grade Break of 0.4583% | 0.2583% more than 0.2000% maximum |
6.0 Itemized Estimate of Probable Costs

Recommended Alternatives

The estimates of probable construction cost for the near-term, recommended mainline alternatives are as follows:

| SEGMENT | ESTIMATED CONSTRUCTION COST |
|---|-----------------------------|
| Anthem Way to Black Canyon City Widening | \$202,900,000 |
| Black Canyon City to Sunset Point (Flex Lanes) | \$128,500,000 |

TABLE 61 – TOTAL ESTIMATED CONSTRUCTION COSTS

The detailed estimates of probable cost are shown on the following pages. The estimated costs are based upon unit prices from ADOT's Construction Cost Data Base. The pavement structural section used for the cost estimate was a flexible pavement throughout the project limits. The recommended pavement section for the study area is estimated at 22.5 inches (11 inches of asphaltic concrete over 11 inches of aggregate base plus 0.5 inch AR-ACFC) between the Anthem and New River TIs and 25.5 inches from the New River TI to the Black Canyon City TI (11 inches of asphaltic concrete over 14 inches of aggregate base plus 0.5 inch AR-ACFC). The existing travel lanes and remaining shoulders will be milled 0.5 inch and replaced with 0.5 inch AR-ACFC.

A project of this length is an excellent candidate for full depth pavement reconstruction through recycling the existing pavement components. There are various pavement recycling schemes that can be used to accomplish this and would use the existing aggregate base and asphaltic concrete materials as the new base and a portion of the new AC resurfacing. Pavement pulverization, foamed asphalt base, and recycled asphaltic pavement are possible approaches that should be evaluated during the final design phase as part of cost savings and reduction of waste materials. For estimating purposes at this conceptual design phase, all new materials were assumed.

Where inside widening is proposed, the existing 4-foot shoulder will be removed and replaced with the new pavement section. Where widening to the outside is proposed, the existing 10-foot shoulder will be removed and replaced with the new pavement section.

The following assumptions were also used for the cost estimate:

- Estimates include ICAP percentage 10.02% (FY 2019 rate).
- Estimates include design costs at 10%. •
- No costs were assigned for new right-of-way. Since the required right-of-way is owned by the • federal government, there would be no cost to ADOT for the land.
- The existing ramps and crossroads are to remain in place if determined to be in satisfactory condition at the time of final design.

- assumed for utility relocations.
- information is available.
- whichever distance is greater.
- Reinforced box culvert quantities are based on Table I fill height conditions with 4:1 side slopes.
- Outlet aprons are required at all box culverts that require extension downstream.
- Existing end sections for pipe culverts are unsalvageable.
- replacement.
- bank protection, are required.

ITS

The roadway widening from Anthem Way to Black Canyon City was assumed to deploy FMS conduit and pull box infrastructure and fiber communications along both sides of the freeway within this section. CCTV cameras were assumed at one-mile spacing, two new DMS in the southbound direction, and one new node building within this project limits near New River (MP 232), where there is a power source available, and which is about 18 miles from Node 15 at I-17/SR 101L.

The flex lanes include ITS within the segment between MP 245 and 252 and includes conduit and pull box infrastructure and fiber communications on one side of the freeway along the flex lane alignment, CCTV at onehalf mile or less spacing for continuous coverage, detection at the flex lane transition areas, two new DMS, lane control signals and traffic gates, and power distribution with limited available power sources. A new node building will also be required at the Sunset Point TI (MP 252) or the Sunset Point rest area, where there are available power sources.

Northbound I-17 will include CCTV at approximate one-mile spacing. These devices will be powered by solar panels and communicate back to field devices along the flex lanes as discussed in this document.

Options for controlling entry into the flex lanes should be investigated at the time of design. State of the art technology for items such as advising motorists of roadway conditions, the availability of alternate routes, and measures for notifying officials of incidents should be researched and implemented at the time of design.

Signing and Pavement Marking

The roadway widening from Anthem Way to Black Canyon City was assumed to require the relocation of existing regulatory and warning signs impacted by the widening. The estimate includes the relocations of these signs as well as the new post supports, foundations, and slip bases necessary.

New signing is included only for the flex lanes and crossovers. No upgrades to existing northbound or southbound signs are included in the estimate. The estimate also includes guide signs shown in the signing concept as well as new signing that will need to be replicated for the southbound direction now that the roadway is separated by barrier or included for the northbound travel direction.

• Potential utility conflicts have been identified as outlined in Section 4.15. A percentage was

 Cost items associated with earthwork, such as roadway excavation, borrow, and rock excavation may vary from those calculated in final design, when more detailed survey and geotechnical

All culverts are extended to the appropriate clear zone requirements or toe of the roadway fill slope.

• Existing reinforced box culverts and pipe culverts are in good condition and do not require

• No improvement to washes upstream and downstream of culverts, such as energy dissipators or

Lighting

The roadway widening from Anthem Way to Black Canyon City is not expected to require upgrades to existing lighting and therefore not included in the roadway widening estimate.

New lighting will be installed at the crossovers for the two-lane flex roadway facility. The estimate includes the installation of light poles, foundations, and fixtures as well as the required conduit and conductors. The required establishment of electrical service at both crossovers is also included.

Bridges

Assumptions for replacement bridges:

No costs are included for replacement or rehabilitation of the Moores Gulch SB or Bumble Bee Road NB bridge; these structure replacements are programmed under different projects.

Replacement bridge unit costs will be greater than the unit costs of a new bridge on a new alignment. Cost factors include:

- Demolition of the existing bridge: Demolition requires traffic control and protection for maintained lanes under the existing bridge. Demolition also requires evaluation of the existing structure for the presence of asbestos and lead-based paint.
- Staged construction and traffic control: The replacement structure will likely need to be constructed adjacent to and/or around existing traffic. Staged construction may be required to maintain traffic movements. Accelerated bridge construction techniques may also be required to reduce the duration of bridge construction and reduce traffic impacts.
- Bridge areas noted account for additional bridge deck, or overbuild width, required to provide adequate bridge width to maintain the required number of traffic lanes during each stage of construction.
- The proposed new bridge at Bumble Bee TI SB is estimated to have a higher unit bridge cost than most typical Arizona bridges due to the long-skewed span of the crossing over I-17 and the likely use of steel girders to facilitate this long span. Other possible options such as the use of a straddle bent or posttensioned spliced girders are considered comparable in cost at this stage of analysis.
- ADOT RDS has requested that all new, widened, and rehabilitated bridges be painted.

Assumptions for widened bridges:

Widening unit bridge costs (cost per square foot) will be greater than the unit cost of a new structure. Cost factors include:

- Partial demolition of the existing bridge at tie-in points: Partial removal of the existing is required to remove the existing barrier and create an appropriate tie-in point for the widened structure. Any demolition also requires evaluation of the existing structure for the presence of asbestos and leadbased paint.
- Existing bridge tie-ins: The widened structure will need to be compatible with and tied to the existing structure.

- control requirements.
- that barrier is also included in the bridge costs.
- have a lower average cost for widening.
- bridge.

Retaining Walls

Retaining wall costs are generally expressed as a cost per square foot of wall. This cost can vary considerably depending on the height and type of wall and the topography. Cast in place concrete walls are generally more cost effective for the shorter walls, while MSE walls are typically more cost effective for taller walls.

Factors such as construction in a cut section or a fill section also impact costs. Cut sections are costlier to construct, particularly if MSE walls are specified due to the large area required behind the walls for straps. MSE walls may not be feasible where walls are required below an existing roadway.

Average wall costs used for this study include the costs of a concrete barrier with a moment slab foundation on top of the wall backfill.

Landscaping

Landscaping costs at \$390,000 per mile are based on the following assumptions:

- 50' average disturbance both sides of I-17
- Permanent irrigation may be used in urbanized areas with available water. Temporary irrigation used for revegetation areas.
- Total disturbance of 315 acres.
- \$200,000 per mile for native plant salvage, nursery storage, and replanting •
- One to 1.5 percent of structures costs assumed for aesthetics and rustication. •
- Salvage, store, and replace top 4-6" surface soil.
- 10% of rock cuts could be stained.
- areas.

Traffic control: Bridge widening will need to be constructed adjacent to traffic, increasing traffic

Where the existing bridge has non-conforming barrier on the non-widened side the cost of replacing

Cast-in-place slab bridges are typically more economical than girder bridges and are anticipated to

Bridge areas include the anticipated additional deck area due to the partial removal of the existing

 Includes herbicide and manual or mechanical weed removal of non-rock roadside areas. Herbicide has been applied to 55% of non-rock areas and manual or mechanical weed removal to 45% of non-rock

TABLE 62 - ESTIMATE OF PROBABLE CONSTRUCTION COST - ANTHEM WAY TI TO BLACKCANYON CITY TI WIDENING

| Item No. | Item Description | Unit Quantity | | | | Total Price | |
|----------|--|---------------|----------|---------|------------|-------------|------------|
| 2010011 | CLEARING AND GRUBBING | ACRE | 182 | \$ | 600.00 | \$ | 109,200 |
| 2020001 | REMOVAL OF STRUCTURES AND OBSTRUCTIONS | L.SUM | 1 | \$ | 90,000.00 | \$ | 90,000 |
| 2020021 | REMOVAL OF CONCRETE CURB AND GUTTER | L.FT. | 10,000 | \$ | 3.00 | \$ | 30,000 |
| 2020027 | REMOVAL OF CONCRETE BARRIER | L.FT. | 2,783 | \$ | 20.00 | \$ | 55,660 |
| 2020036 | REMOVAL OF ASPHALTIC CONCRETE PAVEMENT | SQ.YD. | 88,045 | \$ | 2.50 | \$ | 220,113 |
| 2020041 | REMOVAL OF PIPE | L.FT. | 308 | \$ | 100.00 | \$ | 30,800 |
| 2020048 | REMOVAL OF STRUCTURE (END SECTION) | EACH | 16 | \$ | 300.00 | \$ | 4,800 |
| 2020050 | REMOVE (HEADWALL) | EACH | 25 | \$ | 2,000.00 | \$ | 50,000 |
| 2020053 | REMOVE (SPILLWAY) | EACH | 1 | \$ | 1,000.00 | \$ | 1,000 |
| 2020054 | REMOVE (CATCH BASIN) | EACH | - | \$ | 500.00 | \$ | - |
| 2020071 | REMOVE GUARD RAIL | L.FT. | 51,914 | \$ | 3.50 | \$ | 181,699 |
| 2020080 | REMOVE BITUMINOUS PAVEMENT (MILLING) (1/2") | SQ.YD. | 610,250 | \$ | 3.00 | \$ | 1,830,750 |
| 2020101 | REMOVE FENCE | L.FT. | - | \$ | 3.00 | \$ | - |
| 2030301 | ROADWAY EXCAVATION | CU.YD. | 725,000 | \$ | 6.00 | \$ | 4,350,000 |
| 2030305 | ROCK EXCAVATION | CU.YD. | 740,000 | \$ | 15.00 | \$ | 11,100,000 |
| 3030022 | AGGREGATE BASE, CLASS 2 | CU.YD. | 232,468 | \$ | 36.00 | \$ | 8,368,848 |
| 4040111 | BITUMINOUS TACK COAT | TON | 843 | \$ | 500.00 | \$ | 421,500 |
| 4040116 | APPLY BITUMINOUS TACK COAT | HOUR | 1,396 | \$ | 150.00 | \$ | 209,400 |
| 4040125 | FOG COAT | TON | 180 | \$ | 600.00 | \$ | 108,000 |
| 4040163 | BLOTTER MATERIAL | TON | 539 | \$ | 55.00 | \$ | 29,645 |
| 4040270 | ASPHALT BINDER (PG 70-10) | TON | 14,919 | \$ | 600.00 | \$ | 8,951,400 |
| 4140040 | ASPHALTIC CONCRETE FRICTION COURSE (ASPHALT-RUBBER) | TON | 31,382 | \$ | 50.00 | Ş | 1,569,100 |
| 4140042 | ASPHALT RUBBER MATERIAL (FOR AR-ACFC) | TON | 2,825 | \$ | 550.00 | Ş | 1,553,750 |
| 4140044 | MINERAL ADMIXTURE (FOR AR-ACFC) | TON | 286 | \$ | 90.00 | Ş | 25,740 |
| 4160004 | ASPHALTIC CONCRETE (3/4" MIX) (END PRODUCT) (SPECIAL MIX) | TON | 298,378 | \$ | 35.00 | Ş | 10,443,230 |
| 4160031 | MINERAL ADMIXTURE | TON | 2,835 | \$ | 90.00 | \$ | 255,150 |
| 5010011 | PIPE, CORRUGATED METAL, 24" | L.FT. | 908 | \$ | 80.00 | \$ | 72,640 |
| 5010017 | PIPE, CORRUGATED METAL, 30" | L.FT. | 1,490 | Ş | 110.00 | Ş | 163,900 |
| 5010025 | PIPE, CORRUGATED METAL, 36" | L.FT. | 932 | Ş | 150.00 | Ş | 139,800 |
| 5010030 | PIPE, CORRUGATED METAL, 42" | L.FT. | 34 | Ş | 170.00 | Ş | 5,780 |
| 5010035 | PIPE, CORRUGATED METAL, 48" | L.FI. | 11/ | Ş | 2/0.00 | Ş | 31,590 |
| 5010040 | PIPE, CORRUGATED METAL, 54" | L.FI. | 11 | Ş | 300.00 | \$ | 3,300 |
| 5010045 | PIPE, CORRUGATED METAL, 50" | L.FI. | 115 | \$ | 320.00 | \$ | 36,800 |
| 5010060 | PIPE, CORRUGATED METAL, 78 | L.FI. | 21 | \$ ¢ | 400.00 | \$ ¢ | 8,400 |
| 5010005 | PIPE, CORRUGATED METAL, 84 | L.FI. | 29 | \$ ¢ | 420.00 | \$ ¢ | 12,180 |
| 5010107 | PIPE, CORRUGATED METAL, SLOTTED, 18 | L.FI. | - | Ş ¢ | 170.00 | ş | - |
| 5010251 | STODM DRAIN DIDE 18" | L.FT. | - | ې د | 80.00 | ې د | - |
| 5012516 | | L.FT. | - | ې د | 85.00 | ې د | |
| 501/119 | | EACH | - | ې د | 1 700 00 | ې د | |
| 5014524 | ELARED END SECTION (18) (C-13.20) | EACH | - | э с | 2,000,00 | ç | 19 000 |
| 5014524 | ELARED END SECTION, 24 (C-13.20 OR C-13.25) (PIPE COLVERT) | EACH | 22 | э ¢ | 2,000.00 | ç | 18,000 |
| 5014536 | ELARED END SECTION, 30 (C-13.20 OR C-13.25) (PIPE COLVERT) | EACH | 22 | э ¢ | 2,200.00 | ç | 54 600 |
| 5014530 | ELARED END SECTION, 30 (C-13.20 OR C-13.25) (PIPE COLVERT) | EACH | 21 | э ¢ | 2,000.00 | ç | 5.400 |
| 5014542 | ELARED END SECTION, 42 (C-13.20 OR C-13.25) (PIPE COLVERT) | EACH | 2 | э ¢ | 3,000,00 | ç | 12 000 |
| 5014548 | METAL SAFETY END SECTION (18") | EACH | 4 | э ¢ | 1,400,00 | ç | 12,000 |
| 5014624 | METAL SAFETY END SECTION (24 ") | EACH | 16 | Ś | 1,400.00 | ¢ | 30,400 |
| 5014630 | METAL SAFETY END SECTION (20 ") | EACH | 8 | Ś | 2 200 00 | ¢ | 17 600 |
| 5014636 | METAL SAFETY END SECTION (36") | EACH | 1 | Ś | 2,200.00 | Ś | 2 500 |
| 5014642 | METAL SAFETY END SECTION (30) | EACH | | Ś | 2,500.00 | Ś | 2,500 |
| 5014660 | METAL SAFETY END SECTION (60") | EACH | | Ś | 2,000.00 | Ś | |
| 5014699 | METAL SAFETY END SECTION (30") (DOUBLE) | EACH | | Ś | 3 500 00 | Ś | |
| 5030604 | CONCRETE CATCH BASIN (C-15 92) H=8' OR LESS | FACH | | Ś | 5,000,00 | Ś | |
| 5041996 | DRAINAGE STRUCTURE (HEADWALL) | FACH | 10 | Ś | 5,000.00 | Ś | 50.000 |
| 704X001 | PAVEMENT MARKING & SIGNING | | 10 | ¢ | 767 570 00 | Ś | 767 570 |
| 731X001 | LIGHTING | L SUM | - | Ť | | Ś | - |
| 732X001 | ITS - COMMUNICATION AND ELECTRICAL INFRASTRUCTURE | L. FT. | 172.000 | Ś | 40.00 | Ś | 6.880.000 |
| 732X002 | ITS - COMMUNICATION NODES | EACH | 1 | Ś | 200,000.00 | Ś | 200.000 |
| 732X003 | ITS - DETECTION (STATIONS) | EACH | - | Ś | 20,000.00 | Ś | - |
| 732X005 | ITS - POWER (ELECTRICAL SERVICE) | L, FT. | 145.000 | Ś | 4.50 | Ś | 652,500 |
| 732X007 | ITS - CCTV ASSEMBLY | EACH | 21.0,000 | Ś | 25,000.00 | Ś | 600.000 |
| 732X008 | ITS - DMS (NEW SIGNS AND STRUCTURES) | EACH | 2 | Ś | 175.000.00 | Ś | 350.000 |
| 732X009 | ITS - MISCELLANEOUS ITEMS | L. SUM | 1 | \$ | 180,000.00 | \$ | 180,000 |

| 7320714 | UTILITY RELOCATION WORK |
|-------------------------------|---|
| 807X001 | LANDSCAPING (LANDSCAPE & IRRIGATION) |
| 9020002 | CHAIN LINK FENCE, TYPE 1 (48") |
| 9050001 | GUARD RAIL, W-BEAM, SINGLE FACE |
| 9050026 | GUARD RAIL TERMINAL (TANGENT TYPE) |
| 9050036 | GUARD RAIL, ANCHOR ASSEMBLY |
| 9100009 | CONCRETE BARRIER (VARIABLE HEIGHT) |
| 9100012 | CONCRETE BARRIER (DETAIL K) |
| 9130001 | RIPRAP (DUMPED) |
| 9140137 | SOUND BARRIER WALL (MASONRY) |
| 9140153 | RETAINING WALL (REINFORCED CONCRETE CANTILEVER) |
| 9160001 | EMBANKMENT CURB |
| 9240050 | NEW RIVER BRIDGES (WIDENING) |
| 9240051 | NEW RIVER TI BRIDGES (WIDENING) |
| 9240052 | MOORES GULCH NB BRIDGE (WIDENING) |
| 9240053 | LITTLE SQUAW CREEK NB BRIDGE (WIDENING) |
| 9240054 | AGUA FRIA RIVER BRIDGE (WIDENING) |
| 9240055 | COLDWATER CANYON TI BRIDGES (WIDENING) |
| 9240056 | MOORES GULCH GRADER ROAD |
| 9240150 | REINFORCED CONCRETE BOX CULVERT (6X4) |
| 9240151 | REINFORCED CONCRETE BOX CULVERT (6X6) |
| 9240152 | REINFORCED CONCRETE BOX CULVERT (6X7) |
| 9240153 | REINFORCED CONCRETE BOX CULVERT (8X7) |
| 9240154 | REINFORCED CONCRETE BOX CULVERT (2-8X7) |
| 9240155 | REINFORCED CONCRETE BOX CULVERT (10X3) |
| 9240156 | REINFORCED CONCRETE BOX CULVERT (10X4) |
| 9240157 | REINFORCED CONCRETE BOX CULVERT (10X8) |
| 9240158 | REINFORCED CONCRETE BOX CULVERT (2-10X8) |
| 0040450 | DEINIGOROED CONCRETE DOV CULLVEDT (10V10) |
| 9240159 | REINFORCED CONCRETE BOX CULVERT (10X10) |
| 9240159 9240160 9240161 | REINFORCED CONCRETE BOX CULVERT (10X10) REINFORCED CONCRETE BOX CULVERT (2-10X10) REINFORCED CONCRETE BOX CULVERT (3-10X10) |
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| 9240159 9240160 9240161 | REINFORCED CONCRETE BOX CULVERT (10X10) REINFORCED CONCRETE BOX CULVERT (2-10X10) REINFORCED CONCRETE BOX CULVERT (3-10X10) MISCELLANEOUS WORK (15%) DUST PALLIATIVE (1%) FURNISH WATER (1%) MAINTENANCE AND PROTECTION OF TRAFFIC (15%) EROSION CONTROL AND POLLUTION PREVENTION (1%) CONTRACTOR QUALITY CONTROL (2%) CONSTRUCTION SURVEYING AND LAYOUT (2%) |
| 9240159 9240160 9240161 | REINFORCED CONCRETE BOX CULVERT (10X10) REINFORCED CONCRETE BOX CULVERT (2-10X10) REINFORCED CONCRETE BOX CULVERT (3-10X10) MISCELLANEOUS WORK (15%) DUST PALLIATIVE (1%) FURNISH WATER (1%) MAINTENANCE AND PROTECTION OF TRAFFIC (15%) EROSION CONTROL AND POLLUTION PREVENTION (1%) CONTRACTOR QUALITY CONTROL (2%) CONSTRUCTION SURVEYING AND LAYOUT (2%) |
| 9240159 9240160 9240161 | REINFORCED CONCRETE BOX CULVERT (10X10) REINFORCED CONCRETE BOX CULVERT (2-10X10) REINFORCED CONCRETE BOX CULVERT (3-10X10) MISCELLANEOUS WORK (15%) DUST PALLIATIVE (1%) FURNISH WATER (1%) MAINTENANCE AND PROTECTION OF TRAFFIC (15%) EROSION CONTROL AND POLLUTION PREVENTION (1%) CONTRACTOR QUALITY CONTROL (2%) CONSTRUCTION SURVEYING AND LAYOUT (2%) MOBILIZATION (10%) |
| 9240159 9240160 9240161 | REINFORCED CONCRETE BOX CULVERT (10X10) REINFORCED CONCRETE BOX CULVERT (2-10X10) REINFORCED CONCRETE BOX CULVERT (3-10X10) MISCELLANEOUS WORK (15%) DUST PALLIATIVE (1%) FURNISH WATER (1%) MAINTENANCE AND PROTECTION OF TRAFFIC (15%) EROSION CONTROL AND POLLUTION PREVENTION (1%) CONTRACTOR QUALITY CONTROL (2%) MOBILIZATION SURVEYING AND LAYOUT (2%) MOBILIZATION (10%) |
| 9240159 9240160 9240161 | REINFORCED CONCRETE BOX CULVERT (10X10) REINFORCED CONCRETE BOX CULVERT (2-10X10) REINFORCED CONCRETE BOX CULVERT (3-10X10) MISCELLANEOUS WORK (15%) DUST PALLIATIVE (1%) FURNISH WATER (1%) MAINTENANCE AND PROTECTION OF TRAFFIC (15%) EROSION CONTROL AND POLLUTION PREVENTION (1%) CONTRACTOR QUALITY CONTROL (2%) CONSTRUCTION SURVEYING AND LAYOUT (2%) MOBILIZATION (10%) CONTINGENCIES CONSTRUCTION ENGINEERING |
| 9240159 9240160 9240161 | REINFORCED CONCRETE BOX CULVERT (10X10) REINFORCED CONCRETE BOX CULVERT (2-10X10) REINFORCED CONCRETE BOX CULVERT (3-10X10) MISCELLANEOUS WORK (15%) DUST PALLIATIVE (1%) FURNISH WATER (1%) MAINTENANCE AND PROTECTION OF TRAFFIC (15%) EROSION CONTROL AND POLLUTION PREVENTION (1%) CONTRACTOR QUALITY CONTROL (2%) CONSTRUCTION SURVEYING AND LAYOUT (2%) MOBILIZATION (10%) CONTINGENCIES CONSTRUCTION ENGINEERING AC QUALITY INCENTIVE |
| 9240159 9240160 9240161 | REINFORCED CONCRETE BOX CULVERT (10X10) REINFORCED CONCRETE BOX CULVERT (2-10X10) REINFORCED CONCRETE BOX CULVERT (3-10X10) MISCELLANEOUS WORK (15%) DUST PALLIATIVE (1%) FURNISH WATER (1%) MAINTENANCE AND PROTECTION OF TRAFFIC (15%) EROSION CONTROL AND POLLUTION PREVENTION (1%) CONTRACTOR QUALITY CONTROL (2%) CONSTRUCTION SURVEYING AND LAYOUT (2%) MOBILIZATION (10%) CONTINGENCIES CONSTRUCTION ENGINEERING AC QUALITY INCENTIVE AR-ACFC SMOOTHNESS INCENTIVE |
| 9240159 9240160 9240161 | REINFORCED CONCRETE BOX CULVERT (10X10) REINFORCED CONCRETE BOX CULVERT (2-10X10) REINFORCED CONCRETE BOX CULVERT (3-10X10) MISCELLANEOUS WORK (15%) DUST PALLIATIVE (1%) FURNISH WATER (1%) MAINTENANCE AND PROTECTION OF TRAFFIC (15%) EROSION CONTROL AND POLLUTION PREVENTION (1%) CONTRACTOR QUALITY CONTROL (2%) CONSTRUCTION SURVEYING AND LAYOUT (2%) MOBILIZATION (10%) CONTINGENCIES CONSTRUCTION ENGINEERING AC QUALITY INCENTIVE AR-ACFC SMOOTHNESS INCENTIVE PUBLIC RELATIONS |
| 9240159 9240160 9240161 | REINFORCED CONCRETE BOX CULVERT (10X10) REINFORCED CONCRETE BOX CULVERT (2-10X10) REINFORCED CONCRETE BOX CULVERT (3-10X10) MISCELLANEOUS WORK (15%) DUST PALLIATIVE (1%) FURNISH WATER (1%) MAINTENANCE AND PROTECTION OF TRAFFIC (15%) EROSION CONTROL AND POLLUTION PREVENTION (1%) CONTRACTOR QUALITY CONTROL (2%) CONSTRUCTION SURVEYING AND LAYOUT (2%) MOBILIZATION (10%) CONTINGENCIES CONSTRUCTION ENGINEERING AC QUALITY INCENTIVE AR-ACFC SMOOTHNESS INCENTIVE PUBLIC RELATIONS FINAL DESIGN COSTS (10%) |
| 9240159 9240160 9240161 | REINFORCED CONCRETE BOX CULVERT (10X10) REINFORCED CONCRETE BOX CULVERT (2-10X10) REINFORCED CONCRETE BOX CULVERT (3-10X10) MISCELLANEOUS WORK (15%) DUST PALLIATIVE (1%) FURNISH WATER (1%) MAINTENANCE AND PROTECTION OF TRAFFIC (15%) EROSION CONTROL AND POLLUTION PREVENTION (1%) CONTRACTOR QUALITY CONTROL (2%) CONSTRUCTION SURVEYING AND LAYOUT (2%) MOBILIZATION (10%) CONTINGENCIES CONSTRUCTION ENGINEERING AC QUALITY INCENTIVE AR-ACFC SMOOTHNESS INCENTIVE PUBLIC RELATIONS FINAL DESIGN COSTS (10%) RIGHT OF WAY |
| 9240159 9240160 9240161 | REINFORCED CONCRETE BOX CULVERT (10X10) REINFORCED CONCRETE BOX CULVERT (2-10X10) REINFORCED CONCRETE BOX CULVERT (3-10X10) MISCELLANEOUS WORK (15%) DUST PALLIATIVE (1%) FURNISH WATER (1%) MAINTENANCE AND PROTECTION OF TRAFFIC (15%) EROSION CONTROL AND POLLUTION PREVENTION (1%) CONTRACTOR QUALITY CONTROL (2%) CONSTRUCTION SURVEYING AND LAYOUT (2%) MOBILIZATION (10%) CONTINGENCIES CONSTRUCTION ENGINEERING AC QUALITY INCENTIVE PUBLIC RELATIONS FINAL DESIGN COSTS (10%) RIGHT OF WAY |
| 9240159 9240160 9240161 | REINFORCED CONCRETE BOX CULVERT (10X10) REINFORCED CONCRETE BOX CULVERT (2-10X10) REINFORCED CONCRETE BOX CULVERT (3-10X10) MISCELLANEOUS WORK (15%) DUST PALLIATIVE (1%) FURNISH WATER (1%) MAINTENANCE AND PROTECTION OF TRAFFIC (15%) EROSION CONTROL AND POLLUTION PREVENTION (1%) CONTRACTOR QUALITY CONTROL (2%) CONSTRUCTION SURVEYING AND LAYOUT (2%) MOBILIZATION (10%) CONTINGENCIES CONSTRUCTION ENGINEERING AC QUALITY INCENTIVE PUBLIC RELATIONS FINAL DESIGN COSTS (10%) RIGHT OF WAY INDIRECT COST ALLOCATION (10.02% FY19) |
| 9240159 9240160 9240161 | REINFORCED CONCRETE BOX CULVERT (10X10) REINFORCED CONCRETE BOX CULVERT (2-10X10) REINFORCED CONCRETE BOX CULVERT (3-10X10) MISCELLANEOUS WORK (15%) DUST PALLIATIVE (1%) FURNISH WATER (1%) MAINTENANCE AND PROTECTION OF TRAFFIC (15%) EROSION CONTROL AND POLLUTION PREVENTION (1%) CONTRACTOR QUALITY CONTROL (2%) CONSTRUCTION SURVEYING AND LAYOUT (2%) MOBILIZATION (10%) CONTINGENCIES CONSTRUCTION ENGINEERING AC QUALITY INCENTIVE AR-ACFC SMOOTHNESS INCENTIVE PUBLIC RELATIONS FINAL DESIGN COSTS (10%) RIGHT OF WAY INDIRECT COST ALLOCATION (10.02% FY19) |

STANLEY CONSULTANTS, INC.

| | L.SUM | 1 | \$ | 3,600,000.00 | \$ | 3,600,000 |
|--|---------|--|--------|--|---|--|
| | MILE | 16 | \$ | 390,000.00 | \$ | 6,240,000 |
| | L.FT. | 15,000 | \$ | 10.00 | \$ | 150,000 |
| | L.FT. | 43,463 | \$ | 20.00 | \$ | 869,260 |
| | EACH | 49 | \$ | 3,000.00 | \$ | 147,000 |
| | EACH | 49 | \$ | 1,000.00 | \$ | 49,000 |
| | L.FT. | 2,200 | \$ | 200.00 | \$ | 440,000 |
| | L.FT. | 28,833 | \$ | 40.00 | \$ | 1,153,320 |
| | CU.YD. | 1,400 | \$ | 80.00 | \$ | 112,000 |
| | SQ.FT. | 97,997 | \$ | 35.00 | \$ | 3,429,895 |
| | SQ.FT. | 22,000 | \$ | 60.00 | \$ | 1,320,000 |
| | L.FT. | 43,463 | \$ | 7.00 | \$ | 304,241 |
| | SQ. FT | 14,580 | \$ | 170.00 | \$ | 2,478,600 |
| | SQ. FT. | 7,460 | \$ | 170.00 | \$ | 1,268,200 |
| | SQ. FT. | 4,980 | \$ | 180.00 | \$ | 896,400 |
| | SQ. FT. | 11,820 | \$ | 170.00 | \$ | 2,009,400 |
| | SQ. FT. | 15,980 | \$ | 170.00 | \$ | 2,716,600 |
| | SQ.FT. | 4,480 | \$ | 155.00 | \$ | 694,400 |
| | L. SUM | 1 | \$ | 331,000.00 | \$ | 331,000 |
| | L. FT. | 18 | \$ | 850.00 | \$ | 15,300 |
| | L. FT. | 24 | \$ | 1,170.00 | \$ | 28,080 |
| | L. FT. | 21 | \$ | 950.00 | \$ | 19,950 |
| | L. FT. | 50 | \$ | 1,600.00 | \$ | 80,000 |
| | L. FT. | 58 | Ş | 1,870.00 | Ş | 108,460 |
| | L.FI. | 15 | Ş | 1,350.00 | Ş | 20,250 |
| | L.FI. | 12 | \$ | 1,670.00 | \$ | 20,040 |
| | L.FI. | 225 | ې د | 2,540.00 | ې د | 252 250 |
| | L.FT. | 223 | ې د | 2 170 00 | ç | 182 280 |
| | L.FT. | - | Ś | 2,170.00 | ¢ | 102,200 |
| | | | Ŷ | 2,000100 | Ŷ | |
| | L. FT. | 21 | \$ | 4,310.00 | \$ | 90,510 |
| | L. FT. | 21 | \$ | 4,310.00 SUBTOTAL | \$ \$ | 90,510 89,546,941 |
| | L. FT. | 21 | \$ | 4,310.00 SUBTOTAL | \$ \$ | 90,510 89,546,941 |
| | L. FT. | 21 COST | \$ | 4,310.00 SUBTOTAL 15.00% | \$ \$ \$ | 90,510 89,546,941 13,432,100 |
| Subtotal 1 | L. FT. | 21 COST | \$ | 4,310.00 SUBTOTAL 15.00% | \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 |
| Subtotal 1 | L. FT. | 21 COST | \$ | 4,310.00 SUBTOTAL 15.00% | \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 |
| Subtotal 1 | L. FT. | 21 COST COST | \$ | 4,310.00 SUBTOTAL 15.00% 1.00% | \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 |
| Subtotal 1 | L FT. | 21 COST COST COST | \$ | 4,310.00 SUBTOTAL 15.00% 1.00% | \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 |
| Subtotal 1 | L FT. | COST COST COST COST COST | \$ | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 15.00% | \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 15,446,900 |
| Subtotal 1 | L FT. | COST COST COST COST COST COST | \$ | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 15.00% 1.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 15,446,900 1,029,800 |
| Subtotal 1 | L FT. | COST COST COST COST COST COST COST | \$ | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 1.00% 1.00% 2.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 15,446,900 1,029,800 2,059,600 |
| Subtotal 1 | L. FT. | COST COST COST COST COST COST COST | \$ | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 1.00% 2.00% 2.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 15,446,900 1,029,800 2,059,600 2,059,600 |
| Subtotal 1 Subtotal 2 | L. FT. | COST COST COST COST COST COST COST | | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 1.00% 2.00% 2.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 15,446,900 1,029,800 2,059,600 2,059,600 125,634,541 |
| Subtotal 1 Subtotal 2 | L. FT. | COST COST COST COST COST COST COST | | 4,310.00 SUBTOTAL 15.00% 1.00% 15.00% 1.00% 2.00% 2.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 15,446,900 1,029,800 2,059,600 2,059,600 125,634,541 |
| Subtotal 1 Subtotal 2 | L. FT. | COST COST COST COST COST COST COST COST | | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 1.00% 2.00% 2.00% 10.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 1,029,800 1,029,800 2,059,600 2,059,600 125,634,541 12,563,500 |
| Subtotal 1 Subtotal 2 Subtotal 3 | L. FT. | COST COST COST COST COST COST COST COST | | 4,310.00 SUBTOTAL 15.00% 1.00% 15.00% 1.00% 2.00% 2.00% 10.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 1,029,800 1,029,800 2,059,600 2,059,600 2,059,600 125,634,541 12,563,500 138,198,041 |
| Subtotal 1 Subtotal 2 Subtotal 3 | L. FT. | COST COST COST COST COST COST COST COST | | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 2.00% 2.00% 10.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 1,029,800 2,059,600 2,059,600 2,059,600 125,634,541 12,563,500 138,198,041 |
| Subtotal 1 Subtotal 2 Subtotal 3 | | COST COST COST COST COST COST COST COST | | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 2.00% 2.00% 10.00% 10.00% 10.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 1,029,800 2,059,600 2,059,600 2,059,600 125,634,541 12,563,500 138,198,041 6,910,000 20,739,800 |
| Subtotal 1 Subtotal 2 Subtotal 3 | 200 278 | COST COST COST COST COST COST COST COST | | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 2.00% 2.00% 10.00% 5.00% 10.00% 2.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 1,029,800 2,059,600 2,059,600 125,634,541 12,563,500 138,198,041 6,910,000 20,729,800 |
| Subtotal 1 Subtotal 2 Subtotal 3 | L. FT. | COST COST COST COST COST COST COST COST | | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 1.00% 2.00% 2.00% 10.00% 5.00% 15.00% 3.00 9.000 | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 1,029,800 2,059,600 2,059,600 125,634,541 12,563,500 138,198,041 6,910,000 20,729,800 895,200 840,000 |
| Subtotal 1 Subtotal 2 Subtotal 3 | L. FT. | COST COST COST COST COST COST COST COST | \$ | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 1.00% 2.00% 2.00% 10.00% 5.00% 15.00% 3.00 9,000 | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 1,029,800 2,059,600 2,059,600 125,634,541 12,563,500 138,198,041 6,910,000 20,729,800 895,200 864,000 20,000 |
| Subtotal 1 Subtotal 2 Subtotal 3 Subtotal 4 | L. FT. | COST COST COST COST COST COST COST COST | \$ | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 1.00% 2.00% 2.00% 10.00% 5.00% 15.00% 3.00 9,000 1 | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 1,029,800 2,059,600 2,059,600 125,634,541 12,563,500 138,198,041 6,910,000 20,729,800 895,200 864,000 20,000 167,617,041 |
| Subtotal 1 Subtotal 2 Subtotal 3 Subtotal 4 | L. FT. | COST COST COST COST COST COST COST COST | | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 1.00% 2.00% 2.00% 10.00% 5.00% 15.00% 15.00% 15.00% 10.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 1,029,800 2,059,600 2,059,600 125,634,541 12,563,500 138,198,041 6,910,000 20,729,800 895,200 864,000 20,000 167,617,041 |
| Subtotal 1 Subtotal 2 Subtotal 3 Subtotal 4 | L. FT. | 21 COST COST COST COST COST COST COST TON LN. MI. | \$ | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 1.00% 2.00% 2.00% 10.00% 5.00% 15.00% 15.00% 10.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 1,029,800 2,059,600 2,059,600 125,634,541 12,563,500 138,198,041 6,910,000 20,729,800 895,200 884,000 20,000 167,617,041 16,761,800 |
| Subtotal 1 Subtotal 2 Subtotal 3 Subtotal 4 | L. FT. | 21 COST COST COST COST COST COST COST TON LN. MI. | \$ | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 1.00% 2.00% 2.00% 10.00% 5.00% 15.00% 15.00% 10.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 1,029,800 2,059,600 2,059,600 125,634,541 12,563,500 138,198,041 6,910,000 20,729,800 895,200 884,000 20,000 167,617,041 16,761,800 |
| Subtotal 1 Subtotal 2 Subtotal 3 Subtotal 4 Subtotal 5 | L. FT. | COST COST COST COST COST COST COST COST | | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 1.00% 2.00% 2.00% 10.00% 5.00% 15.00% 10.00% 10.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 1,029,800 2,059,600 2,059,600 125,634,541 12,563,500 138,198,041 6,910,000 20,729,800 895,200 844,000 20,000 167,617,041 16,761,800 - |
| Subtotal 1 Subtotal 2 Subtotal 3 Subtotal 4 Subtotal 5 | L. FT. | COST COST COST COST COST COST COST COST | \$ | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 1.00% 2.00% 2.00% 10.00% 5.00% 15.00% 10.00% 10.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 1,029,800 2,059,600 2,059,600 125,634,541 12,563,500 138,198,041 6,910,000 20,729,800 895,200 864,000 20,000 167,617,041 16,761,800 - 184,378,841 |
| Subtotal 1 Subtotal 2 Subtotal 3 Subtotal 4 Subtotal 5 | L. FT. | COST COST COST COST COST COST COST COST | \$ | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 1.00% 2.00% 2.00% 10.00% 5.00% 15.00% 10.00% 10.00% 10.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 1,029,800 2,059,600 2,059,600 125,634,541 12,563,500 138,198,041 6,910,000 20,729,800 895,200 864,000 20,000 167,617,041 - 184,378,841 - 18,474,800 |
| Subtotal 1 Subtotal 2 Subtotal 3 Subtotal 4 Subtotal 5 | L. FT. | COST COST COST COST COST COST COST COST | \$ | 4,310.00 SUBTOTAL 15.00% 1.00% 1.00% 1.00% 2.00% 2.00% 10.00% 5.00% 15.00% 10.00% 10.00% 10.00% | \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | 90,510 89,546,941 13,432,100 102,979,041 1,029,800 1,029,800 1,029,800 2,059,600 2,059,600 125,634,541 12,563,500 138,198,041 6,910,000 20,729,800 895,200 864,000 20,000 167,617,041 16,761,800 - 184,378,841 18,474,800 |

| Item No. | Item Description | Unit | Quantity | Unit Price | Total Price |
|----------|---|--------|-----------|---------------|------------------|
| 2010011 | CLEARING AND GRUBBING | ACRE | 50 | \$ 600.00 | \$ 30,000 |
| 2020001 | REMOVAL OF STRUCTURES AND OBSTRUCTIONS | L.SUM | - | | \$ - |
| 2020002 | REMOVE BRIDGE | L.SUM | 1 | \$ 400,000.00 | \$ 400,000 |
| 2020021 | REMOVAL OF CONCRETE CURB AND GUTTER | L.FT. | - | \$ 3.00 | \$ - |
| 2020027 | REMOVAL OF CONCRETE BARRIER | L.FT. | 1,123 | \$ 20.00 | \$ 22,460 |
| 2020036 | REMOVAL OF ASPHALTIC CONCRETE PAVEMENT | SQ.YD. | - | \$ 2.50 | \$ - |
| 2020041 | REMOVAL OF PIPE | L.FT. | 70 | \$ 100.00 | \$ 7,000 |
| 2020048 | REMOVAL OF STRUCTURE (END SECTION) | EACH | 7 | \$ 300.00 | \$ 2,100 |
| 2020050 | REMOVE (HEADWALL) | EACH | 11 | \$ 2,000.00 | \$ 22,000 |
| 2020053 | REMOVE (SPILLWAY) | EACH | 1 | \$ 1,000.00 | \$ 1,000 |
| 2020054 | REMOVE (CATCH BASIN) | EACH | 4 | \$ 500.00 | \$ 2,000 |
| 2020071 | REMOVE GUARD RAIL | L.FT. | 13,996 | \$ 3.50 | \$ 48,986 |
| 2020080 | REMOVE BITUMINOUS PAVEMENT (MILLING) (1/2") | SQ.YD. | 98,785 | \$ 3.00 | \$ 296,355 |
| 2020101 | REMOVE FENCE | L.FT. | 1,335 | \$ 3.00 | \$ 4,005 |
| 2030301 | ROADWAY EXCAVATION | CU.YD. | 340,000 | \$ 6.00 | \$ 2,040,000 |
| 2030305 | ROCK EXCAVATION | CU.YD. | 1,580,000 | \$ 15.00 | \$ 23,700,000 |
| 3030022 | AGGREGATE BASE, CLASS 2 | CU.YD. | 104,687 | \$ 36.00 | \$ 3,768,732 |
| 4040111 | BITUMINOUS TACK COAT | TON | 358 | \$ 500.00 | \$ 179,000 |
| 4040116 | APPLY BITUMINOUS TACK COAT | HOUR | 596 | \$ 150.00 | \$ 89,400 |
| 4040125 | FOG COAT | TON | 82 | \$ 600.00 | \$ 49,200 |
| 4040163 | BLOTTER MATERIAL | TON | 244 | \$ 55.00 | \$ 13,420 |
| 4040270 | ASPHALT BINDER (PG 70-10) | TON | 6,965 | \$ 600.00 | \$ 4,179,000 |
| 4140040 | ASPHALTIC CONCRETE FRICTION COURSE (ASPHALT-RUBBER) | TON | 11,487 | \$ 50.00 | \$ 574,350 |
| 4140042 | ASPHALT RUBBER MATERIAL (FOR AR-ACFC) | TON | 1,034 | \$ 550.00 | \$ 568,700 |
| 4140044 | MINERAL ADMIXTURE (FOR AR-ACFC) | TON | 105 | \$ 90.00 | \$ 9,450 |
| 4160004 | ASPHALTIC CONCRETE (3/4" MIX) (END PRODUCT) (SPECIAL MIX) | TON | 139,293 | \$ 35.00 | \$ 4,875,255 |
| 4160031 | MINERAL ADMIXTURE | TON | 1,324 | \$ 90.00 | \$ 119,160 |
| 5010011 | PIPE, CORRUGATED METAL, 24" | L.FT. | 1,294 | \$ 80.00 | \$ 103,520 |
| 5010017 | PIPE, CORRUGATED METAL, 30" | L.FT. | 342 | \$ 110.00 | \$ 37,620 |
| 5010025 | PIPE, CORRUGATED METAL, 36" | L.FT. | 1,163 | \$ 150.00 | \$ 174,450 |
| 5010030 | PIPE, CORRUGATED METAL, 42" | L.FT. | 112 | \$ 170.00 | \$ 19,040 |
| 5010035 | PIPE, CORRUGATED METAL, 48" | L.FT. | 67 | \$ 270.00 | \$ 18,090 |
| 5010040 | PIPE, CORRUGATED METAL, 54" | L.FT. | 240 | \$ 300.00 | \$ 72,000 |
| 5010045 | PIPE, CORRUGATED METAL, 60" | L.FT. | 61 | \$ 320.00 | \$ 19,520 |
| 5010060 | PIPE, CORRUGATED METAL, 78" | L.FT. | - | \$ 400.00 | \$ - |
| 5010065 | PIPE, CORRUGATED METAL, 84" | L.FT. | - | \$ 420.00 | \$ - |
| 5010107 | PIPE, CORRUGATED METAL, SLOTTED, 18" | L.FT. | 355 | \$ 170.00 | \$ 60,350 |
| 5010251 | PIPE, CORRUGATED METAL, 43" X 27" | L.FT. | - | \$ 80.00 | \$ - |
| 5012518 | STORM DRAIN PIPE, 18" | L.FT. | 2,419 | \$ 80.00 | \$ 193,520 |
| 5012524 | STORM DRAIN PIPE, 24" | L.FT. | 135 | \$ 85.00 | \$ 11,475 |
| 5014118 | FLARED END SECTION (18") (C-13.20) | EACH | 19 | \$ 1,700.00 | \$ 32,300 |
| 5014524 | FLARED END SECTION, 24" (C-13.20 OR C-13.25) (PIPE CULVERT) | EACH | 12 | \$ 2,000.00 | \$ 24,000 |
| 5014530 | FLARED END SECTION, 30" (C-13.20 OR C-13.25) (PIPE CULVERT) | EACH | 3 | \$ 2,200.00 | \$ 6,600 |
| 5014536 | FLARED END SECTION, 36" (C-13.20 OR C-13.25) (PIPE CULVERT) | EACH | 7 | \$ 2,600.00 | \$ 18,200 |
| 5014542 | FLARED END SECTION, 42" (C-13.20 OR C-13.25) (PIPE CULVERT) | EACH | - | \$ 2,700.00 | \$ - |
| 5014548 | FLARED END SECTION, 48" (C-13.20 OR C-13.25) (PIPE CULVERT) | EACH | - | \$ 3,000.00 | \$ - |
| 5014618 | METAL SAFETY END SECTION (18") | EACH | 23 | \$ 1,400.00 | \$ 32,200 |
| 5014624 | METAL SAFETY END SECTION (24 ") | EACH | 15 | \$ 1,900.00 | \$ 28,500 |
| 5014630 | METAL SAFETY END SECTION (30 ") | EACH | 5 | \$ 2,200.00 | \$ 11,000 |
| 5014636 | METAL SAFETY END SECTION (36") | EACH | 8 | \$ 2,500.00 | \$ 20,000 |
| 5014642 | METAL SAFETY END SECTION (42") | EACH | 2 | \$ 2,600.00 | \$ 5,200 |
| 5014660 | METAL SAFETY END SECTION (60") | EACH | 2 | \$ 2,700.00 | \$ 5,400 |
| 5014699 | METAL SAFETY END SECTION (30") (DOUBLE) | EACH | 2 | \$ 3,500.00 | \$ 7,000 |
| 5030604 | CONCRETE CATCH BASIN (C-15.92) H=8' OR LESS | EACH | 49 | \$ 5,000.00 | \$ 245,000 |
| 5041996 | DRAINAGE STRUCTURE (HEADWALL) | EACH | 7 | \$ 5,000.00 | \$ 35,000 |
| 704X001 | PAVEMENT MARKING & SIGNING | L. SUM | 1 | \$ 817,670.00 | \$ 817,670 |
| 731X001 | LIGHTING | L. SUM | 1 | \$ 288,000.00 | \$ 288,000 |
| - | | | | | |

TABLE 63 – ESTIMATE OF PROBABLE CONSTRUCTION COST – FLEX LANES

| 732X001 | ITS - COMMUNICATION AND ELECTRICAL INFRASTRUCTURE |
|---------|---|
| 732X002 | ITS - COMMUNICATION NODES |
| 732X003 | ITS - DETECTION (STATIONS) |
| 732X005 | ITS - POWER (ELECTRICAL SERVICE) |
| 732X007 | ITS - CCTV ASSEMBLY |
| 732X008 | ITS - DMS (NEW SIGNS AND STRUCTURES) |
| 732X009 | ITS - MISCELLANEOUS ITEMS |
| 732X010 | ITS - LANE CONTROL SIGNALS |
| 732X011 | TRAFFIC GATE |
| 7320714 | UTILITY RELOCATION WORK |
| 807X001 | LANDSCAPING (LANDSCAPE & IRRIGATION) |
| 9020002 | CHAIN LINK FENCE, TYPE 1 (48") |
| 9050001 | GUARD RAIL, W-BEAM, SINGLE FACE |
| 9050026 | GUARD RAIL TERMINAL (TANGENT TYPE) |
| 9050036 | GUARD RAIL, ANCHOR ASSEMBLY |
| 9100201 | CONCRETE MEDIAN BARRIER |
| 9130001 | RIPRAP (DUMPED) |
| 9140153 | RETAINING WALL (REINFORCED CONCRETE CANTILEVER) |
| 9160001 | EMBANKMENT CUBB |
| 9240057 | BUMBLE BEE TI SB BRIDGE (NEW) |
| 9240152 | REINFORCED CONCRETE BOX CUI VERT (6X7) |
| 9240160 | REINFORCED CONCRETE BOX CUI VERT (2-10X10) |
| | |
| | |
| | MISCELLANEOUS WORK (15%) |
| | |
| | |
| | DUST PALLIATIVE (1%) |
| | EURNISH WATER (1%) |
| | MAINTENANCE AND PROTECTION OF TRAFFIC (12%) |
| | EROSION CONTROL AND POLILITION PREVENTION (1%) |
| | CONTRACTOR QUALITY CONTROL (2%) |
| | CONSTRUCTION SURVEYING AND LAYOUT (2%) |
| | CONSTRUCTION SOLVETING AND EXTOOP (220) |
| | |
| | |
| | MODILIZATION (10%) |
| | |
| | CONTINGENCIES |
| | |
| | |
| | |
| | |
| | PUDLIC RELATIONS |
| | |
| | FINAL DECIGN COSTS (10%) |
| | FINAL DESIGN COSTS (10%) |
| | KIGHT OF WAY |
| | |
| | |
| | ······································ |
| | INDIRECT COST ALLOCATION (10.02% FY19) |
| | |
| | |

| | L. FT. | 41,000 | \$ | 80.00 | \$ | 3,200,000 |
|------------|---------|------------|--------|-----------------|--------|-------------|
| | EACH | 1 | \$ | 200,000.00 | \$ | 200,000 |
| | EACH | 8 | \$ | 20,000.00 | \$ | 160,000 |
| | EACH | 206,000 | \$ | 4.50 | \$ | 1,000,000 |
| | EACH | 32 | \$ | 25,000.00 | \$ | 800,000 |
| | EACH | 2 | \$ | 175,000.00 | \$ | 350,000 |
| | L. SUM | 1 | \$ | 125,000.00 | \$ | 125,000 |
| | EACH | 12 | \$ | 6,000.00 | \$ | 72,000 |
| | EACH | 12 | \$ | 55,000.00 | \$ | 660,000 |
| | L.SUM | 1 | \$ | 500,000.00 | \$ | 500,000 |
| | MILE | 7 | \$ | 390,000.00 | \$ | 2,730,000 |
| | L.FT. | 1,000 | \$ | 10.00 | \$ | 10,000 |
| | L.FT. | 8,965 | \$ | 20.00 | \$ | 179,300 |
| | EACH | 13 | \$ | 3,000.00 | \$ | 39,000 |
| | EACH | 13 | \$ | 1,000.00 | \$ | 13,000 |
| | L.FT. | 33,774 | \$ | 50.00 | \$ | 1,688,700 |
| | CU.YD. | 695 | \$ | 80.00 | \$ | 55,600 |
| | SQ.FT. | 25,000 | \$ | 60.00 | \$ | 1,500,000 |
| | L.FT. | 8,965 | \$ | 7.00 | \$ | 62,755 |
| | SQ. FT | 7,000 | \$ | 200.00 | \$ | 1,400,000 |
| | L. FT. | 174 | \$ | 950.00 | \$ | 165,300 |
| | L. FT. | 56 | \$ | 2,580.00 | \$ | 144,480 |
| | | | | SUBTOTAL | \$ | 58,342,363 |
| | | | | | | |
| | | COST | | 15.00% | \$ | 8,751,400 |
| Subtotal 1 | | | | | \$ | 67,093,763 |
| | | | | | | |
| | | COST | | 1.00% | \$ | 671,000 |
| | | COST | | 1.00% | \$ | 671,000 |
| | | COST | | 12.00% | \$ | 8,051,300 |
| | | COST | | 1.00% | \$ | 671,000 |
| | | COST | | 2.00% | Ş | 1,341,900 |
| - • • • | | COST | | 2.00% | Ş | 1,341,900 |
| Subtotal 2 | | | | | Ş | 79,841,863 |
| | | 0007 | | 10.00% | ~ | |
| e | | COST | | 10.00% | Ş | /,984,200 |
| Subtotal 3 | | | | | Ş | 87,826,063 |
| | | | | E 00% | ė | 4 005 405 |
| | | | | 3.00% | ş | 4,391,400 |
| | 100.000 | TON | ć | 13.00% | ې د | 13,174,000 |
| | 139,293 | | ç ç | 3.00 | ې د | 417,900 |
| | 32 | LIN. IVII. | Ş | 9,000 | ې د | 288,000 |
| Cubtotal 4 | 20,000 | | | 1 | ې د | 20,000 |
| Subtotal 4 | | | | | ş | 100,117,303 |
| | | C097 | | 10.00% | ć | 10 611 900 |
| | 1.00 | ACRE | | 10.00/0 | ې د | 10,011,800 |
| | 1.83 | ACRE | | | Ş | - |
| Subtotal 5 | | | | | ć | 116 700 160 |
| Subtotal 5 | | | | | Ş | 110,729,103 |
| | | | | 10.02% | ć | 11 696 200 |
| | | | | 10.02/0 | ې | 11,050,300 |
| | | TOTAL | | EX LANES COSTS | ć | 128 500 000 |
| | | IUIA | L FLI | EX LAIVES CUSTS | ş | 120,500,000 |

APPENDIX A – AASHTO CONTROLLING DESIGN CRITERIA REPORT

VERTICAL AND HORIZONTAL MAINLINE CURVE INVENTORIES AND BRIDGE EVALUATION

Attachment 1 - Vertical Curve Inventory

Project Name: !-17, Anthem Way Traffic Interchange to Jct. SR 69 (Cordes Junction) Northbound

Project No: 17 MA 229 H6800 01L

Roadway Type: Divided Roadway (Uni-directional)

| VPI Station (ft) | Milepost | | Grade (%) | | Curve | Curve | Stopping Sight | Distance (ft) | Speed (mph) | | |
|------------------|----------|--------|-----------|-----------|-------------|-------|----------------|---------------|-------------|--------|--|
| VFI Station (It) | Begin | End | Approach | Departure | Length (ft) | Туре | Existing | Required | Existing | Posted | |
| 1500+00.00 | 229.10 | 229.30 | 1.7500 | 0.8330 | 1000.00 | Crest | 1677 | 802 | +100 | 75 | |
| 1512+00.00 | 229.40 | 229.50 | 0.8330 | 1.5500 | 800.00 | Sag | +9999 | 802 | +100 | 75 | |
| 1557+50.00 | 230.20 | 230.50 | 1.3530 | 0.1530 | 1400.00 | Crest | 1599 | 812 | +100 | 75 | |
| 1574+00.00 | 230.60 | 230.70 | 0.1690 | -0.5890 | 800.00 | Crest | 1823 | 824 | +100 | 75 | |
| 1594+00.00 | 230.90 | 231.10 | -0.5890 | 0.3000 | 1000.00 | Sag | +9999 | 824 | +100 | 75 | |
| 1614+00.00 | 231.20 | 231.50 | 0.3000 | 2.9000 | 1600.00 | Sag | 2682 | 810 | +100 | 75 | |
| 1650+00.00 | 232.00 | 232.20 | 2.9000 | -1.0700 | 1200.00 | Crest | * 808 | 832 | 74 | 75 | |
| 1670+00.00 | 232.40 | 232.50 | -1.0700 | 2.0000 | 800.00 | Sag | 1082 | 832 | 88 | 75 | |
| 1694+00.00 | 232.80 | 233.00 | 2.0000 | -1.4120 | 1000.00 | Crest | * 795 | 837 | 73 | 75 | |
| 1711+00.00 | 233.10 | 233.30 | -1.4120 | 1.7270 | 800.00 | Sag | 1048 | 837 | 86 | 75 | |
| 1722+00.00 | 233.30 | 233.50 | 1.7270 | 1.3000 | 800.00 | Crest | 2927 | 795 | +100 | 75 | |
| 1736+50.00 | 233.60 | 233.80 | 1.3000 | 0.2500 | 1000.00 | Crest | 1528 | 811 | +100 | 75 | |
| 1747+50.00 | 233.80 | 234.00 | 0.2500 | 3.5000 | 800.00 | Sag | 1000 | 811 | 85 | 75 | |
| 1760+00.00 | 234.00 | 234.30 | 3.5000 | -0.1730 | 1600.00 | Crest | 970 | 817 | 83 | 75 | |
| 1775+00.00 | 234.30 | 234.50 | -0.1730 | 1.7500 | 800.00 | Sag | 5602 | 817 | +100 | 75 | |
| 1788+00.00 | 234.60 | 234.70 | 1.7500 | 1.2370 | 600.00 | Crest | 2403 | 796 | +100 | 75 | |
| 1807+00.00 | 234.90 | 235.10 | 1.2370 | -0.4330 | 1000.00 | Crest | 1146 | 821 | 91 | 75 | |
| 1822+00.00 | 235.20 | 235.40 | -0.4330 | 1.3570 | 800.00 | Sag | +9999 | 821 | +100 | 75 | |
| 1838+00.00 | 235.50 | 235.70 | 1.3570 | 2.5580 | 1000.00 | Sag | +9999 | 794 | +100 | 75 | |
| 1855+00.00 | 235.70 | 236.10 | 2.5580 | -2.1580 | 1900.00 | Crest | 932 | 850 | 79 | 75 | |
| 1877+00.00 | 236.30 | 236.40 | -2.1580 | 1.1940 | 800.00 | Sag | 962 | 850 | 81 | 75 | |
| 1894+00.00 | 236.60 | 236.70 | 1.1940 | -1.0000 | 800.00 | Crest | 892 | 831 | 78 | 75 | |

Meaning Of Symbols:

* = Existing Stopping Sight Distance less than AASHTO required value

Note:

Attachment 1 - Vertical Curve Inventory (Contd.)

Project Name: 17, Anthem Way Traffic Interchange to Jct. SR 69 (Cordes Junction) Northbound

Project No: 17 MA 229 H6800 01L

Roadway Type: Divided Roadway (Uni-directional)

| VPI Station (ft) | Mile | post | Grade (%) | | Curve | Curve | Stopping Sigh | t Distance (ft) | Speed (mph) | | |
|------------------|--------|--------|-----------|-----------|-------------|-------|---------------|-----------------|-------------|--------|--|
| VFT Station (It) | Begin | End | Approach | Departure | Length (ft) | Туре | Existing | Required | Existing | Posted | |
| 1907+00.00 | 236.80 | 237.00 | -1.0000 | 1.0420 | 800.00 | Sag | 3482 | 831 | +100 | 75 | |
| 1931+00.00 | 237.20 | 237.50 | 1.0420 | -5.0000 | 1600.00 | Crest | * 756 | 905 | 67 | 75 | |
| 1979+00.00 | 238.20 | 238.30 | -5.0000 | 0.1750 | 800.00 | Sag | * 638 | 905 | 61 | 75 | |
| 2036+00.00 | 239.30 | 239.40 | 0.1750 | -1.6670 | 800.00 | Crest | 986 | 842 | 82 | 75 | |
| 2054+00.00 | 239.60 | 239.80 | -1.6670 | 3.7930 | 1000.00 | Sag | * 740 | 842 | 69 | 75 | |
| 2083+00.00 | 240.00 | 240.40 | 3.7930 | -3.1820 | 2000.00 | Crest | * 787 | 869 | 71 | 75 | |
| 2105+00.00 | 240.60 | 240.70 | -3.1820 | 2.5710 | 1000.00 | Sag | * 707 | 869 | 66 | 75 | |
| 2140+00.00 | 240.90 | 241.70 | 2.5710 | -2.5000 | 4300.00 | Crest | 1353 | 856 | 98 | 75 | |
| 2171+00.00 | 241.80 | 242.00 | -2.5000 | 1.0210 | 800.00 | Sag | 908 | 856 | 78 | 75 | |
| 2190+00.00 | 242.20 | 242.30 | 1.0210 | -1.6500 | 800.00 | Crest | * 804 | 842 | 73 | 75 | |
| 2187+00.00 | 242.40 | 242.50 | -1.6500 | -0.3280 | 800.00 | Sag | +9999 | 842 | +100 | 75 | |
| 2203+00.00 | 242.70 | 242.80 | -0.3280 | -1.9050 | 800.00 | Crest | 1084 | 846 | 87 | 75 | |
| 2224+00.00 | 243.10 | 243.20 | -1.9050 | -0.1500 | 800.00 | Sag | +9999 | 846 | +100 | 75 | |
| 2244+00.00 | 243.50 | 243.60 | -0.1500 | 2.0050 | 800.00 | Sag | 2622 | 817 | +100 | 75 | |
| 2280+00.00 | 244.10 | 244.40 | 2.0050 | 0.2920 | 1600.00 | Crest | 1420 | 640 | +100 | 65 | |
| 2303+72.42 | 244.50 | 244.80 | 0.2920 | 3.5000 | 1600.00 | Sag | 1897 | 640 | +100 | 65 | |
| | | | | | | | | | | | |
| | | | | | | | | | | | |
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| | | | | | | | | | | | |
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| | | | | | | | | | | | |

Meaning Of Symbols:

= Existing Stopping Sight Distance less than AASHTO required value

Note:

Attachment 1 - Vertical Curve Inventory

Project Name: I-17, Anthem Way Traffic Interchange to Jct. SR 69 (Cordes Junction) Southbound

Project No: 17 MA 229 H6800 01L

Roadway Type: Divided Roadway (Uni-directional)

| VPI Station (ft) | Milepost | | Grade (%) | | Curve | Curve | Stopping Sight | Distance (ft) | Speed (mph) | |
|------------------|----------|--------|-----------|-----------|-------------|-------|----------------|---------------|-------------|--------|
| VFT Station (It) | Begin | End | Approach | Departure | Length (ft) | Туре | Existing | Required | Existing | Posted |
| 2303+90.00 | 244.80 | 244.50 | -3.5000 | -0.2920 | 1600.00 | Sag | 1897 | 689 | +100 | 65 |
| 2280+00.00 | 244.40 | 244.10 | -0.2920 | -2.0510 | 1600.00 | Crest | 1401 | 848 | +100 | 75 |
| 2244+00.00 | 243.60 | 243.50 | -2.0510 | 0.1500 | 800.00 | Sag | 2396 | 848 | +100 | 75 |
| 2224+00.00 | 243.20 | 243.10 | 0.1500 | 1.9050 | 800.00 | Sag | +9999 | 812 | +100 | 75 |
| 2203+00.00 | 242.80 | 242.60 | 1.9050 | 0.3280 | 800.00 | Crest | 1084 | 810 | 89 | 75 |
| 2187+00.00 | 242.40 | 242.20 | 0.3280 | 1.6500 | 800.00 | Sag | +9999 | 810 | +100 | 75 |
| 2172+00.00 | 242.10 | 241.80 | 1.6500 | -2.5000 | 1600.00 | Crest | 912 | 856 | 78 | 75 |
| 2153+00.00 | 241.70 | 241.60 | -2.5000 | 1.2270 | 1000.00 | Sag | 1044 | 856 | 84 | 75 |
| 2142+00.00 | 241.60 | 241.50 | 1.2270 | -0.2410 | 800.00 | Crest | 1135 | 818 | 91 | 75 |
| 2137+00.00 | 241.20 | 241.10 | -0.2410 | 1.0590 | 600.00 | Sag | +9999 | 818 | +100 | 75 |
| 2119+50.00 | 241.10 | 240.80 | 1.0590 | -2.7350 | 1600.00 | Crest | 954 | 861 | 80 | 75 |
| 2106+50.00 | 240.80 | 240.60 | -2.7350 | 0.2380 | 800.00 | Sag | 1136 | 861 | 88 | 75 |
| 2083+00.00 | 240.30 | 240.10 | 0.2380 | -2.4880 | 1200.00 | Crest | 975 | 856 | 81 | 75 |
| 2063+00.00 | 239.90 | 239.80 | -2.4880 | -2.8330 | 600.00 | Crest | 3428 | 862 | +100 | 75 |
| 2051+00.00 | 239.70 | 239.60 | -2.8330 | 2.8130 | 700.00 | Sag | * 528 | 862 | 56 | 75 |
| 2035+00.00 | 239.50 | 239.20 | 2.8130 | -1.0770 | 1600.00 | Crest | 942 | 832 | 81 | 75 |
| 2022+00.00 | 239.10 | 239.00 | -1.0770 | 0.8750 | 500.00 | Sag | 3406 | 832 | +100 | 75 |
| 2014+00.00 | 239.00 | 238.80 | 0.8750 | -1.5710 | 1100.00 | Crest | 985 | 840 | 82 | 75 |
| 2000+00.00 | 238.70 | 238.60 | -1.5710 | 5.1670 | 800.00 | Sag | * 509 | 840 | 55 | 75 |
| 1988+00.00 | 238.50 | 238.30 | 5.1670 | 3.0000 | 1000.00 | Crest | 998 | 772 | 88 | 75 |
| 1947+00.00 | 237.80 | 237.50 | 3.0000 | 0.2410 | 1200.00 | Crest | 969 | 811 | 83 | 75 |
| 1918+00.00 | 237.20 | 237.10 | 0.2410 | 1.0000 | 600.00 | Sag | +9999 | 811 | +100 | 75 |

Meaning Of Symbols:

* = Existing Stopping Sight Distance less than AASHTO required value

Note:

Attachment 1 - Vertical Curve Inventory (Contd.)

Project Name: I-17, Anthem Way Traffic Interchange to Jct. SR 69 (Cordes Junction) Southbound

Project No: 17 MA 229 H6800 01L

Roadway Type: Divided Roadway (Uni-directional)

| VPI Station (ft) | Milepost | | Grade (%) | | Curve | Curve | Stopping Sigh | t Distance (ft) | Speed (mph) | |
|-------------------|----------|--------|-----------|-----------|-------------|-------|---------------|-----------------|-------------|--------|
| VI I Station (it) | Begin | End | Approach | Departure | Length (ft) | Туре | Existing | Required | Existing | Posted |
| 1897+86.03 | 236.80 | 236.70 | 1.0000 | 1.9410 | 600.00 | Sag | +9999 | 800 | +100 | 75 |
| 1877+00.00 | 236.40 | 236.30 | 1.9500 | 2.9580 | 800.00 | Sag | +9999 | 786 | +100 | 75 |
| 1853+00.00 | 236.00 | 235.70 | 2.9580 | -3.0000 | 1700.00 | Crest | * 785 | 866 | 71 | 75 |
| 1837+00.00 | 235.70 | 235.50 | -3.0000 | 1.4840 | 800.00 | Sag | * 723 | 866 | 67 | 75 |
| 1806+00.00 | 235.10 | 234.90 | 1.4840 | -2.7100 | 1400.00 | Crest | * 849 | 860 | 74 | 75 |
| 1775+00.00 | 234.50 | 234.30 | -2.7100 | -1.2500 | 800.00 | Sag | +9999 | 860 | +100 | 75 |
| 1763+00.00 | 234.30 | 234.10 | -1.2500 | -2.6670 | 800.00 | Crest | 1161 | 859 | 90 | 75 |
| 1748+00.00 | 234.00 | 233.80 | -2.6670 | 2.0000 | 800.00 | Sag | * 698 | 859 | 66 | 75 |
| 1731+00.00 | 233.70 | 233.50 | 2.0000 | -1.2860 | 1000.00 | Crest | * 810 | 835 | 74 | 75 |
| 1689+00.00 | 232.90 | 232.70 | -1.2860 | -2.9410 | 800.00 | Crest | 1052 | 864 | 84 | 75 |
| 1672+00.00 | 232.60 | 232.40 | -2.9410 | 0.9550 | 800.00 | Sag | * 819 | 864 | 73 | 75 |
| 1650+00.00 | 232.20 | 232.00 | 0.9550 | -3.0000 | 1200.00 | Crest | * 809 | 866 | 72 | 75 |
| 1613+00.00 | 231.50 | 231.20 | -3.0000 | -0.1580 | 1600.00 | Sag | 2265 | 866 | +100 | 75 |
| 1594+00.00 | 231.10 | 230.90 | -0.1580 | 0.6690 | 800.00 | Sag | +9999 | 817 | +100 | 75 |
| 1574+00.00 | 230.70 | 230.60 | 0.6690 | -0.4480 | 800.00 | Crest | 1366 | 822 | +100 | 75 |
| 1557+00.00 | 230.40 | 230.20 | -0.3330 | -1.2730 | 1000.00 | Crest | 1648 | 835 | +100 | 75 |
| 1513+00.00 | 229.50 | 229.40 | -1.6000 | -0.9200 | 400.00 | Sag | +9999 | 841 | +100 | 75 |
| 1497+00.00 | 229.30 | 229.10 | -1.3330 | -1.7590 | 800.00 | Crest | 2933 | 843 | +100 | 75 |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |

Meaning Of Symbols:

= Existing Stopping Sight Distance less than AASHTO required value

Note:

Attachment 2 - Horizontal Curve Inventory

| HPI Station | Mile | post | S | Superelevation | (ft/ft) | Degree | Speed (mph) | | HSO Grade | | Horizontal SSD (f | | |
|-------------|--------|--------|----------|----------------|---------|-------------|-------------|----------|-----------|------|-------------------|----------|----------|
| (ft) | Begin | End | Existing | AASHTO Min | RDG Max | Existing | AASHTO Max | Method 2 | Posted | (ft) | (%) | Existing | Required |
| 1545+43.00 | 229.70 | 230.50 | 0.015 | 0.015 | 0.10 | 0°-15'-04" | 2°-54' | >100 | 75 | NA | | | |
| 1668+11.00 | 231.90 | 232.90 | 0.015 | 0.015 | 0.10 | 0°-15'-00" | 2°-54' | >100 | 75 | NA | | | |
| 1718+45.00 | 233.30 | 233.40 | *0.023 | 0.061 | 0.10 | 1 °-30'-03" | 2°-54' | 78 | 75 | NA | | | |
| 1749+73.00 | 233.80 | 234.00 | *0.054 | 0.079 | 0.10 | 2°-00'-00" | 2°-54' | 77 | 75 | NA | | | |
| 1768+94.00 | 234.20 | 234.40 | *0.023 | 0.061 | 0.10 | 1°-30'-00" | 2°-54' | 78 | 75 | NA | | | |
| 1795+01.00 | 234.70 | 234.90 | *0.015 | 0.031 | 0.10 | 0°-45'-00" | 2°-54' | 91 | 75 | NA | | | |
| 1819+93.00 | 235.20 | 235.30 | *0.023 | 0.061 | 0.10 | 1°-30'-00" | 2°-54' | 78 | 75 | NA | | | |
| 1866+86.00 | 235.80 | 236.40 | * | 0.061 | 0.10 | 1°-30'-00" | 2°-54' | 73 | 75 | NA | | | |
| 1932+50.00 | 237.20 | 237.60 | *0.015 | 0.041 | 0.10 | 1 °-00'-00" | 2°-54' | 85 | 75 | NA | | | |
| 2019+29.00 | 238.50 | 239.50 | *0.015 | 0.031 | 0.10 | 0°-45'-00" | 2°-54' | 91 | 75 | NA | | | |
| 2071+69.00 | 239.60 | 240.40 | *0.015 | 0.041 | 0.10 | 1 °-00'-00" | 2°-54' | 85 | 75 | NA | | | |
| 2191+90.00 | 242.10 | 242.50 | *0.015 | 0.041 | 0.10 | 1 °-00'-00" | 2°-54' | 85 | 75 | NA | | | |
| 2256+93.00 | 243.50 | 244.00 | 0.050 | 0.048 | 0.10 | 1°-28'-45" | 4°-16' | 84 | 65 | NA | | | |
| 2295+95.00 | 244.30 | 244.70 | *0.015 | 0.063 | 0.10 | 2°-02'-19" | 4°-16' | 70 | 65 | NA | | | |
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Project Name: I-17, Anthem Way Traffic Interchange to Jct. SR 69 (Cordes Junction) Northbound **Project No:** 17 MA 229 H6800 01L

Meaning Of Symbols:

Requires a design exception

Note:

AASHTO Minimum superelevation derived from Method 5 to meet posted speed.

Roadway Engineering Design Guidelines (RDG) Maximum is based on elevation (See RDG Table 202.1A).

Input grade with respect to traffic for inside lane of curve; if both - & + grades within the curve, choose the negative grade;

if all negative grades, choose the largest negative grade; if all positive grades, choose the smallest positive grade.

(See Help file under Help Topics/Approach Grade)

HSO = Horizontal Sightline Offset

Attachment 2 - Horizontal Curve Inventory

| HPI Station | Mile | post | S | Superelevation | (ft/ft) | Degree | Of Curve | Speed | (mph) | HSO | Grade | Horizonta | al SSD (ft) |
|-------------|--------|--------|----------|----------------|---------|-------------|------------|----------|--------|------|-------|-----------|-------------|
| (ft) | Begin | End | Existing | AASHTO Min | RDG Max | Existing | AASHTO Max | Method 2 | Posted | (ft) | (%) | Existing | Required |
| 2296+39.00 | 244.70 | 244.30 | *0.015 | 0.061 | 0.10 | 1°-57'-47" | 4°-16' | 71 | 65 | NA | | | |
| 2256+50.00 | 244.00 | 243.50 | *0.050 | 0.061 | 0.10 | 1°-31'-18" | 2°-54' | 83 | 75 | NA | | | |
| 2132+98.00 | 241.80 | 240.90 | *0.015 | 0.021 | 0.10 | 0°-30'-00" | 2°-54' | 99 | 75 | NA | | | |
| 2107+08.00 | 240.80 | 240.60 | *0.054 | 0.079 | 0.10 | 2°-00'-00" | 2°-54' | 77 | 75 | NA | | | |
| 2062+77.00 | 240.00 | 239.70 | *0.023 | 0.061 | 0.10 | 1 °-30'-00" | 2°-54' | 78 | 75 | NA | | | |
| 2025+73.00 | 239.30 | 239.00 | 0.015 | 0.015 | 0.10 | 0°-15'-00" | 2°-54' | >100 | 75 | NA | | | |
| 1972+98.00 | 238.40 | 237.90 | *0.015 | 0.051 | 0.10 | 1°-15'-00" | 2°-54' | 80 | 75 | NA | | | |
| 1950+10.00 | 237.80 | 237.70 | *0.015 | 0.041 | 0.10 | 1°-00'-00" | 2°-54' | 85 | 75 | NA | | | |
| 1925+88.00 | 237.40 | 237.10 | *0.023 | 0.061 | 0.10 | 1°-30'-00" | 2°-54' | 78 | 75 | NA | | | |
| 1908+24.00 | 237.00 | 236.90 | *0.015 | 0.041 | 0.10 | 1 °-00'-00" | 2°-54' | 85 | 75 | NA | | | |
| 1895+33.00 | 236.80 | 236.70 | *0.015 | 0.041 | 0.10 | 1°-00'-00" | 2°-54' | 85 | 75 | NA | | | |
| 1866+45.00 | 236.40 | 235.80 | * | 0.079 | 0.10 | 2°-00'-00" | 2°-54' | 67 | 75 | NA | | | |
| 1799+91.00 | 235.40 | 234.30 | * | 0.021 | 0.10 | 0°-30'-00" | 2°-54' | 94 | 75 | NA | | | |
| 1665+31.00 | 232.60 | 232.20 | 0.015 | 0.015 | 0.10 | 0°-12'-00" | 2°-54' | >100 | 75 | NA | | | |
| 1545+52.00 | 230.50 | 229.70 | 0.015 | 0.015 | 0.10 | 0°-15'-00" | 2°-54' | >100 | 75 | NA | | | |
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Project Name: I-17, Anthem Way Traffic Interchange to Jct. SR 69 (Cordes Junction) Southbound **Project No:** 17 MA 229 H6800 01L

Meaning Of Symbols:

Requires a design exception

Note:

AASHTO Minimum superelevation derived from Method 5 to meet posted speed.

Roadway Engineering Design Guidelines (RDG) Maximum is based on elevation (See RDG Table 202.1A).

Input grade with respect to traffic for inside lane of curve; if both - & + grades within the curve, choose the negative grade;

if all negative grades, choose the largest negative grade; if all positive grades, choose the smallest positive grade.

(See Help file under Help Topics/Approach Grade)

HSO = Horizontal Sightline Offset

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Project Name: I-17 Black Canyon City to Cordes Junction NB Project Number: 18690 Roadway Type: PRINCIPAL ARTERIAL INTERSTATE - RURAL (MP 244.5 -262)

| IdV | | POST | TRAFFIC | GRADE | GRADE | CURVE | CURVE | STOPPING SIC | HT DISTANCE | SPE | ED |
|----------|--------|--------|---------------|---------|---------|--------|-------|--------------|--------------|-----------|--------|
| STATION | BEGIN | END | DIRECTION | Z | OUT | LENGTH | түре | AVAILABLE | AASHTO | AVAILABLE | DESIGN |
| | | | (1w, 1a or 2) | (%) | (%) | (ft) | | (ft) | MINIMUM (ft) | (hdm) | (hdm) |
| 2337+00. | 245.08 | 245.68 | 1w | 3.5000 | 0.8139 | 2400 | Crest | 1389 | 635 | +100 | 65 |
| 2355+00. | 245.68 | 245.98 | 1w | 0.8139 | 6.0000 | 1200 | Sag | 911 | 635 | 81 | 65 |
| 2420+00. | 247.03 | 247.18 | 1w | 6.0000 | 5.0000 | 800 | Crest | 1479 | 593 | +100 | 65 |
| 2445+00. | 247.41 | 247.75 | 1w | 5.0000 | 0.8500 | 1800 | Crest | 967 | 634 | 84 | 65 |
| 2465+00. | 247.88 | 248.03 | 1w | 0.8500 | 3.2000 | 800 | Sag | 1900 | 634 | +100 | 65 |
| 2480+00. | 248.24 | 248.24 | 1w | 3.2000 | 3.0417 | 0 | GB | GB | GB | GB | 65 |
| 2520+00 | 248.92 | 249.08 | 1w | 3.0417 | 6.0000 | 800 | Sag | 1145 | 611 | 95 | 65 |
| 2592+70. | 250.15 | 250.60 | 1w | 6.0000 | 0.4400 | 2400 | Crest | 965 | 808 | 83 | 75 |
| 2618+00 | 250.78 | 250.93 | 1w | 0.4400 | 1.0416 | 800 | Sag | 6666+ | 808 | +100 | 75 |
| 2643+00 | 251.23 | 251.37 | 1w | 1.0416 | 0.5998 | 800 | Crest | 2842 | 806 | +100 | 75 |
| 2686+00 | 251.83 | 252.29 | 1w | 0.5998 | -4.4300 | 2400 | Crest | 1015 | 893 | 81 | 75 |
| 2709+00 | 252.31 | 252.69 | 1w | -4.4300 | 2.5150 | 2000 | Sag | 1112 | 893 | 85 | 75 |
| 2746+00 | 253.11 | 253.26 | 1w | 2.5150 | 4.5000 | 800 | Sag | 4230 | 778 | +100 | 75 |
| 2769+00 | 253.30 | 253.94 | 1w | 4.5000 | -2.0000 | 3400 | Crest | 1062 | 848 | 86 | 75 |
| 2817+00 | 254.56 | 254.75 | 1w | -2.0000 | -0.2500 | 800 | Sag | +9999 | 848 | +100 | 75 |
| 2849+00 | 255.13 | 255.50 | 1w | -0.2500 | -4.8537 | 2000 | Crest | 968 | 902 | 78 | 75 |
| 2890+00 | 255.83 | 256.31 | 1w | -4.8537 | 1.9000 | 2600 | Sag | 1453 | 902 | +100 | 75 |
| 2920+00 | 256.60 | 256.67 | 1w | 1.9000 | 3.8000 | 400 | Sag | 3867 | 787 | +100 | 75 |
| 2930+00 | 256.71 | 256.94 | 1w | 3.8000 | 1.2000 | 1200 | Crest | 998 | 797 | 86 | 75 |
| 2945+00 | 256.99 | 257.22 | 1w | 1.2000 | 4.7500 | 1200 | Sag | 1294 | 797 | 100 | 75 |
| 2973+00 | 257.35 | 257.92 | 1w | 4.7500 | -2.5000 | 3000 | Crest | 945 | 856 | 80 | 75 |
| 2993+00 | 257.92 | 258.11 | 1w | -2.5000 | 4.2500 | 1000 | Sag | 615 * | 856 | 61 | 75 |
| 3017+00 | 258.40 | 258.55 | 1w | 4.2500 | 3.5833 | 800 | Crest | 2018 | 764 | +100 | 75 |
| 3035+00 | 258.72 | 258.91 | 1w | 3.5833 | 5.0158 | 1000 | Sag | +9999 | 764 | +100 | 75 |
| 3061+00 | 259.16 | 259.40 | 1w | 5.0158 | 0.9723 | 1400 | Crest | 864 | 800 | 29 | 75 |
| | | | | | | | | | | | |

Notes:

Traffic Direction: 1w = One Way Traffic in Station direction 1a = One Way Traffic against Station direction 2 = Two Way Traffic

Grades are with respect to Station direction. * Indicates design exception required. GB indicates grade break. Stopping Sight Distance and Speed not calculated. Calculations are based on AASHTO 2001 and ADOT 2004 Roadway Design Guidelines formulas with adjustments for effective grade.

Attachment 1 I-17 NB 1 -2

ATTACHMENT 1 - VERTICAL CURVE INVENTORY

Project Name: 1-17 Black Canyon City to Cordes Junction NB Project Number: 18690 Roadway Type: PRINCIPAL ARTERIAL INTERSTATE - RURAL (MP 244.5 -262)

DESIGN (mph) AVAILABLE (hqm 83 96 91 79 79 80 80 78
 STOPPING SIGHT DISTANCE

 AVAILABLE
 AASHTO

 (ff)
 MINIMUM (ff)

 2092
 800

 952
 800

 952
 800

 11220
 802

 1128
 810

 11622
 810

 946
 864

 954
 864

 910
 1139

 807
 824

 924
 824

 924
 824

 897
 848
 CURVE TYPE Crest Crest Crest Crest Crest Crest CURVE LENGTH 800 2000 2100 2100 800 800 1600 1600 £ GRADE OUT (%) GRADE IN (%) 0.9420
 TRAFFIC

 DIRECTION

 (1w, 1a or 2)

 1w

 1w
 259.45 259.61 259.70 259.90 259.99 260.15 260.20 260.59 260.86 261.01 261.10 261.49 262.02 262.17 262.03 262.17 262.03 262.64 262.68 262.80 262.86 263.16 OST END VPI STATION 3078+00. 3092+00. 3106+00. 3151+00. 3170+50. 3212+50 3233+50 3233+50 3233+50 3261+00. 3261+00.

| Notes: | Traffic Direction: Traffic Direction: 1w = One Way Traffic in Station direction 1a = One Way Traffic against Station direction 2 = Two Way Traffic | Grades are with respect to Station direction. * Indicates design exception required. GB indicates grade break. Stopping Sight Distance and Speed not calculated. GB indicates grade break. Stopping Sight Distance and Speed not calculated. Calculations are based on AASHTO 2001 and ADOT 2004 Roadway Design Calculations are based on AASHTO 2001 and ADOT 2004 Roadway Design Calculations are based on AASHTO 2001 and ADOT 2004 Roadway Design Guidelines formulas with adjustments for effective grade. Attachment 1 1-17 NB 2 -2 |
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Project Name: 1-17 Black Canyon City to Cordes Junction SB Project Number: 18690 Roadway Type: PRINCIPAL ARTERIAL INTERSTATE - RURAL (MP 244.5 -262)

| IdA | MILE | POST | TRAFFIC | GRADE | GRADE | CURVE | CURVE | STOPPING SIC | SHT DISTANCE | SPE | ED |
|----------|-------------|----------|---------------|---------|---------|------------|-------------|---------------------|--------------|-----------|--------|
| STATION | BEGIN | END | DIRECTION | Z | OUT | LENGTH | TYPE | AVAILABLE | AASHTO | AVAILABLE | DESIGN |
| | | | (1w, 1a or 2) | (%) | (%) | (ft) | | (ff) | MINIMUM (ft) | (mph) | (hdm) |
| 2319+00. | 244.95 | 244.95 | 1a | 3.5000 | 3.7000 | 0 | GB | GB | GB | GB | 65 |
| 2320+50. | 244.98 | 244.98 | 1a | 3.7000 | 3.5000 | 0 | GB | GB | GB | GB | 65 |
| 2324+50. | 245.07 | 245.07 | 1a | 3.5000 | 3.4400 | 0 | GB | GB | GB | GB | 65 |
| 2331+00. | 245.13 | 245.35 | 1a | 3.4400 | 0.9040 | 006 | Crest | 875 | 688 | 75 | 65 |
| 2342+50. | 245.41 | 245.63 | 1a | 0.9040 | -1.5100 | 006 | Crest | 897 | 655 | 79 | 65 |
| 2348+50. | 245.67 | 245.67 | 1a | -1.5100 | -1.7053 | 0 | GB | GB | GB | GB | 65 |
| 2356+50. | 245.72 | 246.02 | 1a | -1.7053 | 6.0000 | 1200 | Sag | 642 * | 728 | 60 | 65 |
| 2385+00. | 246.37 | 246.52 | 1a | 6.0000 | 5.4642 | 800 | Crest | 2414 | 728 | +100 | 65 |
| 2409+00. | 246.82 | 246.97 | 1a | 5.4642 | 6.0000 | 800 | Sag | 6666+ | 728 | +100 | 65 |
| 2419+50 | 247.10 | 247.10 | 1a | 6.0000 | 6.0433 | 0 | GB | GB | GB | GB | 65 |
| 2428+50. | 247.19 | 247.34 | 1a | 6.0433 | 5.3600 | 800 | Crest | 1979 | 729 | +100 | 65 |
| 2436+50. | 247.34 | 247.49 | 1a | 5.3600 | 6.0000 | 800 | Sag | 6666+ | 728 | +100 | 65 |
| 2450+50. | 247.55 | 247.82 | 1a | 6.0000 | -0.3000 | 1400 | Crest | 692 * | 728 | 63 | 65 |
| 2458+50. | 247.83 | 247.83 | 1a | -0.3000 | -0.5000 | 0 | GB | GB | GB | GB | 65 |
| 2469+50. | 247.97 | 248.12 | 1a | -0.5000 | 2.4100 | 800 | Sag | 1176 | 674 | 90 | 65 |
| 2481+00. | 248.12 | 248.40 | 1a | 2.4100 | -0.7563 | 1500 | Crest | 1011 | 674 | 83 | 65 |
| 2494+50 | 248.44 | 248.59 | 1a | -0.7563 | -1.2100 | 800 | Crest | 2778 | 635 | +100 | 65 |
| 2504+25. | 248.60 | 248.80 | 1a | -1.2100 | 6.0000 | 1050 | Sag | e06 * | 728 | 58 | 65 |
| 2517+00. | 248.87 | 249.02 | 1a | 6.0000 | 5.0024 | 800 | Crest | 1482 | 728 | +100 | 65 |
| 2534+00. | 249.15 | 249.38 | 1a | 5.0024 | 2.3300 | 1200 | Crest | 984 | 712 | 79 | 65 |
| 2546+00. | 249.40 | 249.58 | 1a | 2.3300 | 5.9000 | 1000 | Sag | 1091 | 726 | 83 | 65 |
| 2553+50. | 249.63 | 249.63 | 1a | 5.9000 | 6.1000 | 0 | GB | GB | GB | GB | 65 |
| 2561+00. | 249.77 | 249.77 | 1a | 6.1000 | 6.3000 | 0 | GB | GB | GB | GB | 65 |
| 2566+50. | 249.80 | 249.96 | 1a | 6.3000 | 5.6600 | 800 | Crest | 2086 | 733 | +100 | 65 |
| 2571+00. | 249.97 | 249.97 | 1a | 5.6600 | 5.8300 | 0 | GB | GB | GB | GB | 65 |
| Notes: | Traffic Dir | rection: | | | | Grades are | with respec | ot to Station direc | tion. | | |

Traffic Direction: 1w = One Way Traffic in Station direction 1a = One Way Traffic against Station direction 2 = Two Way Traffic

Grades are with respect to Station direction. * Indicates design exception required. GB indicates grade break. Stopping Sight Distance and Speed not calculated. Calculations are based on AASHTO 2001 and ADOT 2004 Roadway Design Guidelines formulas with adjustments for effective grade.

Attachment 1 I-17 SB 1 - 3

CURVE INVENTORY ATTACHMENT 1 - VERTICAL

Project Name: 1-17 Black Canyon City to Cordes Junction SB Project Number: 18690 Roadway Type: PRINCIPAL ARTERIAL INTERSTATE - RURAL (MP 244.5 -262)

SPEED AVAILABLE DESIGN (mph) STOPPING SIGHT DISTANCE AVAILABLE AASHTO (ft) MINIMUM (ft) €E CURVE ТҮРЕ Crest Sag Crest Sag BB BBB CURVE LENGTH £ -1.3110 0.0000 GRADE OUT .4546 .5329 1143 0632 0440 .3110 GRADE 5000 5000 5000 5000 NI (%) TRAFFIC DIRECTION (1w, 1a or 2)
 250.04
 250.04
 250.04

 250.21
 250.21
 250.21

 250.22
 250.37
 250.63

 250.63
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 OST END MILEF VPI STATION

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| 2/90+00. | 253.91 | CI.4CZ | σ | 0.000 | 1004.7- | 201 | CIGN | 201 | 010 | t | 2 |
|----------|--------|--------|----|---------|---------|------|-------|-------|-----|------|----|
| 2800+25. | 254.26 | 254.26 | 1a | -2.4361 | -2.4500 | 0 | GB | GB | GB | GB | 75 |
| 2810+00. | 254.42 | 254.56 | 1a | -2.4500 | -2.0000 | 600 | Sag | +9999 | 785 | +100 | 75 |
| 2819+00. | 254.63 | 254.77 | 1a | -2.0000 | -0.1820 | 600 | Sag | 10962 | 812 | +100 | 75 |
| 2830+00. | 254.89 | 255.02 | 1a | -0.1820 | 1.0000 | 600 | Sag | 6666+ | 831 | +100 | 75 |
| 2847+00. | 255.10 | 255.46 | 1a | 1.0000 | -3.5000 | 2000 | Crest | 626 | 831 | 83 | 75 |
| 2862+00. | 255.50 | 255.61 | 1a | -3.5000 | -1.5000 | 600 | Sag | 3200 | 792 | +100 | 75 |
| 2873+00. | 255.65 | 255.85 | 1a | -1.5000 | -4.0000 | 1100 | Crest | 974 | 792 | 85 | 75 |
| 2888+00. | 255.99 | 256.07 | 1a | -4.0000 | -2.3950 | 400 | Sag | 6666+ | 780 | +100 | 75 |
| 2907+00. | 256.31 | 256.47 | 1a | -2.3950 | 1.5000 | 800 | Sag | 820 * | 839 | 74 | 75 |
| | | | | | | | | | | | |

Notes:

| Traffic Direction: | 1w = One Way Traffic in Station direction | 1a = One Way Traffic against Station direction | |
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|--------------------|---|--|--|

Grades are with respect to Station direction. * Indicates design exception required. GB indicates grade break. Stopping Sight Distance and Speed not calculated. Calculations are based on AASHTO 2001 and ADOT 2004 Roadway Design Guidelines formulas with adjustments for effective grade.

Attachment 1 I-17 SB 2 - 3

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Project Name: 1-17 Black Canyon City to Cordes Junction SB Project Number: 18690 Roadway Type: PRINCIPAL ARTERIAL INTERSTATE - RURAL (MP 244.5 -262)

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|--------------|-----------|---------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|--|--|--|--|
| ED | DESIGN | (hqm) | 75 | 75 | 75 | 75 | 75 | 75 | 75 | 75 | 75 | 75 | 75 | 75 | 75 | 75 | 75 | 75 | 75 | 75 | | | | |
| SPE | AVAILABLE | (hdm) | +100 | +100 | +100 | 78 | +100 | +100 | +100 | +100 | 91 | 80 | 92 | 80 | +100 | 81 | 63 | 87 | 78 | 77 | | | | |
| SHT DISTANCE | AASHTO | MINIMUM (ft) | 839 | 875 | 606 | 606 | 855 | 866 | 875 | 905 | 905 | 882 | 885 | 885 | 846 | 846 | 852 | 852 | 853 | 853 | | | | |
| STOPPING SIC | AVAILABLE | (ft) | 2219 | 1824 | +9999 | 968 | 2698 | +9999 | +9999 | 6666+ | 1259 | 984 | 1257 | 978 | 1709 | 996 | 639 * | 1099 | 903 | 894 | | | | |
| CURVE | түре | | Crest | Sag | Sag | Crest | Crest | Sag | Sag | Sag | Crest | Crest | Sag | Crest | Sag | Crest | Sag | Crest | Sag | Crest | | | | |
| CURVE | LENGTH | (ft) | 600 | 1000 | 400 | 1200 | 400 | 600 | 400 | 600 | 600 | 1200 | 800 | 2000 | 800 | 2100 | 800 | 1600 | 600 | 1600 | | | | |
| GRADE | OUT | (%) | 0.9378 | 3.5000 | 5.1980 | 2.4320 | 2.0000 | 3.0000 | 3.5000 | 5.0000 | 3.8750 | 1.2000 | 4.0000 | -0.5163 | 1.9214 | -2.9400 | 2.2300 | -0.6300 | 2.3230 | -2.0000 | | | | |
| GRADE | Z | (%) | 1.5000 | 0.9378 | 3.5000 | 5.1980 | 2.4320 | 2.0000 | 3.0000 | 3.5000 | 5.0000 | 3.8750 | 1.2000 | 4.0000 | -0.5163 | 1.9214 | -2.9400 | 2.2300 | -0.6300 | 2.3230 | | | | |
| TRAFFIC | DIRECTION | (1w, 1a or 2) | 1a | 1a 1 | 1a | | | | |
| POST | END | | 256.83 | 257.00 | 257.19 | 257.49 | 257.81 | 258.51 | 258.76 | 258.91 | 259.17 | 259.43 | 260.01 | 260.68 | 261.03 | 261.52 | 262.17 | 262.64 | 262.80 | 263.14 | | | | |
| MILEI | BEGIN | | 256.74 | 256.84 | 257.11 | 257.26 | 257.71 | 258.40 | 258.68 | 258.79 | 259.07 | 259.23 | 259.87 | 260.30 | 260.88 | 261.12 | 262.02 | 262.34 | 262.68 | 262.84 | | | | |
| IdV | STATION | | 2925+00. | 2934+00. | 2947+00. | 2959+00. | 2982+00. | 3016+00. | 3030+00. | 3037+00. | 3052+00. | 3064+00. | 3099+00. | 3128+00. | 3152+00. | 3171+50. | 3212+50. | 3233+50. | 3246+50. | 3260+00. | | | | |

Traffic Direction: 1w = One Way Traffic in Station direction 1a = One Way Traffic against Station direction 2 = Two Way Traffic

Notes:

Grades are with respect to Station direction. * Indicates design exception required. GB indicates grade break. Stopping Sight Distance and Speed not calculated. Calculations are based on AASHTO 2001 and ADOT 2004 Roadway Design Guidelines formulas with adjustments for effective grade.

Attachment 1 I-17 SB 3 - 3

ATTACHMENT 2 - HORIZONTAL CURVE INVENTORY

Project Name: 1-17 BBC to Jct. SR 69 NB-(Posted Speed) Project No: 17 MA 232 H6800 01L

| 1 | 1 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | |
|---------------------|-------------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|--|
| (mph) | DESIGN | 65 | 65 | 65 | 65 | 65 | 65 | 65 | 65 | 65 | 65 | 65 | 65 | 65 | |
| SPEED | EXISTING | 59 | 54 | 54 | 67 | 59 | 59 | 54 | 54 | 63 | 67 | 54 | 54 | 59 | |
| F CURVE | AASHTO MAX | 4°-15' | 4°-15' | 4°-15' | 4°-15' | 4°-15' | 4°-15' | 4°-15' | 4°-15' | 4°-15' | 4°-15' | 4°-15' | 4°-15' | 4°-15' | |
| DEGREE O | EXISTING | 0°-59.43' | 4°-00.00' | 4°-00.00' | 2°-00.00' | 3°-00.00' | 3°-00.00' | 4°-00.00' | 4°-00.00' | 2°-30.00' | 2°-00.00' | 4°-00.00' | 4°-00.00' | 3°-00.00' | |
| ft/ft) | AASHTO MAX | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | |
| RELEVATION (| EXISTING | *0.015 | *0.108 | *0.108 | *0.015 | *0.050 | *0.050 | *0.108 | *0.108 | *0.015 | *0.015 | *0.108 | *0.108 | *0.050 | |
| SUPE | AASHTO MIN | 0.033 | 0.099 | 660.0 | 0.062 | 0.087 | 0.087 | 0.099 | 0.099 | 0.075 | 0.062 | 660.0 | 0.099 | 0.087 | |
| OST | END | 245.13 | 245.45 | 245.90 | 246.41 | 246.64 | 246.92 | 247.46 | 247.95 | 248.22 | 248.61 | 249.22 | 249.62 | 249.97 | |
| MILEP | BEGIN | 244.81 | 245.37 | 245.68 | 246.33 | 246.54 | 246.78 | 247.31 | 247.63 | 248.11 | 248.45 | 249.02 | 249.40 | 249.78 | |
| | | 2319+39.17 | 2338+22.43 | 2353+75.36 | 2381+12.87 | 2392+89.59 | 2406+69.16 | 2435+26.25 | 2458+62.84 | 2475+92.69 | 2495+27.97 | 2527+18.75 | 2547+80.82 | 2566+47.66 | |

| 65 | 75 | 75 | 75 | 75 | 75 | 75 | 75 | 75 | |
|------------|------------|------------|------------|------------|------------|------------|------------|------------|---------------------|
| | | | | | | | | | |
| 97 | 72 | 75 | 68 | 76 | 67 | 73 | 75 | 83 | |
| 4°-15' | 3°-00' | 3°-00' | 3°-00' | 3°-00' | 3°-00' | 3°-00' | 3°-00' | 3°-00' | |
| 0°-30.00' | 0°-40.00' | 1°-15.00' | 0°-45.00' | 0°-36.00' | 2°-00.00' | 1°-30.00' | 1°-15.00' | 0°-29.77' | |
| 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | |
| 0.015 | *0.015 | *0.015 | *0.015 | *0.015 | *0.015 | *0.015 | *0.015 | *0.015 | |
| SC | 0.028 | 0.051 | 0.031 | 0.025 | 0.079 | 0.061 | 0.051 | 0.021 | |
| 250.42 | 253.07 | 255.00 | 257.35 | 258.92 | 259.85 | 260.24 | 261.14 | 261.49 | |
| 250.13 | 252.20 | 254.19 | 257.07 | 257.66 | 259.65 | 260.04 | 260.46 | 261.29 | |
| 2587+27.93 | 2716+58.29 | 2815+36.00 | 2950+26.60 | 3008+88.70 | 3089+63.95 | 3109+85.92 | 3145+20.60 | 3175+58.89 | Meaning Of Symbols. |

Meaning Of symbous: RC = Remove Adverse Crown * = Existing Superelevation o

ge nded 1 AASHTO 2-1

| /ENTORY | |
|-----------------|--|
| CURVE IN | |
| RIZONTAL | |
| AENT 2 - HC | |
| ATTACHN | |

Project Name: 1-17 BCC to Jct SR 69 - SB (Posted Speed)

| Project No: 1 | 17 MA 232 H68 | 00 01L | | | | | | | |
|---------------------|---------------|--------|-------------------|------------|-------------------|-----------|-------------------|----------|--------|
| | MILEPO | DST | SUPE | RELEVATION | (ft/ft) | DEGREE (| DF CURVE | SPEED | (mph) |
| HPI STALION (III) | BEGIN | END | AASHTO MIN | EXISTING | AASHTO MAX | EXISTING | AASHTO MAX | EXISTING | DESIGN |
| 2319+24.87 | 244.81 | 245.13 | 0.034 | *0.015 | 0.100 | 1°-00.57' | 4°-15' | 58 | 65 |
| 2355+89.81 | 245.78 | 245.93 | 0.062 | *0.015 | 0.100 | 2°-00.00' | 4°-15' | 67 | 65 |
| 2372+07.37 | 246.13 | 246.26 | 0.087 | *0.030 | 0.100 | 3°-00.00' | 4°-15' | 59 | 65 |
| 2387+35.07 | 246.40 | 246.56 | 0.099 | *0.071 | 0.100 | 4°-00.00' | 4°-15' | 54 | 65 |
| 2402+30.11 | 246.72 | 246.81 | 0.099 | *0.071 | 0.100 | 4°-00.00' | 4°-15' | 54 | 65 |
| 2419+15.02 | 247.08 | 247.10 | 0.087 | *0.071 | 0.100 | 3°-00.00' | 4°-15' | 59 | 65 |
| 2433+59.30 | 247.24 | 247.45 | 660.0 | *0.071 | 0.100 | 4°-00.00' | 4°-15' | 54 | 65 |
| 2456+90.52 | 247.60 | 247.92 | 660.0 | *0.071 | 0.100 | 4°-00.00' | 4°-15' | 54 | 65 |
| 2481+92.63 | 248.07 | 248.47 | 0.055 | *0.015 | 0.100 | 1°-45.00' | 4°-15' | 69 | 65 |
| 2511+95.31 | 248.75 | 248.94 | 0.033 | *0.015 | 0.100 | 1°-00.00' | 4°-15' | 59 | 65 |
| 2535+42.38 | 249.23 | 249.35 | 0.087 | *0.030 | 0.100 | 3°-00.00' | 4°-15' | 59 | 65 |
| 2553+91.45 | 249.58 | 249.69 | 0.099 | *0.071 | 0.100 | 4°-00.00' | 4°-15 | 54 | 65 |
| 2566+15.73 | 249.85 | 249.89 | 0.099 | *0.071 | 0.100 | 4°-00.00' | 4°-15' | 54 | 65 |
| 2576+19.53 | 250.04 | 250.08 | 0.099 | *0.071 | 0.100 | 4°-00.00' | 4°-15' | 54 | 65 |
| 2588+82.22 | 250.23 | 250.36 | 660.0 | *0.071 | 0.100 | 4°-00.00' | 4°-15' | 54 | 65 |
| 2600+95.07 | 250.50 | 250.57 | 0.087 | *0.071 | 0.100 | 3°-00.00' | 4°-15' | 59 | 65 |
| 2615+98.47 | 250.72 | 250.91 | 0.087 | *0.030 | 0.100 | 3°-00.57' | 4°-15' | 59 | 65 |
| 2638+49.77 | 251.05 | 251.38 | 0.079 | *0.015 | 0.100 | 2°-00.00' | 3°-00' | 67 | 15 |
| 2717+12.62 | 252.21 | 253.08 | 0.028 | *0.015 | 0.100 | 0°-40.00' | 3°-00' | 72 | 15 |
| 2821+99.17 | 254.35 | 255.06 | 0.079 | *0.024 | 0.100 | 2°-00.00' | 3°-00' | 67 | 75 |
| 2852+34.34 | 255.29 | 255.46 | 0.042 | *0.015 | 0.100 | 1°-00.00' | 3°-00' | 59 | 75 |
| 2880+90.52 | 255.74 | 256.04 | 0.079 | *0.024 | 0.100 | 2°-00.00' | 3°-00' | 67 | 75 |
| Meaning Of Symbols. | | | | | | | | | |

Q, 0 ng Of Symbols = Existing Sup 2-1

- HORIZONTAL CURVE INVENTORY (CONTD.) 2 ATTACHMENT

0 (mph) DESIGN 75 75 75 75 75 75 75 75 75

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) MAX 3°-00' 3°-00' 3°-00' 3°-00' 3°-00' 3°-00' 3°-00' 3°-00'

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Speed) ç PC DC SB 69 SR Jct q BCC 7 <u> -</u> Z t ā

| | ft/ft) | AASHTO MAX | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | 0.100 | |
|---------------|--------------|-------------------|------------|------------|------------|------------|------------|------------|------------|------------|--|
| (5 | RELEVATION (| EXISTING | *0.015 | *0.015 | *0.015 | *0.015 | *0.015 | *0.015 | *0.015 | *0.015 | |
| li naich abec | SUPE | AASHTO MIN | 0.042 | 0.051 | 0.079 | 0.079 | 0.031 | 0.031 | 0.042 | 0.021 | |
| 300 01L | OST | END | 256.65 | 257.34 | 257.71 | 258.72 | 259.44 | 259.94 | 261.15 | 261.61 | |
| 7 MA 232 H6 | MILEP | BEGIN | 256.24 | 257.04 | 257.63 | 258.28 | 259.22 | 259.60 | 260.46 | 261.30 | |
| Project No. | | HPI STATION (#) | 2910+05.73 | 2949+38.92 | 2983+77.10 | 3019+60.96 | 3060+02.13 | 3089+29.37 | 3144+97.56 | 3178+47.71 | |

| ct No: 17 ATION (ft) | MA 232 H6 MILEF | 800 01L oost FND | |
|-------------------------|--------------------|------------------------|--|
| 10+05.73 | 256.24 | 256.65 | |
| 149+38.92 | 257.04 | 257.34 | |
| 983+77.10 | 257.63 | 257.71 | |
| 19+60.96 | 258.28 | 258.72 | |
| 060+02.13 | 259.22 | 259.44 | |
| 189+29.37 | 259.60 | 259.94 | |
| 44+97.56 | 260.46 | 261.15 | |
| 178+47.71 | 261.30 | 261.61 | |
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ing Of Symbols: = Existing Super Mean *

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ROADWAY ENGINEERING GROUP ROADWAY PREDESIGN SECTION

PAGE 1 OF 1

| | | DATE: | 3/7/2018 | | | | |
|-------|------------------------------------|-------|-----------------------|------------------|------------------|---------------------|--|
| TO: | Amin Aman BRIDGE GROUP | | FEDERAL REFERENCE NO: | | | TRACS NO: H6800 | |
| | BRIDGE MANAGEMENT SECTION, MD 635E | | HIGHWAY: | H6800 01L: I-17, | Anthem Way TI to | Jct. SR 69 | |
| | | | LOCATION: | H6800 01L: | -17, Anthem W | ay TI to Jct. SR 69 | |
| | | | MP LIMITS: | 229.00 | TO: | 260.00 | |
| FROM: | Navaphan Viboolmate | | PROJECT DESCRIPTION: | | | | |
| | Bridge Group | | | | | | |

SUBJEC BRIDGE EVALUATION REQUEST

Please evaluate the following structures per AASHTO guidelines:

| ROUTE | MILEPOST | STR. NO. | BRIDGE | BRIDGE | | BRIDGI | E RAIL / B | ARRIER | | A | AC OVERLA | Y | VERT | TICAL | BRIDGE | BRIDGE |
|-------|----------|---------------------|----------------------------|------------------------------------|------------------------------|-----------------------------|---------------------------|------------------------------|------------------------------|---------------------------------------|------------------------|--------------------|-------------|---------------|----------------|-------------------|
| NO. | | AND | LENGTH | ROADWAY | ТҮРЕ | GEOM. | STRUC | Railings | Transitions | THICKNESS | REMOVE | REPLACE / | CLEAI | RANCE | LOAD | SUFFICIENCY |
| | | NAME | | WIDTH | | ОК | ОК | ОК | ОК | (EXISTING) | _ | NEW | (MINI | MUM) | RATING | RATING |
| N7* | N11 | N8 & A209 | N49 | N51 | A206A | A206B | A206C | N36A | N36B | A201 | (MINIMUM) | (MAXIMUM) | NB/EB | SB/WB | N66 | SRB |
| | | 02537 | 220 | 143 | Concrete | Yes | Yes | Yes | N/A | 0" | NA | NA | 17.42 | 17.37 | HS 20+ | 98.50 |
| l 17 | 229 | Anthem Way TI UP | Comments: impact in the | Approximately e shoulders. | 5-feet of co | mpression j | joint seal at | the east jo | int, westbour | nd outside lane | has moderate | adhesion failure | e.The comp | ression joint | seals exhibit | minor debris |
| | | 05740 | | | | | | | | | | | | | | |
| l 17 | 231.2 | RCB | Comments | : Culvert not a | t Grade | | | | | | | | | | | |
| | | 01290 | 347 | 42 | Concrete | Yes | Yes | Yes | No | 4" | 4" | 1" | NA | NA | HS 20 | 96.50 |
| 1 1 7 | 221.4 | New River | Commonto | | Barrier | | | | lanth have a | anarata daali ta | n ha inanastas | | | | naturation das | k analant Than |
| / | 231.4 | Bridge NB | be overlaid | with 1" thick a | opropriate as | sphaltic ove | erlay | noved full c | ieptn, bare c | | p be inspected | i, repaired if nee | eded and se | aled with pe | netrating dec | k sealant . I nen |
| | | | The soffit h The bridge | as light staining has been wide | g following s ned along b | ame patteri oth sides ar | n as bottom nd the new | n mat of reir slab is abo | nforcement. ut 2" thicker | In span 6 the ha than the old slal | airline cracks a b. | along the marks | are more vi | sible than in | other spans. | |
| | | 01291 | 347 | 42 | Concrete Barrier | Yes | Yes | Yes | No | 4" | 4" | 1" | NA | NA | HS 20 | 96.50 |
| l 17 | 231.4 | Bridge SB | Comments: | Existing AC ov | erlay on brid | lge deck sh | ould be rer | moved full c | lepth, bare c | oncrete deck to | p be inspected | l, repaired if nee | eded and se | aled with pe | netrating dec | k sealant .Then |
| | | | The soffit h | as light staining has been wide | g following s ned along b | ame patteri oth sides ar | n as bottom nd the new | n mat of reir slab is abo | nforcement. ut 2" thicker | In span 6 the ha than the old slal | airline cracks a b. | along the marks | are more vi | sible than in | other spans. | |
| | | 01292 | 159 | 38 | Concrete | Yes | Yes | Yes | Yes | 1" | NA | NA | 19.86 | 20.76 | HS 20+ | 94.00 |
| l 17 | 232.02 | New River | | | Damei | | | | | | | | | | | |
| | | II OF ND | | | | | | | | | | | | | | |
| | | 01293 | 145 | 38 | Concrete | Yes | Yes | Yes | Yes | 1" | NA | NA | 15.93 | 16.69 | HS 20+ | 94.00 |
| 1 17 | 232.02 | New River | | | Barrier | | | | | | | | | | | |
| | 202.02 | TI OP SB | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |

| | | 05742 | | | | | | | | | | | | | | |
|-------|--------|---------------------------|--------------|------------------|---------------------|--------------|---------------|---------------|--------------|--------------------|-----------------|----------------|---------------|--------------|----------------|-----------------|
| 1 1 7 | 000 45 | | 0 | Outoutouto | t Ora da | | | | | | | | | | | |
| 1 17 | 232.45 | KCD ND | Comments | Culvert not a | t Grade | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | | 05743 | | | | | | | | | | | | | | |
| 1 1 7 | 222 52 | | Commonto | | t Crada | | | | | | | | | | | |
| 1 17 | 232.32 | ICD 3D | Comments | Cuiven not a | l Grade | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | | 05744 | | | | | | | | | | | | | | |
| 1 1 7 | 233.85 | RCB NB | Commonte | Culvert not a | t Grada | | | | | | | | | | | |
| / | 233.03 | NOB NB | Comments | . Cuiven not a | l Glade | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | | 05745 | | | | | | | | | | | | | | |
| 1 17 | 233.85 | RCB SB | Comments | Culvert not a | t Grade | | | | | | | | | | | |
| , | 200.00 | | Commenta | | | | | | | | | | | | | |
| | | | | | | | | | | | | | - | | | |
| | | 01294 | 151 | 28 | Concrete | Yes | Yes | Yes | Yes | 1" | NA | NA | 16.10 | 16.10 | HS 20+ | F 95.9 |
| 1 17 | 235 94 | Table Mesa | | | Damei | | | | | | | | | | | |
| | 200.01 | TI UP SB | Comments | Repair emban | kment errosi | ion on the v | vest side | | | | | | | | | |
| | | | | | | - | | • | | | • | • | | - | | |
| | | 01295 | 161 | 28 | Concrete Barrier | Yes | Yes | Yes | Yes | 1" | NA | NA | 16.63 | 16.63 | HS 20+ | F 95.7 |
| 1 17 | 235.94 | Table Mesa | | | Damer | | | | | | | | | | | |
| | 200101 | IT UP NB | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | | 00967 | 195 | 38 | Concrete Barrier | Yes | Yes | Yes | Yes | 1" | NA | NA | NA | NA | HS 20+ | 94.60 |
| l 17 | 238.2 | Moores | 0 (| F 1 14 | | | | | | | | | | | | |
| | | | Comments | Erosion at the | northeast ba | ank protecti | on | | | | | | | | | |
| | | 00000 | 470 | 01.0 | | Maa | Maa | Maa | Maa | 0" | | | | | | E 05 0 |
| | | 00339 | 178 | 31.8 | Concrete Barrier | Yes | Yes | Yes | Yes | 0 | NA | NA | NA | NA | HS 16.1 | F 65.2 |
| l 17 | 238.6 | Moores Gulch Br SB | Commonte | Bridge replac | emont is pr | ogramod in | 2022 | | | | | | | | | |
| | | | Comments | . Bridge replac | ement is pr | ogramed in | 2022 | | | | | | | | | |
| | | 05746 | | | | | | - | | | | | 1 | | | |
| | | 03740 | | | | | | | | | | | | | | |
| l 17 | 238.65 | RCB NB | Comments | Culvert not a | t Grade | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | | 00968 | 315 | 32.5 | Concrete | Yes | Yes | Yes | Yes | 1" | NΔ | NΔ | ΝΔ | NΔ | HS 20+ | 88 50 |
| | | 00300 | 515 | 02.0 | Barrier | 163 | 163 | 163 | 163 | • | | 110 | | | 115 204 | 00.00 |
| l 17 | 239.2 | Lit Squaw Crk Br NB | | | | | • | | | | | | • | | | |
| | | | | | | | | | | | | | | | | |
| | | 02965 | 200 | 62 | Concrete | Vee | Yoe | Voc | Vae | ٥" | NΔ | NΔ | NA | NA | HS 20+ | 00 80 |
| | | 02303 | 203 | 02 | Barrier | 103 | 103 | 103 | 103 | Ŭ | | 144 | 114 | | 115 20+ | 30.00 |
| l 17 | 239.55 | Little Squaw Crk Br SB | Comments | A large eroded | d area exists | at the base | e of rail ban | nk at the nor | thwest corne | er next to slope | protection toe. | Rocks have be | en washed o | out from bel | nind the wires | creating large |
| | | | cavity where | water still flov | ving behind t | he rail banl | k . | | | | | | | | a i i | |
| | | | Channel ha | is a small strea | am running u | nder N. spa | an at the tin | ne of inspec | mon. Most c | of fill under Spar | 1 ∠ has washed | a out exposing | the old concr | ete floor on | the downstrea | am end with 18" |

| | | 05747 | | | | | | | | | | | | | | |
|------|--------|------------------------|-----------|----------------------------|----------------------------------|----------------------------|-------------------------------|---------------------------------|------------------------------|-----------------------------|------------------|-------------------|---------|-------|---------|-------|
| l 17 | 241.78 | RCB SB & West Fr Rd | Comments | Culvert not a | t Grade | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | | 05748 | | | | | | | | | | | | | | |
| 1 17 | 241 95 | RCB NB & | Commente | Culvert not a | t Grade | | | | | | | | | | | |
| , | 241.00 | Ramp | Comments. | Cuiven nor a | l Olade | | | | | | | | | | | |
| | | 00969 | 109 | 40 | Concrete Barrier | Yes | Yes | Yes | Yes | 1" | NA | NA | 15.92 | 15.92 | HS 20+ | 96.50 |
| 17 | 242.15 | TI UP NB | Comments: | The W joint s | eal has faller | through.R | epair fatigu | e cracks | | | | | - | - | | |
| | | 00970 | 109 | 40 | Concrete Barrier | Yes | Yes | Yes | Yes | 1" | NA | NA | 16.00 | 16.00 | HS 20+ | 96.40 |
| l 17 | 242.15 | TI UP SB | Comments: | | | | | | | | | | | | | |
| | | 00863 | 224 | 28 | Concrete Barrier | Yes | Yes | Yes | Yes | 1" | NA | NA | 16.50 | 18.12 | HS 20+ | 91.30 |
| 17 | 242.98 | Mud Springs UP | Comments: | | | | | | | | | | | | | |
| | | 01807 | 363 | 42 | Concrete Barrier | Yes | Yes | Yes | Yes | 1" | NA | NA | NA | NA | HS 20+ | 96.80 |
| 17 | 243.34 | Agua Fria Rvr Br NB | Comments: | | | | | | | | | | | | | |
| | | 01808 | 363 | 42 | Concrete Barrier | Yes | Yes | Yes | Yes | 1" | NA | NA | NA | NA | HS 20+ | 96.80 |
| 17 | 243.34 | Agua Fria Rvr Br SB | Comments: | | | - | | | _ | | | _ | - | - | | |
| | | 00764 Coldwater | 97 | 38.3 | Concrete Barrier | Yes | Yes | Yes | Yes | 1" | NA | NA | 14.25 | 14.25 | HS 20+ | 96.00 |
| 17 | 244.37 | Cyn TI OP NB | Comments: | | | | | | | | | | | | | |
| | | 00765 Coldwater | 97 | 38.3 | Concrete Barrier | Yes | Yes | Yes | Yes | 1" | NA | NA | 14.68 | 14.68 | HS 20+ | 96.00 |
| 17 | 244.37 | Cyn TI OP SB | Comments: | | | | | | | | | | | | | |
| | | 01170 | 210 | 28 | H-2-1 on curb | Yes | Yes | Yes | Yes | 0" | NA | NA | 16.29 | 16.29 | HS 20+ | 99.00 |
| 17 | 248.4 | Bumble Bee TI UP SB | Comments: | Replace com Substandard | np seal in jt a barrier repla | t P2; Resto cement is p | re 1/2" Bit j preffered bu | t filler at ab ut not requir | uts.Repair ci ed as Non N | acks observed IHS bridge | in the girders a | at different loca | itions. | - | | |
| | | 01171 | 161 | 38 | Concrete | No | Yes | Yes | Yes | 0" | NA | NA | 15.22 | 16.14 | HS 18.3 | 93.40 |
| 17 | 248.4 | Bumble Bee TI OP NB | Comments: | Bridge rehabi | litation is pro | grammed i | n 2020. | | | | | | • | | | |

| | | 01237 | 107 | 38 | H-2-1 on curb | Yes | No | No | No | 2" | 2" | 1" | 16.51 | 16.51 | HS 20+ | 94.00 |
|------|--------|------------------------|--------------------------------------|---|---|---|-----------------------------|--------------|----------------|-----------------|----------------|-------------------|-------------|--------------|----------------|---------------|
| l 17 | 252.5 | OP NB | Comments be overlaid Substanda | Existing AC ov with 1" thick a rd barrier repla | verlay on bric opropriate as cement is re | lge deck sh sphaltic ove commende | iould be rer erlay. d | moved full c | lepth, bare co | oncrete deck to | p be inspected | d, repaired if ne | eded and se | aled with pe | netrating decl | sealant .Then |
| | | 01352 | 107 | 38 | H-2-1 on curb | Yes | No | No | No | 1" | 1" | 1" | 17.43 | 17.43 | HS 20+ | 94.00 |
| 17 | 252.5 | OP SB | Comments be overlaid Substanda | Existing AC ov with 1" thick a rd barrier repla | verlay on bric opropriate as cement is re | lge deck sh sphaltic ove commende | ould be rer erlay. d | noved full c | lepth, bare co | oncrete deck to | p be inspected | d, repaired if ne | eded and se | aled with pe | netrating decl | sealant .Then |
| | | 00750 Badger | 88 | 38 | ,Thrie | Yes | No | No | Yes | 1" | 1" | 1" | 16.05 | 16.05 | HS 20+ | F 93.0 |
| 17 | 255.9 | Spgs TI OP SB | Comments be overlaid Substanda | ients:Existing AC overlay on bridge deck should be removed full depth, bare concrete deck top be inspected, repaired if needed and sealed with penetrating deck sealant .Then rlaid with 1" thick appropriate asphaltic overlay. andard barrier replacement is recommended 0 38 11-1-1 Yes No Yes 1" 1" 15.01 HS 20+ F 93.0 | | | | | | | | | | | | |
| | | 00749 Badger | 90 | 38 | H-1-1 ,Thrie beam | Yes | No | No | Yes | 1" | 1" | 1" | 15.01 | 15.01 | HS 20+ | F 93.0 |
| 17 | 256.05 | Spgs TI OP NB | Comments be overlaid Substanda | Existing AC ov with 1" thick a rd barrier repla | verlay on bric opropriate as cement is re | lge deck sh sphaltic ove commende | iould be rer erlay. d | moved full c | lepth, bare co | oncrete deck to | p be inspected | d, repaired if ne | eded and se | aled with pe | netrating decl | sealant .Then |
| | | 00751 Bloody | 90 | 38 | H-1-1 ,Thrie beam | Yes | No | No | Yes | 1" | 1" | 1" | 15.32 | 15.32 | HS 20+ | F 93.0 |
| l 17 | 259.43 | Basin TI OP NB | Comments be overlaid Substanda | Existing AC ov with 1" thick a rd barrier repla | verlay on bric opropriate as cement is re | lge deck sh sphaltic ove commende | iould be rer erlay. d | moved full c | lepth, bare co | oncrete deck to | p be inspected | d, repaired if ne | eded and se | aled with pe | netrating decl | sealant .Then |
| | | 00752 Bloody | 90 | 38 | ,Thrie beam | Yes | No | No | Yes | 1" | 1" | 1" | 15.76 | 16.05 | HS 20+ | F 93.0 |
| 17 | 259.43 | Basin TI OP SB | Comments be overlaid Substanda | Existing AC ov with 1" thick a rd barrier repla | verlay on bric opropriate as cement is re | lge deck sh sphaltic ove commende | ould be rer erlay. d | moved full c | lepth, bare co | oncrete deck to | p be inspected | d, repaired if ne | eded and se | aled with pe | netrating decl | sealant .Then |
| | | | | | | | | | | | | | | | | |

Evaluation Completed by: Masudur Rahman

Date:

3/7/2018

Note: *N numbers are NBI numbers and A numbers are Arizona Items Number for bridge inventory

APPENDIX B – NEAR-TERM PREFERRED ALTERNATIVE TYPICAL SECTIONS AND PLAN & PROFILE

Typical Sections

Key Map

Plan Sheets

I-17 SB Profile (Black Canyon City to Sunset Point)

I-17 NB Profile (Sunset Point)

Alternative FL Profile (Black Canyon City)

North Crossover Profile

I-17 NB Profile (Black Canyon City)

Existing R/W 156'

Existing R/W 93'





SOUTHBOUND -

Inside Widening from New River Rd TI to Sta 1925+00 Outside Widening from Sta 1925+00 to Sta 2105+00 Inside Widening from Sta 2105+00 to Black Canyon City

SB RECOMMENDED CUT SLOPE RATIO

| Stai | tion | Cut Slope Ratio | | | | | |
|---------|---------|-----------------|--|--|--|--|--|
| Begin | End | Cur Slope Rallo | | | | | |
| 1490+00 | 1750+00 | 1H:1V | | | | | |
| 1750+00 | 1771+00 | 0.75H:1V | | | | | |
| 1771+00 | 1857+00 | 1H:1V | | | | | |
| 1857+00 | 1864+00 | 0.75H:1V | | | | | |
| 1864+00 | 1885+00 | 1H:1V | | | | | |
| 1885+00 | 1915+00 | 0.75H:1V | | | | | |
| 1915+00 | 1933+00 | 1H:1V | | | | | |
| 1933+00 | 1951+00 | 1H:1V | | | | | |
| 1951+00 | 1971+00 | 0.75H:1V | | | | | |
| 1971+00 | 2076+00 | 1H:1V | | | | | |
| 2076+00 | 2335+00 | 0.75H:1V | | | | | |

NB RECOMMENDED CUT SLOPE RATIO

MP 232.0 to MP 242.1

| Station | | | |
|-----------|---------|-----------------|--|
| Begin | End | Cut Slope Ratio | |
| 1490+00 | 1674+00 | 1H:1V | |
| 1674+00 | 1699+00 | 0.75H:1V | |
| 1699+00 | 1703+00 | 1H:1V | |
| 1703+00 | 1742+00 | 0.75H:1V | |
| 1742+00 | 1750+00 | 1H:1V | |
| 1750+00 | 1775+00 | 0.75H:1V | |
| 1775+00 | 1803+00 | 1H:1V | |
| 1803+00 | 1835+00 | 0.75H:1V | |
| 1835+00 | 1852+00 | 1H:1V | |
| 1852+00 | 1868+00 | 0.75H:1V | |
| 1868 + 00 | 1889+00 | 1H:1V | |
| 1889+00 | 1895+00 | 0.75H:1V | |
| 1895+00 | 1927+00 | 1H:1V | |
| 1927 + 00 | 1930+00 | 0.75H:1V | |
| 1930+00 | 1959+00 | 1H:1V | |
| 1959+00 | 1967+00 | 0.75H:1V | |
| 1967 + 00 | 1988+00 | 1H:1V | |
| 1988+00 | 2010+00 | 1H:1V | |
| 2010+00 | 2027+00 | 0.75H:1V | |
| 2027+00 | 2035+00 | 1H:1V | |
| 2035+00 | 2040+00 | 0.75H:1V | |
| 2040+00 | 2065+00 | 1H:1V | |
| 2065+00 | 2078+00 | 0.75H:1V | |
| 2078+00 | 2123+00 | 0.75H:1V | |
| 2123+00 | 2335+00 | 0.75H:1V | |





* 15 Feet of Height or Cut, Whichever is Lower

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40

66

70

78

85

28

37

54

58

65

68

60

80

100

120

160

200

Ditch Flow Line

ROCKFALL CONTAINMENT DITCH

1-17 TRACS NO. H6800 OIL

DESIGN

DRAWN

CHECKED

F.H.W.A. REGION STATE SHEET TOTAL NO. SHEETS RECORD DRAWING PROJECT NO. 9 ARIZ. 017-A(ARV)S 017 MA 229 Exst ADOT R/W Existing R/W 96' Pvmt Str Existing Frontage Road from Rock Springs Rd to Sta 2207+00 Sct No. 2 DATE NAME ARIZONA DEPARTMENT OF TRANSPORTATION PRELIMINARY 04/19 TWS INFRASTRUCTURE DELIVERY AND OPERATIONS DIVISION STAGE I RM 04/19 ROADWAY DESIGN SERVICES JAN 04/1 15% Review 1661 East Camelback Road, Suite 400 Phoenix, Arizona 85016 Phone: (602) 333-2200 NOT FOR TYPICAL SECTIONS CONSTRUCTION Stanley Consultants OR RECORDING ANTHEM WAY TI TO SUNSET POINT TI DWG NO.G-01.03 017-A(ARV)S OF_{-}

| Flex Lanes Recommended Cut Slope Ratios | | | | |
|--|---------|-----------|--|--|
| Station | | Cut Slope | | |
| Begin | End | Ratio | | |
| 2335+00 | 2364+00 | 1H:1V | | |
| 2364+00 | 2385+00 | 0.75H:1V | | |
| 2385+00 | 2397+00 | 1H:1V | | |
| 2397+00 | 2415+00 | 1H:1V | | |
| 2415+00 | 2443+00 | 0.75H:1V | | |
| 2443+00 | 2455+00 | 1H:1V | | |
| 2455+00 | 2680+00 | 0.75H:1V | | |

ROCK CONTAINMENT DITCH DETAIL



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APPENDIX C – FINAL SUMMARY OF COMMENTS AND RESPONSES FOR DRAFT FINAL DCR

REVIEW COMMENTS

| Submittal: | Draft Final Design Concept Report | Project Name: | I-17, Anthem Way TI to Jct. SR 69 |
|--------------------------|--------------------------------------|-------------------------|--------------------------------------|
| Date: | 3/08/2019 | Project No: | 17 MA 229 H6800 01L |
| Comment Due Date: | 3/22/2019 | Federal Aid No: | STP-017-A(ARV)S |
| Designer/ Consultant: | Stanley Consultants, Inc. | ADOT Project Manager | Asadul Karim, P.E. Major Projects |

ACTION CODES: A= WILL COMPLY *C= ADOT TO EVALUATE

*B= CONSULTANT TO EVALUATE

*D= DESIGN TEAM RECOMMENDS NO FURTHER ACTION

* REQUIRES A <u>WRITTEN EXPLANATION</u> AND FINAL DISPOSITION BY CONSULTANT/DESIGNER

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| TITLE | NO | PAGE NO | COMMENT | CODE | DISPOSITION | CODE |
| ADOT/Asadul Karim/ Project Manager | 1-1 | Exec. Summary | 2 nd bullet - Put "on" before Friday and Saturday. | A | Will add. | A |
| ADOT/Asadul Karim/ Project Manager | 1-2 | E.S. Table | Add (mile) to the Length column. | A | Will add. | A |
| ADOT/Asadul Karim/ Project Manager | 1-3 | Pg. 1 | Purpose and Need - 3 rd para., 1 st sentence – The purpose of the project is the add capacity todelete "to" after capacity. | D | Grammar is correct as shown. | D |
| ADOT/Asadul Karim/ Project Manager | 1-4 | Pg. 1 | Description of the project – 2 nd para., can you rephrase it? Hard to understand. Make it simple. | A | Will simplify paragraph. | A |
| ADOT/Asadul Karim/ Project Manager | 1-5 | Pg. 2 | Public Info. Meeting 1.4.1.2 – 2 nd para., …along I-17 in the study area – revise it to within study area. | A | Will revise. | A |
| ADOT/Asadul Karim/ Project Manager | 1-6 | Pg. 4 – Sec. 1.5.1 | Interstate I-17, 1 st para., after the table – "within the limits of the study"change it to within the study limits". | A | Personal preference item, but will revise. | A |
| ADOT/Asadul Karim/ Project Manager | 1-7 | Pg. 7 | Rephrase it to: There are no railroad crossings within the study limits. | D | Text is correct as shown. | D |

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| ADOT/Asadul Karim/ Project Manager | 1-8 | Pg. 15, Sec. 2.1.4 | Rephrase the 1 st sentence to make it more clear and understandable. | A | Will re-phrase. | A |
| ADOT/Asadul Karim/ Project Manager | 1-9 | Pg. 19, Sec. 2.3 | Conclusions #10 – "the northbound climbing lane should begin at" Where it starts and ends now? Please rephrase the sentence with further clarifications. | A | Older versions of the DCR included a more substantial climbing lane write-up. We will add part of it back in so that the conclusion makes more sense or revise the conclusion statement. | A |
| ADOT/Asadul Karim/ Project Manager | 1-10 | Pg. 51 | CCTV Monitoring 2 nd para., 2 nd sentence. Add "and" and delete comma between "Black Canyon City TI, at the Sunset Point Rest Area". | A | Will revise. | A |
| ADOT/Asadul Karim/ Project Manager | 1-11 | General | I did not see a cost item for PR? | C | Will add. ADOT Communications provided a PR cost of approx. \$41,000 that will be added to the estimate. | A |
| ADOT/David Benton/Bridge Design Manager | 2-1 | Pg. 47 | The existing vertical clearance on the SB direction for the inside widening at Rock Springs TI UP SB can be maintained with a break in the cross slope to maintain 16ft clear. Why can't we do that on the NB direction as well to maintain the 15.92 ft clear on the Rock Springs TI UP NB Bridge? The way I read it is that the only recommendation for a grade break is the SB direction only. Is this the case? And if so why? Can you please update the statement to reflect both NB and SB directions in that section, so it isn't confusing? | A | Will add statement that a cross slope break can also be added in NB direction to maintain the existing vertical clearance. (However, a design exception will still be required for VC less than 16'.) | A |
| ADOT/Craig Regulski/Sr. Project Manager | 3-1 | Tables 20 - 21 | Missing labels for NB and SB for the configuration of the gore point. | A | Will add. | A |
| ADOT/Reed Henry/ Predesign Section Mgr | 4-1 | Sec. 2.2 | Tables indicate a 4-1/2 year crash evaluation period but text states it a 5 year period. Please rectify time period and crash numbers. | A | Will revise. | A |
| ADOT/Reed Henry/ Predesign Section Mgr | 4-2- | Pg. 29 | Flex lane figure shows 6' inside shoulder and 4' inside shoulder to barrier. Following paragraph indicates a 2' shy distance for the inside barrier, should the reference to shy distance be removed? | A | Will remove reference. | A |

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| ADOT/Reed Henry/ Predesign Section Mgr | 4-3 | Pg. 38 | Section 4.3.1 4th Para. Please clarify how the structural section is different due to overlays? | A | The difference in the pavement section thickness between the mainline and the shoulder from the overlays is variable across the project length as the shoulder has been paved with asphalt rubber in some areas, but not others. Asphalt rubber is proposed for mainline travel lanes and both shoulders as shown in the typical sections in Appendix A. This information will be added to the DCR. | A |
| ADOT/Reed Henry/ Predesign Section Mgr | 4-4 | Pg. 58 | Sections 4.21 and 4.22 may be impacted by revisions to safety study and DE/DV request. | A | Section will be updated to correspond to DE/DV request. | A |
| ADOT/Reed Henry/ Predesign Section Mgr | 4-5 | Pg. 62 | Section 5.1 reference AASHTO Interstate Standard. | A | Will add reference. | A |
| ADOT/Reed Henry/ Predesign Section Mgr | 4-6 | Pg. 62 | Section 5.4 MP 252.21 to MP 253.08 | A | Entry will be deleted since it's outside the construction limits. | A |
| ADOT/Reed Henry/ Predesign Section Mgr | 4-7 | Pg. 63 | Section 5.4 do not use the word "adequate". Suggest stating it does not meet recommended minimum AASHTO. | A | Will revise. | A |
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| ADOT/ Bob LaJeunesse/ NW District | 5-1 | 3 | Table 1 would be easier to read if it was sorted by construction date. | A | Will sort table by construction date. | A |
| ADOT/ Bob LaJeunesse/ NW District | 5-2 | Appendix B C-01.30 | It looks like vehicles coming off the SB flex lanes could still access the Coldwater Canyon exit ramp. This could create a weaving problem that needs some attention. | C | Text will be added to call the final designer's attention to the questions. Barrier could be extended south past the exit gore. Rumble strips could be added in the gore. Relative ramp volumes at BCC will be added. | A |
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| ADOT/James Bramble/ NW District | 6-1 | Pg. 54 Section 4.14.1 | Is the statement that the flex lanes will likely be a separate project still accurate? Perhaps modify it to state that it could be separate or at least a separate phase of one overall project. | A | Text will be revised. | A |

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| ADOT/James Bramble/ NW District | 6-2 | Pg. 54 Section 4.14.1 | Although the traffic volumes are low, detouring NB traffic to use Sunset Point during the SB Bumble Bee bridge work will not be desirable. | С | Text will be expanded. The proposed phasing with routing Bumble Bee drivers north to Sunset Point, then back to the Bumble Bee TI would be inconvenient. Shifting the Bumble Bee Road alignment would be complicated by topography and already-tight geometrics. Consider accelerating construction with night or weekend work to limit inconvenience. Consider liquidated damages. | A |
| ADOT/James Bramble/ NW District | 6-3 | Pg. 54 Section 4.14.1 | Bridge Construction; please identify the structure that would be reconstructed over existing roadways. I know it is stated elsewhere but it would be helpful to add it here | A | Will add structure name. | A |
| ADOT/James Bramble/ NW District | 6-4 | Pg. 55 Section 4.16 | Signing and Pavement Marking - Milling and replacing the existing pavement friction course is the preferred method for stripe obliteration other than minor, short sections of striping. | A | Estimate assumed milling and replacing pavement friction course would be utilized for stripe obliteration wherever applicable. It was assumed that RPMs would be obliterated before milling. Text will be revised to reflect these assumptions. | A |
| ADOT/James Bramble/ NW District | 6-5 | Pg. 56 Section 4.18 | ADOT has typically been including items for either spraying herbicide or mechanically removing noxious and invasive weeds. This could be a substantial item due the project's length and duration and could possibly be mentioned in this section. | A | Will add paragraph to address Noxious and Invasive Species treatment that can be incorporated as needed. Noxious weed treatment will also be added to the cost estimate. | A |
| ADOT/John Litteer/ NW District | 7-1 | 16-17 | Sec 2.1.6: Clarify discussion, suggest separate the discussions on the diverge and merge conditions (both directions). For NB merge, include discussion for length needed for trucks at the top of the hill to regain operating speed. | A | Northbound and southbound results will be identified in Tables 20 and 21. Climbing lane calculations included in Preliminary Traffic Report cite that trucks would regain normal operating speed of 65 MPH at approximately MP 252.65. This information will be cited in the discussion. | A |
| ADOT/John Litteer/ NW District | 7-2 | 16-17 | Also, it sounds from the discussion that the option lane for the flex lanes does not provide capacity, and that two exit lanes would be required. Figure 11 and plans still shows option lanes. Suggest also show | A | Results indicate that a combination trapped lane and optional exit lane configuration is necessary for both the NB and SB approaches to the flex lanes. Text will be added to clarify these are the | A |

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| | | | schematic diagrams of alternatives discussed, and recommended alternative. | | recommended alternatives. These lane configurations are reflected on the recommended alternative shown in Figure 11 and on plans in Appendix B. | |
| ADOT/John Litteer/ NW District | 7-3 | 16-17 | Please also discuss the short distance for NB south crossover, and that consideration should be given to extend the crossover length for separation from SB flex operations and potential wrong way movements. | С | More description/detail will be added to the text. The final designer should try to lengthen the crossover so that it's more uninviting to NB traffic when the flex lanes are open to SB traffic. | A |
| ADOT/John Litteer/ NW District | 7-4 | 28 | Sec 3.3.4: Suggest reference percentage of truck volumes (in RDG Table 302.4) when discussing 12' shoulders. Traffic data in report shows high truck percentage. | A | Will be added. | A |
| ADOT/John Litteer/ NW District | 7-5 | 28, 37, Table 32 etc. | Should discussion on median barriers for flex lanes include glare screen? Could help with opposing headlights at night, visual distractions, etc. | A | Text will be added to consider the addition of glare screen to 42" median barrier. | A |
| ADOT/John Litteer/ NW District | 7-6 | 47 | Sec 4.11.6: Discuss how access will be prevented from SB flex lanes to SB exit ramp. | С | Text will be added to the DCR. See also response to Comment 5-2. | A |
| ADOT/John Litteer/ NW District | 7-7 | 48 | Sec 4.11.8: Discuss how access will be prevented from NB flex lanes to NB exit ramp, and from SB entrance ramp to SB flex lanes. | A | Text will be added. Similar to previous comment. The SB entrance ramp ties into I-17 downstream of the flex lane entrance. Barrier will prevent access from SB entrance ramp to SB flex lanes at Sunset Point. | A |
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| ADOT/Todd Steinberger/ NW District | 8-1 | General | Has the capacity of the new median cut ditch been analyzed to see the impact of the construction of the southbound flex lanes. Will ponding on inside shoulder and passing lane occur? | A | Inlets are added along the flex lanes barrier and were placed to meet spread criteria. | A |
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| ADOT/Jim Windsor/ TSM&O | 9-1 | | No comments on ITS. Agree with lighting direction. | | | |
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| ADOT/ Navaphan Viboolmate/ Bridge | 10-1 | | | | | |

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|------------------|------|---------|---------|---------|-------------|-------|
| TITLE | NO | SHEET, | | INITIAL | | FINAL |
| | | PAGE NO | COMMENT | CODE | DISPOSITION | CODE |

| MAG/Chaun Hill | 11-1 | | No comments. | | | |
|--|------|----|---|---|--|---|
| | | | | | | |
| ADOT/Joan Lovell/ Systems Technology Group | 12-1 | 50 | Add to the first sentence in 4.13 ITS/ Incident Management : and is now incorporated in the Statewide ITS Architecture | A | Will comply. | A |
| ADOT/Joan Lovell/ STG | 12-2 | 50 | 413.1 Recommended ITS Element. The bullets items need to match the Headings on the following pages. | A | Will comply. | A |
| ADOT/Joan Lovell/ STG | 12-3 | | 413.1 Recommended ITS Element . Add Bullet Flex Lanes to the bulleted items and place it in the proper order of headings on the following pages | A | Will comply. | A |
| ADOT/Joan Lovell/ STG | 12-4 | 51 | Remove References to one mile spacing for detection between AW and BCC. Detection will only be needed in concert with the Flex lanes | A | Will comply. | A |
| ADOT/Joan Lovell/ STG | 12-5 | 51 | Remove the word "acoustic" from the first Paragraph | A | Will comply. | A |
| ADOT/Joan Lovell/ STG | 12-6 | 51 | Remove reference to detection at one mile spacing in the CCTV Monitioring . | A | Will comply. | A |
| ADOT/Joan Lovell/ STG | 12-7 | 51 | CCTV Monitoring Add: Placement of CCTV in areas where power is readily available and CCTV can be powered by #2 AWG and smaller wire. Otherwise fixed cameras with a solar powered application shall be used. | С | If this comment is also applicable within the Flex Lanes section, it may limit the ability of ADOT to clear the fixed lanes if it requires using fixed cameras with solar rather than pan/tilt/zoom (PTZ) cameras powered by larger wire sizes than a #2 AWG. PTZ cameras would give ADOT much greater flexibility in the use of cameras to clear the flex lanes. Larger wires will be needed to provide enough cameras for complete coverage of the flex lanes. | A |
| ADOT/Joan Lovell/ STG | 12-8 | 52 | Flex Lanes: Paragraph 5 remove the word "Phoenix" from ADOT Phoenix Traffic Operations Center (TOC) | A | Will comply. | A |
| ADOT/Joan Lovell/ STG | 12-9 | 53 | Flex Lanes Delete: "as well as along the corridor" 2 nd Paragraph on page 53 to read "The use of detectors is anticipated to supplement the CCTV camera system for clearance verification. Detector stations can be installed at key locations near the entry gates and at the end of the flex lanes." | С | Most of the detectors will be placed near the flex lane crossovers. They are not needed south of Black Cyn City or on the flex lanes. | A |
| | | | | | | |

| AGENCY/REVIEWER/ TITLE | ITEM NO | DWG, SHEET, PAGE NO | COMMENT | INITIAL CODE | DISPOSITION | FINAL CODE |
|------------------------------------|------------|---------------------------|--|-----------------|-------------|---------------|
| ADOT/Brent Conner/ Geotechnical | 13-1 | Gen'l | ADOT has reviewed the preliminary geotechnical report by Wood. We have no comments on the preliminary geotechnical report or DCR. There may be opportunities in final design following completion of the geotechnical investigation to reduce excavation volume. The proposed outside widening at the Cape Horn geohazard may be evaluated in final design as discussed at the March project meeting. | A | Agreed. | A |
| | | | | | | |

APPENDIX D – APPROVED DESIGN EXCEPTION AND DESIGN VARIANCE LETTERS