

Arizona Department of Transportation

Environmental Planning

DRAFT
Noise Analysis Technical Report

West Kingman Traffic Interchange

Federal Project No. 040-A(212)N ADOT Project No. 040 MO 048 H7993 01 L

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APPROVED

By Ivan Racic at 1:02 pm, Feb 26, 2020

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DRAFT Noise Analysis Technical Report FOR West Kingman Traffic Interchange Interstate 40 MP 48.32 to MP 51.75 (Stockton Hill Road) US Route 93 MP 69.60 to MP 71

Federal Project No. 040-A(212)N ADOT Project No. 040 MO 048 H7993 01 L

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January 30, 2020

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EXECUTIVE SUMMARY

Project Objectives

The Arizona Department of Transportation (ADOT) is initiating an engineering and environmental study to identify and evaluate alternatives for a proposed Traffic Interchange (TI) to connect Interstate 40 (I-40) and U.S. Route 93 (US 93). The project limits on I-40 extend from milepost (MP) 48.32 to MP 51.75 (Stockton Hill Road) and along US 93 from MP 69.60 to approximately MP 71.00 (US 93/1-40 system interchange).

The West Kingman Traffic Interchange (TI) project would improve capacity and operational efficiency by providing a high-speed interchange between Interstate 40 (I-40) and United States Route 93 (US 93). A free-flowing connection between I-40 and US 93 would increase local and regional mobility, provide better access between regional economic hubs, eliminate the "bottleneck" along the future I-11 corridor, and support interstate commerce.

Current Noise Environment

Land use in the project area may be categorized as Federal Highway Administration (FHWA) Activity Category B, C, D, E, F and G as defined in the Code of Federal Regulations (CFR) Title 23 Part 772 (23 CFR 772) and ADOT Noise Abatement Requirements (NAR) (ADOT, 2017). Residential areas within the study area, which for the purposes of this noise analysis is defined as within 650 feet of the future edge of pavement for the two Build Alternatives, include single-family, multifamily (apartments), mobile home and recreational vehicle communities. These uses were evaluated as Category B in this noise study. Category C uses include schools, parks, a sports complex, multi-use pedestrian paths and trails and a historic building, each afforded protection as Department of Transportation Act of 1966 Section 4(f) resources in addition to a privately funded school, a non-profit institutional structure and a government health facility. The 4(f) properties were evaluated for mitigation per Category C noise abatement criteria per 23 CFR 772 and the ADOT NAR. Evaluation of these properties per 23 CFR 774.15 is not addressed in this report; however, the noise level predictions reported inform the evaluation of 4(f) properties completed for the EA.

Commercial uses within the study area include hotels/motels, restaurants, gas stations/truck stops with convenience stores/food service, office buildings and office parks categorized as Activity Category E. Locations with an outdoor use (pool, sitting, dining or common area) were included in the evaluation of potential noise impacts. Vacant or undeveloped residential properties or parcels were evaluated as Category G uses. Category F land uses, such as auto repair shops on Beale Street were not included in the study.

ADOT *Highway Performance Monitoring System (HPMS)* data indicate traffic on I-40 is highest between 12:00 p.m. and 1:00 p.m. in the eastbound direction and 12:30 p.m. and 1:30 p.m. in the westbound direction. For the purpose of noise model validation, noise measurements were recorded between 11:30 a.m. and 5:40 p.m. including this peak period; however, traffic was free flowing during the entire measurement interval. Measurements ranged between 57 A-weighted decibels dB(A) adjacent to a single-family home on Fort Beale Drive north of US 93/Beale Street

to 61 dBA on an undeveloped parcel located approximately 175 feet north of the I-40 westbound (WB) lanes.

The proposed improvements include a significant reconfiguration and shifting of an existing traffic interchange and the addition of through travel lanes. As such, the project is considered a Type I project per 23 Code of Federal Regulations (CFR) Part 772.5 and a determination of impacts and mitigation must be considered under 23 CFR 772 and NEPA.

Noise Impact Information

This analysis was performed in compliance with the current (May 2017) *ADOT Noise Abatement Requirements* (NAR). The ADOT NAR establishes official policy on highway noise and describes the process that is used in determining traffic noise impacts and evaluating abatement measures. The ADOT NAR is based on the noise levels approaching the FHWA Noise Abatement Criteria (NAC). ADOT defines "approaching" as within 1 dBA of the FHWA NAC for Activity Categories A, B, C, D, and E. There are no noise impact thresholds for Activity Category F or G. ADOT requires that feasible and reasonable measures be considered and evaluated to abate traffic noise at all identified traffic noise impacts.

A summary of noise analysis parameters is presented in **Table ES-1**. In general, peak hour noise levels are predicted to increase above the 2040 No-Build, with the number of noise-sensitive land uses (receptors) impacted by Build Alternative I and Build Alternative IV virtually identical.

West Kingman Traffic Interchange							
Noise Analysis Parameters	Existing	Future 2040					
Noise Analysis Farameters	2017	No-Build	Build				
No. of Modeled Receivers	310	310	310				
No. of Representative Noise Receptors	535	535	535				
Range of Peak Hour Noise Levels, dBA	41 - 79	43 - 81	43 - 81				
No. of Receptors Exceeding the ADOT Approach of the FHWA Noise Abatement Criteria (NAC)	275	336	330				
No. of Barriers Evaluated for Mitigation	N/A	N/A	9				
No. of Barriers Satisfying ADOT Noise Abatement Requirements (NAR) Reasonableness and Feasibility Criterion	N/A	N/A	2				
No. of Recommended Barriers	N/A	N/A	3 ¹				
Total Cost of Recommended Mitigation	N/A	N/A	\$6,888,954 ²				
Average Cost per benefited (5 dBA or more)	N/A	N/A	\$21,939				

Table ES-1. Summary of Noise Analysis

- One barrier is recommended to replace an existing noise wall located along the existing I-40 eastbound (EB) on-ramp from Beale Street which would be removed by the Build Alternative. The barrier, NB#1 does not meet one or more of the ADODT NAR reasonableness and feasibility requirements.
- 2. Mitigation cost is based on \$35/ft² for new construction; \$85/ft² for wall segments on structure.

Noise Abatement Measures Determination (Recommended/Not Recommended)

ADOT considers mitigation for noise sensitive areas predicted to be impacted by highway traffic noise levels from ADOT's transportation improvement projects. The noise level impact determination used in this analysis is based on the ADOT Noise Abatement Requirements (NAR), dated May 2017. Noise barriers (walls) were considered as mitigation measures that would provide noise shielding to impacted locations. Reasonableness and feasibility criteria were evaluated for each proposed noise wall or wall combination (two or more wall) per ADOT NAR guidelines.

A total of nine noise walls were evaluated to provide mitigation of future (2042) peak hour noise levels associated with Build Alternative. Two of the barriers evaluated meet all ADOT NAR requirements and are recommended. A third barrier does not meet one or more of the ADOT NAR requirements but is recommended to replace an existing noise wall located along the I-40 EB on-ramp from Beale Street. The remaining six barriers are not recommended. The total cost of recommended mitigation is \$6,888,954 at an average cost of \$21,939 per benefited receptor. All recommendations are based on preliminary (30% or less) design information and should be revaluated at future stages of design. ADOT encourages designers to examine and explore all possibilities that would be conducive to project delivery schedule, eliminating impacts while safeguarding taxpayers' money.

INTRODUCTION

The Arizona Department of Transportation (ADOT) is initiating an engineering and environmental study to identify and evaluate alternatives for a proposed Traffic Interchange (TI) to connect Interstate 40 (I-40) and U.S. Route 93 (US 93). The project limits on I-40 extend from milepost (MP) 48.32 to MP 51.75 (Stockton Hill Road) and along US 93 from MP 69.60 to approximately MP 71.00 (US 93/1-40 system interchange, refer to Figures 1 and 2).

Purpose and Need

The West Kingman Traffic Interchange (TI) project would improve capacity and operational efficiency by providing a high-speed interchange between Interstate 40 (I-40) and United States Route 93 (US 93). A free-flowing connection between I-40 and US 93 would increase local and regional mobility, provide better access between regional economic hubs, eliminate the "bottleneck" along the future I-11 corridor, and support interstate commerce.

Project Description

The original design and environmental study for this project resulted in the preparation of a Design Concept Report and a draft Environmental Assessment (EA), both published in 2015. Since the project was not fiscally constrained, it was shelved until funding was available. In the interim, some improvements were completed under a different project to address the most critical needs at the Beale Street traffic interchange (TI). Project funding has now been identified for a portion of the improvements, and the design is being revisited based on current conditions in the project area and current standards. During these investigations and based on coordination with stakeholders, modifications to the previously recommended alternative have been identified. The modifications include improving the:

- Configuration of the new West Beale Street TI (incorporating free-flow ramps)
- Width of Beale Street following construction
- Lengthened merge lanes from Beale Street onto US 93 to include parallel merging lanes
- System-to-system ramp configurations lengthening parallel merge lanes.

In addition, by shifting the widening of I-40 to the median, the cuts into the hills, impacts to Clack Canyon, and overall earthwork would be reduced. The project limits have been expanded along I-40 and US 93 from the original study to allow for necessary improvements in capacity to Stockton Hill Road and to allow for transition to existing lane configurations at the project termini. ADOT is in the process of refining the design of this updated alternative and completing the environmental studies.

Figure 1. Project Location Map

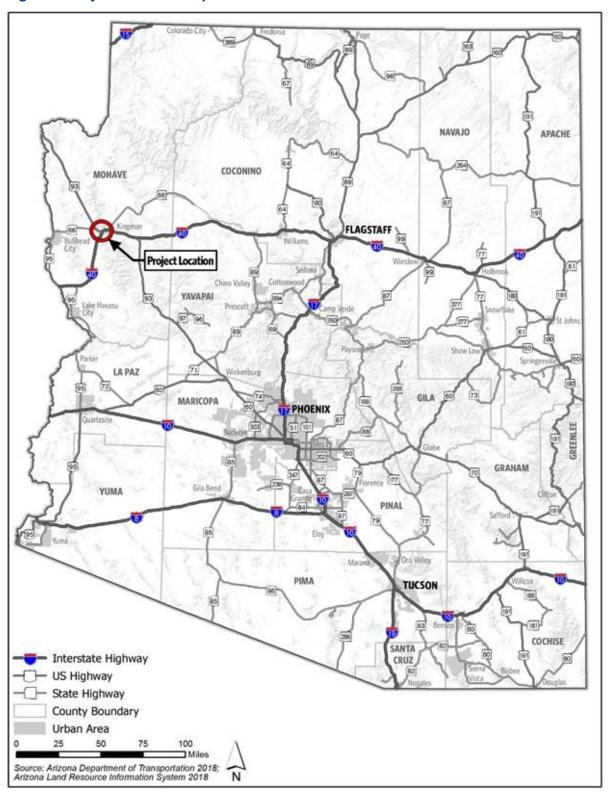
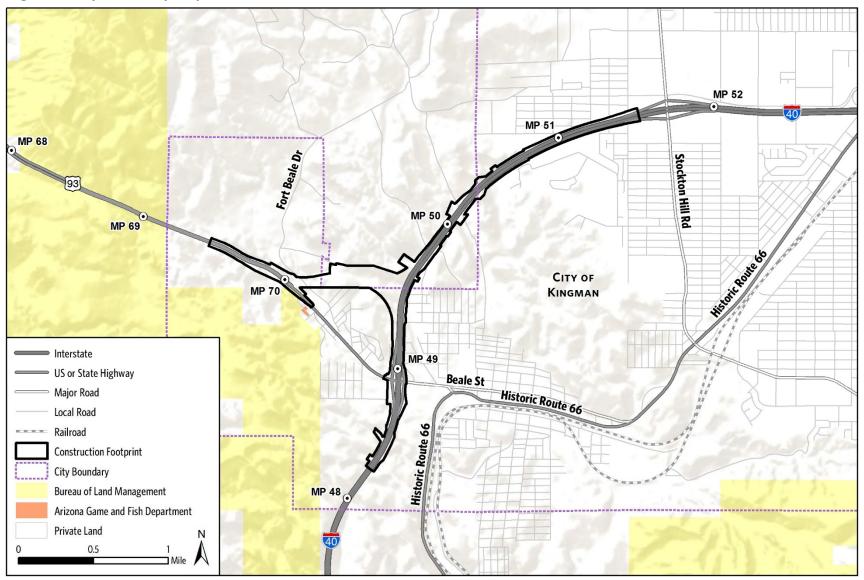


Figure 2. Project Vicinity Map



The current scope of work includes the following:

- Provide free-flow, grade-separated ramps to service I-40 westbound (WB) to US 93 northbound (NB) and US 93 southbound (SB) to I-40 eastbound (EB), resulting in approximately one mile of new highway ramps
- Widen and conduct deck rehabilitation of the existing White Cliff Road Overpass EB #1839 and White Cliff Road Overpass WB #1840
- Widen Clack Canyon Wash Bridge EB #1837
- Rehabilitate the deck of Clack Canyon Wash Bridge WB #1838
- Widen of I-40 and US 93
- Construct new cable barrier as needed
- Construct new on-site drainage collection and conveyance systems
- Extend existing culverts and pipes as needed

Type I Trigger for Noise Analysis

As per 23 CFR 772 and the ADOT NAR traffic noise analysis is required for any projects that receive federal-aid funds or are otherwise subject to FHWA approval. They include federal projects that are administered by Local Public Agencies (LPAs) as well as ADOT. In addition to federal projects, it is required for other ADOT-funded projects that involve:

- construction of a highway on new alignment or
- a significant change in the horizontal or vertical alignment of an existing highway or
- adding new through lanes to an existing highway.

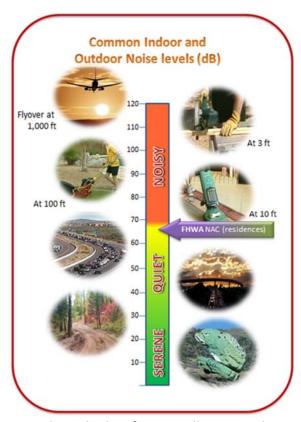
The proposed improvements include a significant reconfiguration and shifting of an existing traffic interchange and the addition of through travel lanes. Therefore, this project meets the definition of a Type I project as defined in ADOT NAR (ADOT, 2017) and a detailed traffic noise analysis is required. Per 23 CFR 772, if any segment or component of an alternative meets the definition of a Type I project, then the entire alternative is considered a Type I project and subject to noise analysis requirements. Land use in the project area may be primarily categorized as FHWA Activity Category B, C, D and E and includes single-family and multifamily units (apartments), mobile home communities, assisted living communities, a recreational vehicle short-term rental park, commercial uses including motels and restaurants, office buildings, and Section 4(f) multi-use paths, recreation areas, a public golf course and a school. Category F and G activity areas for which noise abatement criteria are not defined include gas stations/convenience stores and undeveloped residential parcels.

FUNDAMENTALS OF TRAFFIC NOISE

Sound is the sensation produced by stimulation of the hearing organs produced by continuous and regular vibrations of a longitudinal pressure wave that travels through an elastic medium (air, water, metal, wood) and can be heard when they reach a person's or animal's ear. When sound travels through air, the atmospheric pressure wave variations occur periodically. It travels in air at a speed of approximately 1087 ft. per second at sea level and temperature of 32 °F. Noise is usually defined as any "unwanted sound," and consists of sounds that are perceived as interfering with communication, work, rest, and recreation. It is characterized as a non-harmonious or discordant group of sounds.

Sound Pressure Levels, Decibels, Frequencies and A-Weighted Decibels-dB(A)

Noise can be measured in Pa (Pascal). A healthy human ear can detect a pressure variation of 20 μ Pa and it is referred to as threshold of hearing.



Logarithmic scale is useful for handling numbers on a wide scale, but for a smaller span, the decibel or (dB) scale is used. Sound pressure level (SPL) is calculated is using measured sound level and the hearing threshold of 20 μ Pa or 20 x 10⁻⁶ Pa as the reference level, this level can also be defined as 0 dB. The decibel alone is insufficient to describe how human ear responds to sound pressures at all frequencies. The human ear has peak response in the range of 2,500 to 3,000 Hz and has a somewhat low response at low or even high frequencies. In response to the human ear sensitivity, the A-weighted noise level, referenced in units of dB(A), was determined to better resemble people's perception of sound levels. This dB(A) unit of measurement is used in noise studies and reporting. Changes in sound level under 3 dB(A) are not noticed by human ear, while the human ear perceives a 10 dBA increase in sound level to be a doubling of sound.

Noise Descriptors

The most commonly used noise descriptor in traffic noise analysis is Equivalent Sound Level (L_{eq}). L_{eq} represents an average of the sound energy occurring over a specified period. In effect, L_{eq} is the steady-state sound level containing the same acoustical energy as the timevarying sound that actually occurs during the same period. The 1-hour A-weighted equivalent sound level [$L_{Aeq(h)}$] is the energy average of A-weighted sound levels occurring during a one-hour period and is the basis for noise criteria used by ADOT.

What are source, receiver, receptor, and path when talking about traffic noise?

Traffic noise is a combination of the noises produced by vehicle engines, exhaust, and tires. The source of highway traffic comes from vehicles traveling on highways. The noise level at the *Source* depends on pavement type, number of heavy trucks, traffic volumes, and traffic speeds. The predominant noise sources in vehicles at speeds less than 30 miles per hour (mph) are engine and exhaust. At speeds greater than 30 mph, tire noise becomes the dominant noise source.

In Figure 3, the Receptor is any location where people are affected by the traffic noise. It can be residence, park, school, playground and any other place where frequent human use occurs. An area between the source and the receptor (receiver represents a receptor(s) when modeled in FHWA Traffic Noise Model) is considered a path. Depending on the path surface, propagation of sound may be reduced; such is the case for the soft ground and fresh snow. Doubling the distance between the source and receptor reduces noise by 3 dBA depending on the ground.

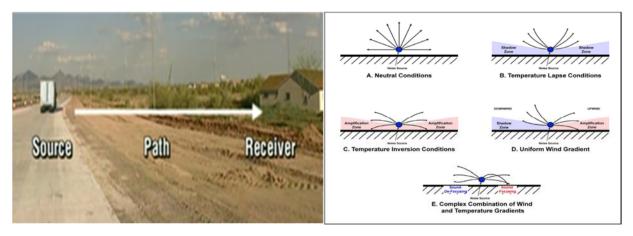


Figure 3. Source, Propagation Path, Receptor

Air changes its density due to variation of humidity and temperature, and wind influences refraction of sound waves. Wind, humidity, and temperature may have a significant impact, but only influences the receptors located a long distance away from source. As residents are usually much closer to the noise source, any atmospheric conditions are insignificant for consideration. For more information on noise, please visit ADOT Environmental Planning Noise webpage.

NOISE IMPACT CRITERIA

As required by 23 CFR 772.11(e), the point at which noise levels "approach" the Noise Abatement Criteria (NAC) established by the Federal Highway Administration (FHWA) is defined by ADOT as 1 dBA, for Activity Categories A, B, C, D, and E (**Table 2**). There is no noise impact threshold for Category F or Category G locations. As required by 23 CFR 772.5, ADOT defines a Substantial Increase in noise levels as an increase in noise levels of 15 dBA in the predicted noise level over the existing noise level.

Table 2. FHWA Noise Abatement Criteria [1]

Activity Category	dB(A), Leq1h²	Activity Description
А	57 (exterior)	Land on which serenity and quiet are of extraordinary significance and serve an important public need, and where the preservation of those qualities is essential if the area is to continue to serve its intended purpose
В	67 (exterior)	Residential
С	67 (exterior)	Active sports areas, amphitheaters, auditoriums, campgrounds, cemeteries, day care centers, hospitals, libraries, medical facilities, parks, picnic areas, places of worship, playgrounds, public meeting rooms, public or nonprofit institutional structures, radio studios, recording studios, recreation areas, Section 4(f) sites, schools, television studios, trails, and trail crossings
D	52 (interior)	Auditoriums, day care centers, hospitals, libraries, medical facilities, places of worship, public meeting rooms, public or nonprofit institutional structures, radio structures, recording studios, schools, and television studios
E	72 (exterior)	Hotels, motels, offices, restaurants/bars, and other developed lands, properties or activities not included in categories A–D or F
F		Agriculture, airports, bus yards, emergency services, industrial, logging, maintenance facilities, manufacturing, mining, rail yards, retail facilities, shipyards, utilities (water resources, water treatment, electrical), and warehousing
G		Undeveloped lands that are not permitted

¹ Sources: Federal Highway Administration (2011); 23 Code of Federal Regulations § 772

² The 1-hour equivalent loudness in A-weighted decibels, which is the logarithmic average of noise over a 1-hour period

NOISE SENSITIVE LAND USES

Land use in the project area may be categorized as FHWA Activity Category B, C, D, E, and G. The Category B land uses in the study area, which for the purposes of this noise analysis is defined as within 650 feet of the future edge of pavement for the Build Alternative, include 19 named and unnamed residential areas including single-family, multi-family (apartments), and mobile home communities located proximate to I-40. Category C uses include the City of Kingman-owned Cerbat Cliffs Golf Course, a picnic area at the Positive Alternative Campus, the Camp Beale Monolith Connector multi-use trail, and the Camp Beale Springs parking area, which are also afforded protection per Section 4(f) of the Department of Transportation Act of 1966. Additional Category C land uses include four assisted living communities. Where impacted by design year peak hour noise levels, the 4(f) properties were evaluated for mitigation per Category C noise abatement criteria per 23 CFR 772 and the ADOT NAR. Evaluation of these properties per 23 CFR 774.15 Constructive use determinations is not addressed in this report; however, the noise level predictions reported inform the evaluation of 4(f) properties completed for the EA.¹

Commercial uses include the Fort Beale RV Park, fast food restaurants, gas stations/truck stops with convenience stores/food service, three motels and a hotel, office space for the Helen's Place Assisted Living Facility categorized as Activity Category E. Only those commercial uses with outdoor use areas with an outdoor use (pool, sitting, dining or common area), such as the Motel 6 and Home2Suites Hotel were included in the evaluation of potential Category E noise impacts. Category G land uses include eight undeveloped residential parcels.

For this analysis, peak traffic hour noise levels have been calculated at locations representing one or more receptor location (receivers). **Figure 4** shows the receiver locations and **Table 4** (p. 22 of this report) lists the Activity Category, description and number of receptors represented by each.

EXISTING NOISE ENVIRONMENT

The methodology used for highway noise level measurements is to comply with procedures specified in Section 4 - Existing-Noise Measurements in the Vicinity of Highways - of the FHWA document FHWA-PD-96-046/DOT-VNTC-FHWA-96-5, *Measurement of Highway-Related Noise* (FHWA, 1996).

Ambient noise levels were established by field measurements Activity Categories B and G for validation of the FHWA Traffic Noise Model version 2.5 (TNM). Existing noise levels were predicted using the FHWA TNM model and the existing peak hour traffic as reported in the Change of Access Report, I-40/US 93 West Kingman System Traffic Interchange [traffic analysis/traffic report] (ADOT, 2020).

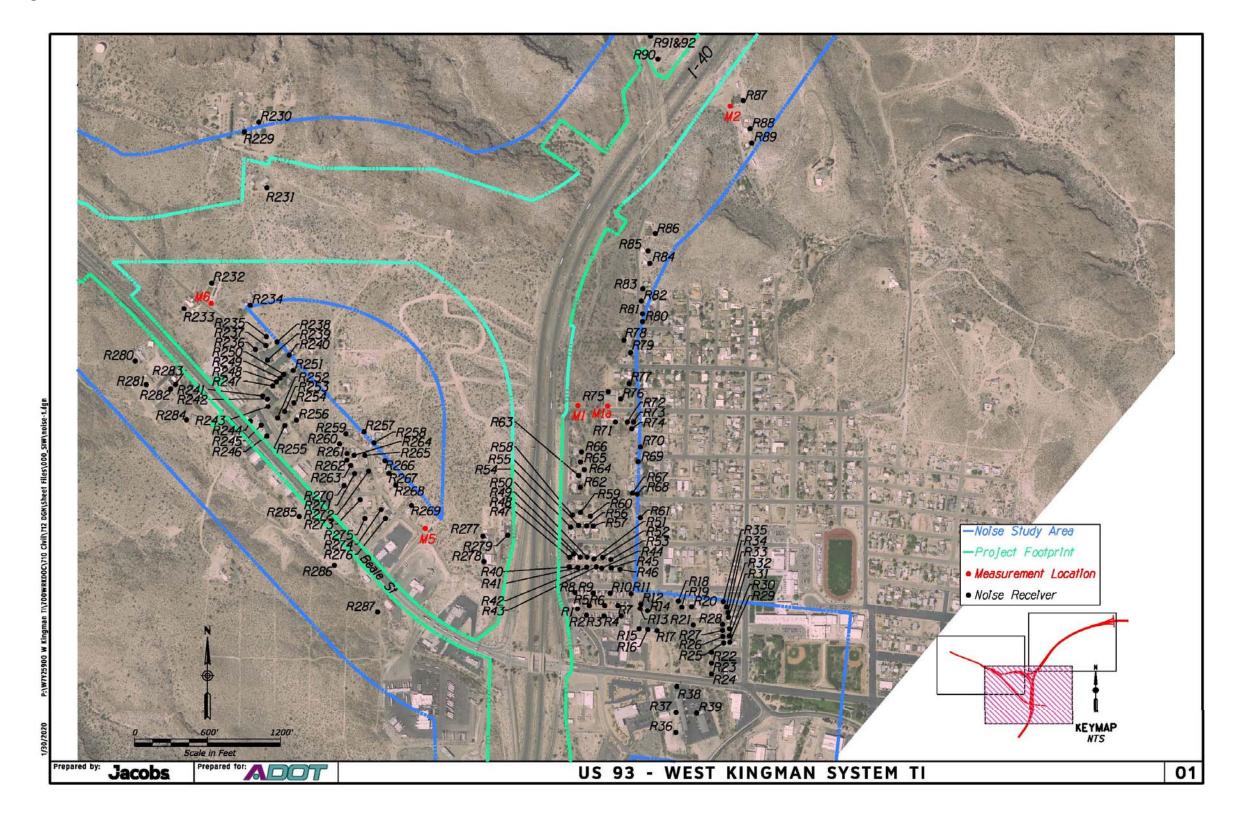
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¹ There are three properties/facilities that have been evaluated as Section 4(f) Resources for the EA. Only portions of those properties within the noise study area that have not been incorporated into transportation facilities are included in this noise study. Appendix F includes a map of all 4(f) Resources in the project area and those portions included in this noise study. Trails shown on the map that are planned or proposed but not developed were not included in the analysis.

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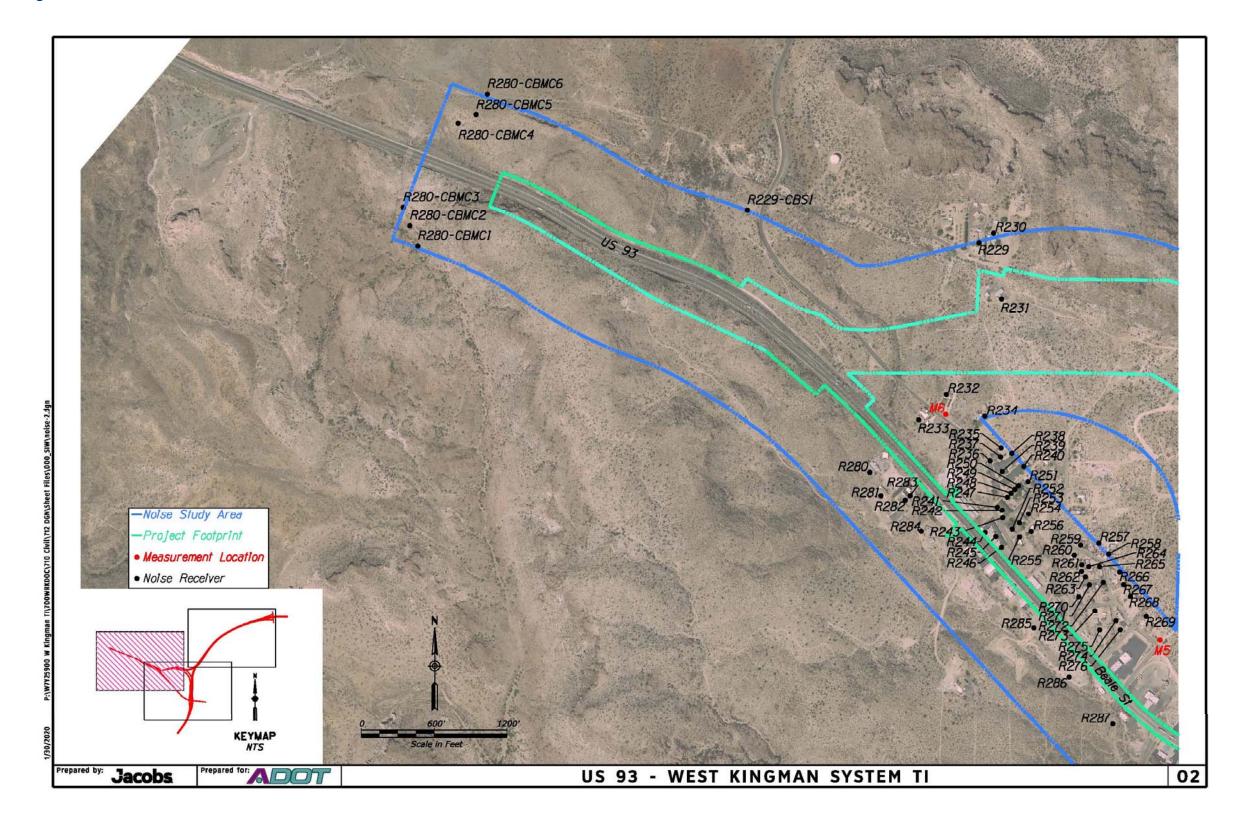
Figure 4. Noise Receivers



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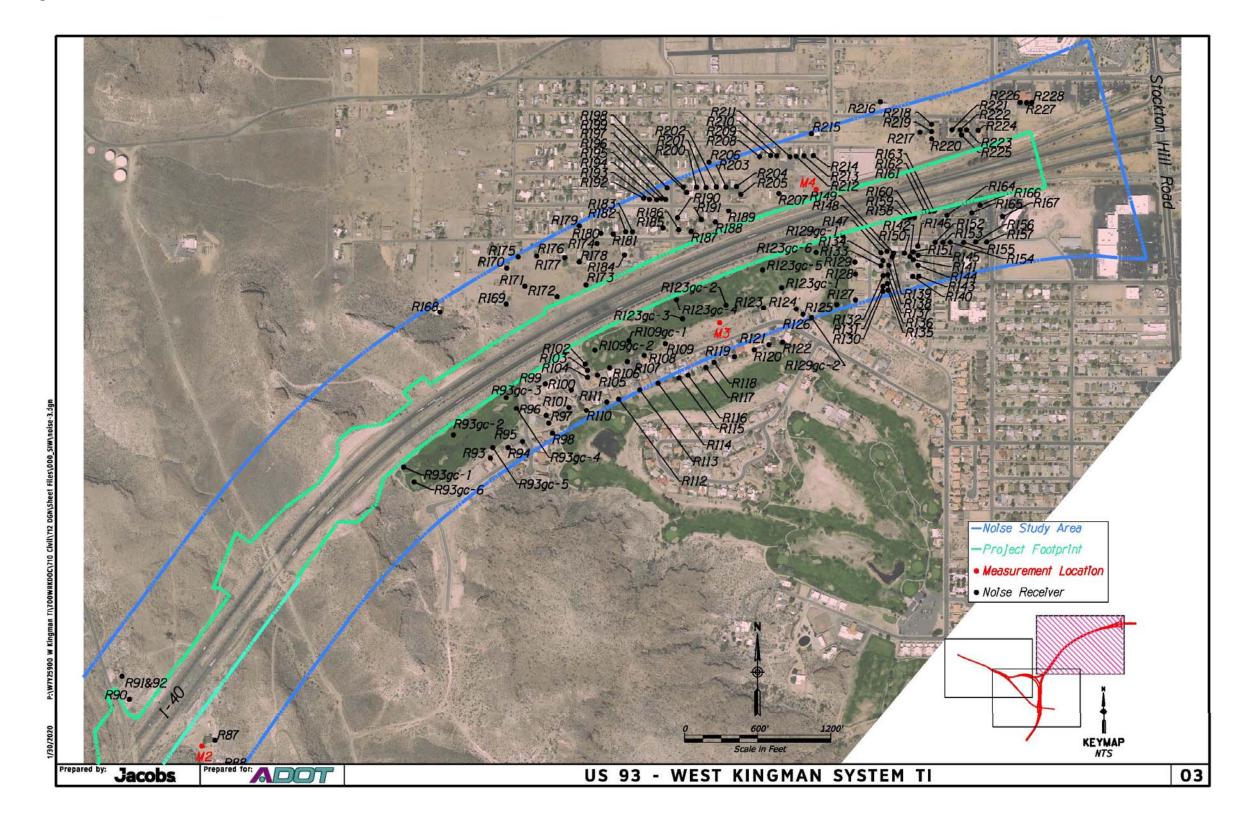
Figure 4. Noise Receivers



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Figure 4. Noise Receivers



Short-term noise level monitoring was conducted within the project limits on July 9, 2019. Two 15-minute measurements were taken under meteorologically acceptable conditions, with winds less than 12 mph and dry pavement at six locations representing each of the evaluated Activity Categories (B and G). If a variation of 3 or dBA or more was recorded for the first two measurements, additional measurements were taken until consecutive measurements were within the 3 dBA tolerance. Measurements were recorded with a Larson Davis Model 820 Class I integrating sound level meter (SLM). The SLM was calibrated prior to each measurement with a Larson Davis Model CAL200.² The measured noise level ranged from 49 dBA to 69 dBA. **Figure 4** shows the location of the noise level monitoring sites (in red), and **Appendix B** includes the noise measurement data sheets.

Background Noise Consideration

Any noise source contributing to the noise levels at a receptor, other than observed traffic noise, must be identified and captured in the TNM model, for instance other major roadway sources such as the two major cross-streets (Beale Street and Stockton Hill Road) in the project area, for the modeled receiver representing that location. Additional noise sources in the study area include train traffic and flights out of the Kingman Municipal Airport. The Atchison Topeka (A-T) rail line runs parallel to I-40 and Route 66 approaching Beale Street from the south where it loops east, crossing over north 2nd Street to the Kingman Railroad Depot located at 400 E. Andy Devine. It then continues to the east where the eastbound and westbound tracks split at south 6th Street and traverse around residential and recreational land uses (baseball fields) before turning to the northeast and parallel to Andy Devine Avenue. The following train activity data were refrenced from online sources³:

- 100 daily trains including two trips by the Amtrak Southwest Chief
- Assume 2 engines per train, 40 mph operational speed
- Assume daylight hours from 7 a.m. to 10 p.m., nighttime hours from 10 p.m. to 7 a.m. per Federal Transit Administration (FTA) guidelines
- Assume 4.17 events/hour evenly spaced throught the day

One location was evaluated for background contributions for train noise the FTA Noise Impact Assessment Spreadsheet v. 1/29/2019 (FTA spreadsheet). Receiver R39 (Figure 4, Detail 01) is an outdoor pool at the Motel 6 located on the south side of Beale Street, west of Grandview Avenue and approximately 840 feet west of the wetbound train tracks. Based on the above parameters and a modeled existing peak hour noise level of 59 dBA, train activitiy is estimated to contribute

² A valid calibration certificate is on file with the ADOT EP Noise and Air Team at the time of measurements, in line with ADOT NAR and *Instruction on Determination of Existing Noise Levels and Noise Measurement Data Form*.

³ Lacking specific train data, two online sources were research to provide an estimate of train activity in the project area; *Follow the Tracks to Kingman Arizona*, available at http://kingmanarizonatrains.com/train-viewing-area.htm and Southwest Chief Train Schedule available at https://www.amtrak.com/content/dam/projects/dotcom/english/public/documents/timetables/Southwest-Chief-Schedule-110319.pdf

44 dBA to the ambient noise environment at this receptor during dayttime hours and 44 dBA during nighttime hours. The contribution of train noise at this locations is 1 dBA; therefore, train noise was not considered further in the analysis of project-related peak hour noise impacts. Calculations sheets from the FTA spreadsheet are included in **Appendix C**.

The Kingman Municipal Airport is located east of I-40 and approximately 5 miles northeast of the project area. **Appendix** noise contour available D shows a at http://www.re.state.az.us/AirportMaps/Public Airports/Kingman Airport Noise&Traffic.pdf that was developed for the airport (Kingman Airport, 2006). The 65 Ldn and 70 Ldn noise contours are contained well within the aiport boundaries. Per 14 CFR Part 150, Appendix A Table 1, the 65 Ldn contour is the threshold for residential land uses and a 70 Ldn is the threshold of compatibility for outdoor recreation uses. Because the airport is located approximately five miles northeast of the project area and the residential and recreational use impact threshold are contained well within its boundaries, noise from the Kingman Airport were not considered further in this analysis.

Traffic Noise Model - Validation

For the purpose of validation of the FHWA TNM, the noise level measurements taken are representative of free-flow conditions, without traffic controls as much a practicable, away from sound reflective objects (warehouses, parked trucks, privacy walls etc.), without being influenced by other noise sources (aircrafts, lawn mowers, engines running, running water, loud insects, birds, animals), and with a clear view to the roadway.

To ensure that the noise model used to predict traffic noise impacts accurately reflects the sound levels in the noise study area, a model was constructed using the same traffic volumes, speed, and vehicle types that were present during the sound level measurements. Modeled values must be within ±3.0 dBA of the measured levels for the model to be validated.

Validated FHWA TNM runs were used to incorporate features of the topographic and built environment necessary to accurately predict both existing and future $L_{eq(h)}$ peak hour traffic noise levels. Noise from sources other than traffic is not captured in the model and when non-traffic noise is present, such as aircraft/railroad/industrial facility/playground noise, TNM will under predict the actual noise level. Conversely, the noise reducing effect of alternative pavement types, such as asphalt rubber friction course (ARFC) or rubberized asphalt, are not captured in the model and when present TNM can over predict the actual noise level. To create the model, design files outlining major roadways, topographical features, and sensitive receptors were imported into the TNM model as background features and the corresponding traffic volumes were entered manually. The measured and modeled noise levels are provided in the **Table 3** on the next page.

Monitoring Location (Receiver)	Activity Category	Land Use Description	Measured Level	Modeled Noise Level	Model Variation
			dBA	dBA	dBA
M1	G	Undeveloped Parcel	59.1	65.0 (60.2) ¹	+5.9 (+1.1) ¹
M1a	В	Residential Adjacent	58.9	61.1 (56.3)	+2.2 (-2.6) ¹
M2	В	Residential Adjacent	59.5	60.9 (56.1)	+1.4 (-3.4)1
M3	G	Undeveloped Parcel	58.1	61.5 (56.7)	+3.4 (-1.4)1
M4	G	Undeveloped Parcel	60.7	64.3 (59.5) ¹	+3.6 (-1.2)1
M5	В	Residential Adjacent	58.5	58.7 ²	+0.2
M6	В	Residential Adjacent	57.2	n/a²	n/a

Table 3. Model Calibration of Measured Noise Levels

- 1. Numbers in parentheses represent the potential noise reduction from the rubberized asphalt surface of the I-40 in the project area with the exception of the overpasses at Beale Street and Stockton Hill Road.
- 2. The primary traffic noise source at measurement locations M5 and M6 are existing Beale Street, which does not have a rubberized asphalt surface. In addition, traffic counts were not recorded at M6.

A comparison of measured to modeled noise levels assuming a loose soil condition still yields a substantial (3 dBA+) variation at three locations (M1, M3 and M4). A hard soil assumption increases the disparity. However, consultation with project design engineers indicates that I-40 within the project limits has an ARFC overlay. The *Arizona Quiet Pavement Pilot Program: Comprehensive Report* (ADOT, 2018) indicates that an average noise reduction of 4.8 dBA for near field, wayside (50-feet from the source), and neighborhood locations⁴. Accounting for this reduction, better agreement was achieved between measured and modeled levels at these locations, with slight over-adjustment at M2. Therefore, the loose soil condition was assumed for all modeling scenarios.

PREDICTED PEAK HOUR NOISE LEVELS

Traffic noise analysis predictions rely on project specific traffic data as listed below and which pertains to all lanes including, general purpose, ramps, High Occupancy Vehicle, Traffic Interchange, and roundabouts, at Level of Service (LOS) C and on other highway influenced infrastructure that may not be considered inconsequential to increasing noise levels within project area.

• Traffic volumes, with lateral distribution (per lane).

⁴ Neighborhood (Site 3C) locations in the study were located an average of 245 feet from the traffic noise source behind a neighborhood perimeter wall or backyard privacy wall. An average 11.6 dBA noise reduction was recorded, which included an assumed 5 dBA for the wall, or a net 6.5 dBA without a wall.

- Vehicle type, vehicle distribution of automobiles, medium trucks, heavy trucks, busses and motorcycles with particular attention to percentage of heavy trucks with lateral distribution (per lane).
- Speed of traffic (per lane)

When predicting noise levels for the design year, a 'worst-case' approach is used, wherein the traffic characteristics that produce the worst traffic noise impact. In general, this should reflect LOS C traffic conditions during the peak noise hour with traffic moving at five miles per hour above the posted speed limit. If future traffic volumes are less than maximum LOS C volumes, future traffic volumes will be utilized. If no other information is available, the peak hourly volume should be 10% of the predicted Annual average daily traffic (AADT), with factors K, D, and T included in the analysis and with lateral lane across the travel lanes of a multiple-lane highway. An exception to worst-case approach is pavement type, as all TNM-noise level predictions must utilize "average" pavement type unless, FHWA approval to use a different pavement type has been obtained.

Roadway Geometry & Topographic Data and Ground Type

The roadway geometry data used for the noise modeling effort, such as roadway and lane width, horizontal and vertical coordinates, were based on the electronic roadway geometry data and 30% design plans using MicroStation © (Jacobs, 2020). Aerial photographs were extracted from Google EarthTM and orthorectified to the MicroStation © roadway coordinates (Google, 2020). Terrain lines determine the elevation of sound propagation interfering feature between source and the noise receiver. Ground type for modeling purposes is determined as loose soil. One, two and three-lane cross sections were modeled with one representative roadway in each direction for all roadway segments.

Traffic Volumes and Mix

Different vehicle types have different noise emission levels, with trucks producing higher noise levels than passenger automobiles. Furthermore, trucks with higher cargo weight capacity produce higher noise levels than trucks of lower cargo weight capacity. Vehicles are categorized as follows:

- Automobiles are categorized as vehicles with two axles and four wheels designed primarily for passenger or cargo (light trucks) transportation. Generally, the gross weight of an automobile is less than 10,000 pounds.
- Medium trucks are categorized as vehicles having two axles. Generally, the gross weight of a medium truck is greater than 10,000 pounds but less than 26,400 pounds.
- Heavy trucks are categorized as vehicles having three or more axles and designed for the transportation of cargo. Generally, the gross weight of a heavy truck is greater than 26,400 pounds.

I-40 is the dominant source of traffic in the study area. At the I-40/Beale Street service interchange the northbound peak hour on I-40 typically occurs Friday afternoon between 12:00 and 1:00 pm, as the traffic heads from Phoenix to Las Vegas. The southbound peak hour typically occurs on Sunday afternoon between 12:30 p.m. and 1:30 p.m. as the traffic returns from Las Vegas to Phoenix. Friday volumes are higher than Sunday volumes; therefore, Friday afternoon was selected as the design peak hour for the traffic analysis (ADOT, 2020).

Modeled roadway segments include I-40 beginning south of Beale Street at MP 48.32 north to Stockton Hill Road at MP 51.75, Beale Street, Stockton Hill Road, and US 93 beginning west of I-40 at MP 69.60 east to the I-40/Beale Street service interchange to MP 71.00. Peak hour volumes from the traffic study for the existing and Build Alternative are presented in **Appendix E**. For the No Build Alternative, existing peak hour volumes were projected to the design year 2042 using a 2.3% annual growth factor identified in the traffic study. LOS C volumes referenced in the *Highway Capacity Manual, Sixth Edition: A Guide for Multimodal Mobility Analysis* (Transportation Research Board, 2016), were used for all scenarios where exceeded by the peak hour volumes.

The following truck percentages for the modeled roadway segments within the study area are based on average annual daily traffic volume data reported in the ADOT *Highway Performance Monitoring System (HPMS) Locations Report* (ADOT, 2016):

- I-40 south of Beale Street (includes EB/WB on-ramps @ Beale Street): 42.8%
- I-40 north of Beale Street (includes EB/WB on-ramps @ Stockton Hill Road, EB/WB off-ramps @ Stockton Hill Road and Beale Street): 30.2%
- I-40 WB to US 93 WB (Build Alternative Ramp WN): 30.2%
- US 93 EB to I-40 EB (Build Alternative Ramp SE): 30.2%
- I-40 EB to US 93 WB (Build Alternative Ramp EN): 30.2%
- US 93 EB to I-40 WB (Build Alternative Ramp SW): 30.2%
- US 93 (Beale Street) between State Route 68 and I-40: 20.5%
- Stockton Hill Road: 10%⁵

Percentages assigned to medium vs. heavy trucks were multiplied by the generally observed ration of medium to heavy truck counts recorded during the noise measurement intervals, which are generally 1-2% medium trucks and 18-23% heavy trucks.

Vehicle Speed

The modeled vehicle speeds are as follows:

Cars and medium truck - 5 mph above posted speed, or 80 mph on existing and future
 I-40, 60 mph on existing and future US 93 and future Build Alternative directional

⁵ A 10% truck volume on Stockton Hill Road was assumed lacking data for this road per the ADOT NAR (ADOT, 2017).

ramps, 50 mph for service interchange on ramps, and 40 mph for Stockton Hill Road and Beale Street

- Heavy trucks posted speed (5 mph less than cars) for these segments
- Traffic signals within the project limits were modeled per Final Report on Project 25-34 Supplemental Guidance on the Application of FHWA's TNM – Appendix B Signalized Interchanges, Intersections and Roundabouts guidelines (Transportation Research Board, 2014).

Atmospheric Variables

Noise level is affected by temperature and humidity. For noise modeling purposes, FHWA recommends the default values for the temperature of 68 degrees Fahrenheit and the humidity of 50 percent.

Receptor and Receiver Locations

The ADOT NAR defines a "receptor" as a discrete or representative location of a noise sensitive area(s) for any of the land uses listed in **Table 2**. The "receiver" is defined as a location used in noise modeling to represent the measured and predicted noise level at a particular point. The noise-sensitive receptors are located in the backyard or common outdoor areas of Category B residential properties. Placement of receivers for Category C, D, E and G land uses follow ADOT NAR guidelines.

Shielding Effects

TNM 2.5 can account for the noise shielding effects created by existing noise barriers, privacy walls, buildings, and terrain changes that are an obstruction between noise sources and receptors. Neighborhood privacy walls were modeled as barriers, while large buildings and the second and third row of homes in residential areas were modeled as building rows. Rocky outcroppings and cut-and-fill slopes and corresponding elevation changes were modeled as terrain lines. For the Build alternative, jersey barriers were modeled at 26-inches at inside/outside roadway shoulders and 36-inches in the median where indicated in the roadway design plans.

Based on the assumptions stated in this report, FHWA TNM 2.5 predicts noise levels along the project route in the design year after construction of the project has occurred. Actual noise levels in the future may differ somewhat due to a number of factors outside the scope of this modeling effort.

This analysis determines the traffic noise impacts based upon the FHWA NAC, which is referred to in ADOT's NAR. The FHWA NAC specify an allowable traffic noise level for different categories of land use and activities. Homes, churches, schools, and parks are classified in Categories B and C, and the noise abatement criteria for these categories is 67 dBA hourly equivalent sound level $(L_{eq(h)})$. In the absence of traffic noise impacts, the consideration of noise abatement measures is not warranted.

Noise Impact Evaluation Summary

Table 4 shows the list of receivers with predicted future noise levels. Noise levels formatted in *italics* meet or exceed the ADOT approach criteria of the FHWA NAC at the respective receiver. For receivers representing 4(f) resources, **bold italicized** values represent an approach or exceedance of the Category C NAC as well as a 3 dBA or more increase above No-Build projected peak hour noise levels. This information is included to inform the evaluation of 4(f) properties in the EA. For the purposes of this noise study, only the Category C NAC has been considered in the evaluation of impacts and noise mitigation for these properties⁶.

Table 4. Peak Hour Noise Levels

Receiver	Activity	NAC¹	No. of	Description	Existing	No Build	Built Alt.	Mitigation	
No.	Category	IUAC	Receptors	Description	(2019)	(2042)	(2042)	Considered	
	Fort Beale RV Park (Figure 4, Detail 01)								
R1	Е	71	2	Pool Area	70	71	71	No -	
	_		_					Visibility	
R2	Е	71	5	RV Stall	68	69	69	No	
R3	Е	71	4	RV Stall	65	67	67	No	
R4	Е	71	4	RV Stall	61	63	62	No	
R5	E	71	4	RV Stall	66	68	68	No	
R6	E	71	4	RV Stall	64	66	66	No	
R7	E	71	4	RV Stall	63	65	65	No	
R8	Е	71	5	RV Stall	68	70	71	No -	
								Visibility	
R9	Е	71	5	RV Stall	64	66	67	No	
R10	E	71	4	RV Stall	62	64	65	No	
R11	Е	71	3	RV Stall	62	64	64	No	
			Positive	e Alternative Cam	pus (school)				
R12	С	66	3	Picnic Table	62	64	64	No	
R13	D	52	3	Bldg. Facade	62(42) ¹	44	44	No	
R14	D	52	3	Bldg. Facade	62(41) ¹	43	43	No	
R15	D	52	3	Bldg. Facade	63(43) ¹	45	45	No	
R16	D	52	3	Bldg. Facade	63(43) ¹	45	45	No	
R17	D	52	3	Bldg. Facade	62(42) ¹	44	44	No	
				City Park Additi	on				
R18	В	66	1	SFH	60	62	61	No	
R19	В	66	1	SFH	60	62	61	No	
R20	В	66	1	SFH	60	62	62	No	
R21	В	66	1	SFH	61	63	62	No	
				Arizona Inn					
R22	E	71	1	Motel	61	63	63	No	
R23	Е	71	1	Motel	63	65	65	No	

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⁶ A 3 dBA increase in peak hour noise levels above the No-Build scenario is one of the factors considered when determining project's constructive use of a Section 4(f) property per 23 CFR 774.15. This information is provided here to inform the 4(f) evaluation in the EA.

Receiver	Activity		No. of		Existing	No Build	Built Alt.	Mitigation	
No.	Category	NAC ¹	Receptors	Description	(2019)	(2042)	(2042)	Considered	
			Arizo	na Inn (Figure 4,	Detail 01)				
								No -	
R24	E	71	1	Motel	69	71	71	Access	
								Issues	
	City Park Addition								
R25	В	66	1	SFH	59	61	61	No	
R26	В	66	1	SFH	59	61	61	No	
R27	В	66	1	SFH	59	61	61	No	
R28	В	66	1	SFH	59	61	61	No	
R29	В	66	1	SFH	59	61	61	No	
R30	В	66	1	SFH	59	61	61	No	
R31	В	66	1	SFH	59	61	61	No	
R32	В	66	1	SFH	59	61	61	No	
R33	В	66	1	SFH	59	61	61	No	
R34	В	66	1	SFH	59	61	61	No	
R35	В	66	1	SFH	59	61	61	No	
				otel 6 (Figure 4, De					
R36	E	71	3	Bldg. Perim	59	61	61	No	
R37	Е	71	3	Bldg. Perim	61	63	63	No	
R38	E	71	3	Bldg. Perim	69	72	72	No, Access Issues	
R39	E	71	2	Pool Area	59	61	61	No	
1.00				Vista #1 (Figure 4			<u> </u>		
R40	В	66	1	SFH	67	69	73	Yes	
R41	В	66	1	SFH	65	67	69	Yes	
R42	В	66	1	SFH	65	66	67	Yes	
R43	В	66	1	SFH	63	65	66	Yes	
R44	В	66	1	SFH	63	64	65	Yes	
R45	В	66	1	SFH	62	64	64	No	
R46	В	66	1	SFH	61	63	63	No	
R47	В	66	1	SFH	67	69	72	Yes	
R48	В	66	1	SFH	66	68	70	Yes	
R49	В	66	1	SFH	65	67	69	Yes	
R50	В	66	1	SFH	65	66	67	Yes	
R51	В	66	1	SFH	64	66	66	Yes	
R52	В	66	1	SFH	63	65	65	No	
R53	В	66	1	SFH	62	64	64	No	
R54	В	66	1	SFH	67	69	69	Yes	
R55	В	66	1	SFH	63	65	65	No	
R56	В	66	1	SFH	62	64	64	No	
R57	В	66	1	SFH	62	64	63	No	
R58	В	66	1	SFH	67	69	69	Yes	
R59	В	66	1	SFH	64	65	66	Yes	
R60	В	66	1	SFH	63	65	65	No	
			Stowel	Addition (Figure	4, Detail 01)				
R61	В	66	1	SFH	60	62	61	No	

Receiver	Activity		No. of		Existing	No Build	Built Alt.	Mitigation
No.	Category	NAC ¹	Receptors	Description	(2019)	(2042)	(2042)	Considered
			Monte	Vista #1 (Figure 4	, Detail 01)			
R62	В	66	1	SFH	65	67	65	No
R63	В	66	1	SFH	65	66	64	No
R64	В	66	1	SFH	64	66	63	No
R65	В	66	1	SFH	65	67	64	No
R66	В	66	1	SFH	69	71	65	No
			Stowell	Addition (Figure	4, Detail 01)			
R67	В	66	1	SFH	60	62	60	No
R68	В	66	1	SFH	60	61	60	No
R69	В	66	1	SFH	60	62	59	No
R70	В	66	1	SFH	61	62	59	No
			Longvie	w Addition (Figure	4, Detail 01)		
R71	В	66	1	SFH	64	66	61	No
R72	В	66	1	SFH	63	65	61	No
R73	В	66	1	SFH	62	64	60	No
R74	В	66	1	SFH	63	65	61	No
R75	В	66	1	SFH	67	69	65	No
R76	В	66	1	SFH	65	66	63	No
R77	В	66	1	SFH	64	65	63	No
R78	В	66	1	SFH	67	69	67	Yes
R79	В	66	1	SFH	65	67	65	No
R80	В	66	1	SFH	66	67	66	Yes
R81	В	66	1	SFH	66	67	66	Yes
R82	В	66	1	SFH	67	68	66	Yes
R83	В	66	1	SFH	67	68	67	Yes
			Unnamed	Subdivision (Figu		-		
R84	В	66	1	SFH	67	69	67	Yes
R85	В	66	1	SFH	68	69	68	Yes
R86	В	66	1	SFH	70	71	69	Yes
R87	В	66	1	SFH	65	66	65	No
R88	В	66	1	MH	66	67	67	Yes
R89	В	66	1	SFH	64	66	65	No
R90	В	66	1	MH	72	73	71	Yes
R91	В	66	1	SFH	72	73	73	Yes
R92	В	66	1	SFH (2nd Story)	73	74	73	Yes
			Country Club	Canyon Estates (F	igure 4, Deta	ail 03)		
R93	В	66	1	SFH	65	66	69	Yes
			Cerbat Cliff	s Golf Course (Fig	ure 4, Detail	03)		
R93gc-1	С	66	5	Recreation	76	<i>77</i>	79	Yes
R93gc-2	С	66	5	Recreation	70	71	74	Yes
R93gc-3	С	66	5	Recreation	72	73	75	Yes
R93gc-4	С	66	5	Recreation	70	71	74	Yes
R93gc-5	С	66	5	Recreation	68	69	71	Yes
R93gc-6	С	66	5	Recreation	67	69	71	Yes
	T		Country Club	Canyon Estates (F	1		T	1
R94	В	66	1	SFH	64	66	68	Yes

Receiver	Activity		No. of		Existing	No Build	Built Alt.	Mitigation
No.	Category	NAC ¹	Receptors	Description	(2019)	(2042)	(2042)	Considered
	T		Country Club	Canyon Estates (F	_		T	,
R95	В	66	1	SFH	64	65	68	Yes
R96	В	66	1	SFH	67	69	71	Yes
R97	В	66	1	SFH	66	68	70	Yes
R98	В	66	1	SFH	64	66	68	Yes
R99	В	66	1	SFH	70	72	73	Yes
R100	В	66	1	SFH	68	70	72	Yes
R101	В	66	1	SFH	67	68	71	Yes
R102	В	66	1	SFH	71	72	74	Yes
R103	В	66	1	SFH	70	71	73	Yes
R104	В	66	1	SFH	69	70	72	Yes
R105	В	66	1	SFH	68	70	72	Yes
R106	В	66	2	SFH	69	70	72	Yes
R107	В	66	2	SFH	68	70	72	Yes
R108	В	66	2	SFH	68	69	71	Yes
R109	В	66	1	SFH	68	69	71	Yes
				4(f) Recreational				1
R109gc-1	С	66	10	Recreation	73	74	77	Yes
R109gc-2	С	66	10	Recreation	70	72	73	Yes
			Country Club	Canyon Estates (F	igure 4, Deta	ail 03)		
R110	В	66	2	SFH	66	67	69	Yes
R111	В	66	1	SFH	65	66	68	Yes
R112	В	66	2	SFH	63	65	66	Yes
R113	В	66	2	SFH	62	63	64	No
R114	В	66	2	SFH	63	64	65	No
R115	В	66	1	SFH	64	65	67	Yes
R116	В	66	2	SFH	64	65	67	Yes
R117	В	66	1	SFH	63	64	65	No
R118	В	66	2	SFH	63	64	65	No
R119	В	66	2	SFH	63	64	66	Yes
R120	В	66	2	SFH	63	64	65	No
R121	В	66	1	SFH	62	64	64	No
	T	1	Kingman Golf	Course Estates (F	-			1
R122	В	66	1	SFH	63	64	65	No
	T			rbat Country Club				1
R123	В	66	3	SFH	66	67	68	Yes
		1		4(f) Recreational	· ·		· · · · · · · · · · · · · · · · · · ·	1
R123gc-1	С	66	6	Recreation	70	71	73	Yes
R123gc-2	С	66	6	Recreation	70	71	72	Yes
R123gc-3	С	66	6	Recreation	70	71	73	Yes
R123gc-4	С	66	6	Recreation	77	78	79	Yes
R123gc-5	С	66	6	Recreation	73	75	76	Yes
R123gc-6	С	66	6	Recreation	76	78	79	Yes
	T			ry Club Estates (F	_	•		1
R124	В	66	1	SFH	65	67	68	Yes
R125	В	66	1	SFH	65	66	67	Yes

Receiver	Activity		No. of		Existing	No Build	Built Alt.	Mitigation
No.	Category	NAC ¹	Receptors	Description	(2019)	(2042)	(2042)	Considered
1101	category	10.10	•	try Club Estates (F		•	(20.2)	Constacted
R126	В	66	1	SFH	61	62	63	No
				Country Club Ma	nor	<u> </u>		1.0
R127	В	66	1	SFH	61	63	64	No
R128	В	66	1	SFH	67	69	70	Yes
R129	В	66	1	SFH	70	72	74	Yes
	С	erbat Clif	fs Golf Course,	4(f) Recreational	Resource (Fi	igure 4, Detai	01)	I
R129gc-1	С	66	6	Recreation	77	79	80	Yes
R129gc-2	С	66	6	Recreation	64	66	67	Yes
			Country	Club Manor (Figur	e 4, Detail 03	3)		
R130	В	66	1	SFH	64	65	66	Yes
R131	В	66	1	SFH	64	66	67	Yes
R132	В	66	1	SFH	65	67	68	Yes
R133	В	66	1	SFH	67	69	70	Yes
R134	В	66	1	SFH	67	69	70	Yes
R135	В	66	1	SFH	62	64	65	No
R136	В	66	1	SFH	64	66	67	Yes
R137	В	66	1	SFH	65	67	68	Yes
R138	В	66	1	SFH	67	68	69	Yes
R139	В	66	1	SFH	67	69	70	Yes
R140	В	66	1	SFH	60	62	62	No
R141	В	66	1	SFH	64	66	66	Yes
R142	В	66	1	SFH	64	66	66	Yes
R143	В	66	1	SFH	65	67	67	Yes
R144	В	66	1	SFH	65	67	67	Yes
R145	В	66	1	SFH	67	69	70	Yes
R146	В	66	1	SFH	68	70	71	Yes
R147	В	66	1	SFH	68	70	77	Yes
R148	В	66	1	SFH	68	70	71	Yes
R149	В	66	1	SFH	68	70	71	Yes
R150	В	66	1	SFH	67	69	70	Yes
R151	В	66	1	SFH	66	68	69	Yes
		Ga	ardens at Kingr	nan Assisted Livin	g (Figure 4, [Detail 03)		
R152	С	66	2	Assisted Living	69	71	72	Yes
R153	С	66	2	Assisted Living	69	71	71	Yes
R154	С	66	2	Assisted Living	68	70	71	Yes
	T			Rehab & Care Cen		i ,	T	
R155	С	66	5	Assisted Living	67	69	70	Yes
R156	С	66	5	Assisted Living	67	69	69	Yes
R157	С	66	5	Assisted Living	67	69	70	Yes
	1		Helen's Plac	e Adult Living (Fig	ure 4, Detai	03)	I	T
R158	Е	71	1	Office Bldg.	79	81	81	No Outdoor
		-		Facade				Use
R159	E	71	1	Office Bldg.	78	80	81	No Outdoor
		-		Facade				Use
R160	Е	71	1	Office Bldg.	78	80	80	No Outdoor
				Facade				Use

Receiver	Activity		No. of		Existing	No Build	Built Alt.	Mitigation
No.	Category	NAC1	Receptors	Description	(2019)	(2042)	(2042)	Considered
140.	category	TURCI		ce Adult Living (Fig		<u> </u>	(2042)	considered
R161	С	66	1	Assisted Living	79	81	81	Yes
R162	C	66	1	Assisted Living	79	81	81	Yes
R163	C	66	1	Assisted Living	78	80	80	Yes
RIOS				r for Alzheimer's C			00	163
R164	С	66	4	Assisted Living	75	78	78	Yes
R165	C	66	4	Assisted Living	75	77	77	Yes
R166	C	66	4	Assisted Living	78	80	80	Yes
11200		- 55	·	tes by Hilton (Figu			- 55	
R167	E	71	2	Hotel Pool	66	68	68	Yes
11207		l		nnamed Neighbor		l .		
R168	В	66	1	МН	66	68	71	Yes
R169	В	66	1	SFH	69	71	74	Yes
R170	В	66	1	MH	64	65	68	Yes
R171	G	-	1	vacant parcel	68	69	71	No
R172	G	_	1	vacant parcel	74	75	76	No
R173	G	_	1	vacant parcel	75	76	78	No
R174	G	_	1	vacant parcel	68	69	71	No
R175	В	66	1	MH	64	65	67	Yes
R176	В	66	1	MH	65	67	69	Yes
R177	В	66	1	SFH	68	69	71	Yes
R178	В	66	1	SFH	69	71	73	Yes
11210	<u>-</u>		Kingman Coun	try Club Addition (1
R179	В	66	1	SFH	64	66	67	Yes
R180	В	66	1	SFH	67	68	70	Yes
R181	В	66	1	SFH	68	69	71	Yes
R182	В	66	1	SFH	68	69	71	Yes
R183	В	66	1	SFH	69	70	72	Yes
R184	В	66	1	SFH	71	72	75	Yes
R185	В	66	3	SFH	70	71	73	Yes
R186	В	66	1	SFH	71	72	74	Yes
R187	G	-	1	vacant parcel	72	73	75	No
R188	В	66	1	SFH	72	74	<i>75</i>	Yes
R189	В	66	1	SFH	71	72	73	Yes
R190	В	66	3	SFH	68	70	71	Yes
R191	В	66	2	SFH	70	72	73	Yes
R192	В	66	3	МН	65	66	67	Yes
R193	В	66	1	МН	65	66	68	Yes
R194	В	66	1	МН	65	67	68	Yes
R195	В	66	1	MH	66	67	68	Yes
R196	В	66	1	MH	66	67	68	Yes
R197	В	66	1	MH	64	66	67	Yes
R198	В	66	1	SFH	66	67	68	Yes
R199	В	66	1	SFH	66	68	69	Yes
R200	В	66	1	MH	66	67	69	Yes
R201	В	66	1	MH	67	68	69	Yes

Receiver	Activity		No. of		Existing	No Build	Built Alt.	Mitigation
No.	Category	NAC ¹	Receptors	Description	(2019)	(2042)	(2042)	Considered
			Kingman Coun	try Club Addition	(Figure 4, De	tail 03)		
R202	В	66	1	MH	67	68	69	Yes
R203	В	66	1	MH	67	69	70	Yes
R204	В	66	1	MH	68	69	70	Yes
R205	В	66	2	MH	69	71	72	Yes
R206	В	66	1	MH	63	64	65	No
R207	В	66	3	MH	72	73	74	Yes
R208	В	66	1	MH	65	67	68	Yes
R209	В	66	1	MH	66	67	68	Yes
R210	В	66	1	MH	66	68	68	Yes
R211	В	66	1	MH	67	68	69	Yes
R212	В	66	1	MH	67	68	69	Yes
R213	В	66	1	MH	67	69	69	Yes
R214	В	66	1	MH	67	69	69	Yes
R215	В	66	1	MH	64	66	66	Yes
R216	В	66	4	Duplex	64	66	66	Yes
R217	В	66	4	Fourplex	69	71	71	Yes
			Cimarron	Apartments (Figu	re 4, Detail 0	3)		
R218	В	66	6	Apartments	66	68	69	Yes
R219	В	66	6	Apartments	68	70	70	Yes
R220	В	66	6	Apartments	70	73	73	Yes
R221	В	66	5	Apartments	70	73	73	Yes
R222	В	66	5	Apartments	70	72	73	Yes
R223	В	66	6	Apartments	71	73	73	Yes
R224	В	66	6	Apartments	71	73	73	Yes
R225	В	66	1	BB Court	71	73	73	Yes
			KRMC U	rgent Care (Figure	4, Detail 03)		
R226	D	52	1	Patient Room	68(48) ¹	69(49) ¹	69(49) ¹	No
R227	D	52	1	Patient Room	68(48) ¹	70(50) ¹	70(50) ¹	No
R228	D	52	1	Patient Room	68(48) ¹	70(50) ¹	70(50) ¹	No
			Residential	Parcels/Unnamed	d Neighborh	ood		
R229	В	66	1	SFH	56	57	63	No
			Camp Be	ale Springs (Figure	e 4, Detail 02	2)		
R229-	С	66	1	Parking area	55	57	58	No
CBS1	C							110
	T		ntial Parcels/U	nnamed Neighbo				1
R230	В	66	1	SFH	55	57	63	No
R231	В	66	1	MH	53	54	69	Yes
R232	В	66	1	SFH	58	60	59	No
	T	•		Metcalfe Acre			T	1
R233	В	66	1	MH	65	66	62	No
R234	В	66	1	SFH	58	59	58	No
	T	•	Kingman Pla	ce Apartments (Fi	gure 4, Deta	-	T	
R235	В	66	1	BB Court	57	59	58	No
R236	В	66	1	Apartment	60	61	60	No
R237	В	66	1	Apartment	57	59	58	No
R238	В	66	1	Apartment	57	58	58	No

Receiver	Activity		No. of		Existing	No Build	Built Alt.	Mitigation			
No.	Category	NAC ¹	Receptors	Description	(2019)	(2042)	(2042)	Considered			
Kingman Place Apartments (Figure 4, Detail 02)											
R239	В	66	1	Gazebo	59	60	59	No			
R240	В	66	1	Gazebo	57	59	58	No			
11240	Ь	00		ate Inn (Figure 4,		39	38	INO			
R241	Е	71	1	Abandoned	62	63	63	No			
R241	E	71	1	Abandoned	61	62	62	No			
R242	E	71	1	Abandoned	62	63	62	No			
K245		/1	Т.	Abandoned	02	03	02	No, Access			
R244	E	71	1	Motel Room	73	73	71	Issues			
R245	E	71	1	Motel Room	70	71	68	No			
R246	E	71	1	Motel Room	72	72	69	No			
Metcalfe Acres (Figure 4, Details 01 & 02)											
R247	В	66	1	SFH	61	62	61	No			
R248	В	66	1	SFH	60	61	60	No			
R249	В	66	1	SFH	60	61	60	No			
R250	В	66	1	SFH	59	60	59	No			
R251	В	66	8	Apartments	58	59	58	No			
R252	В	66	1	SFH	62	63	61	No			
R253	В	66	1	SFH	61	62	60	No			
R254	В	66	1	SFH	59	60	58	No			
R255	В	66	1	SFH	64	65	62	No			
R256	В	66	1	SFH	62	62	60	No			
R257	В	66	1	SFH	60	61	58	No			
R258	В	66	1	SFH	60	62	59	No			
R259	В	66	1	SFH	60	61	58	No			
R260	В	66	1	SFH	61	62	58	No			
R261	В	66	1	SFH	61	62	59	No			
R262	В	66	1	SFH	62	63	60	No			
R263	В	66	1	SFH	62	63	60	No			
R264	В	66	1	SFH	61	62	59	No			
R265	В	66	1	SFH	61	62	59	No			
R266	В	66	1	SFH	61	62	60	No			
R267	В	66	1	SFH	61	63	60	No			
R268	В	66	1	SFH	61	63	61	No			
R269	В	66	1	SFH	62	63	61	No			
R270	В	66	1	SFH	65	66	63	No			
R271	В	66	1	SFH	63	63	60	No			
R272	В	66	1	SFH	62	63	60	No			
R273	В	66	1	SFH	65	66	63	No			
R274	В	66	1	SFH	64	65	62	No			
R275	В	66	1	SFH	68	68	66	Yes			
R276	В	66	1	SFH	64	65	62	No			
R277	В	66	1	SFH	65	67	65	No			
R278	В	66	1	SFH	69	71	71	Yes			
	Monte Vista (Figure 4, Details 01)										
R279	В	66	1	SFH	<i>75</i>	77	73	Yes			

Receiver No.	Activity Category	NAC ¹	No. of Receptors	Description	Existing (2019)	No Build (2042)	Built Alt. (2042)	Mitigation Considered			
Metcalfe Acres (Figure 4, Details 01 & 02)											
R280	В	66	1	SFH	61	62	60	No			
	Camp Beale Monolith Connector (Figure 4, Detail 02)										
R280- CBMC1	С	66	1	Trail	48	50	51	No			
R280- CBMC2	С	66	1	Trail	49	51	51	No			
R280- CBMC3	С	66	1	Trail	53	55	56	No			
R280- CBMC4	С	66	1	Trail	61	63	65	No			
R280- CBMC5	С	66	1	Trail	60	61	63	No			
R280- CBMC6	С	66	1	Trail	56	58	59	No			
	Metcalfe Acres (Figure 4, Details 01 & 02)										
R281	В	66	1	SFH	58	59	58	No			
R282	В	66	1	SFH	66	67	64	No			
R283	В	66	1	SFH	68	69	66	No			
R284	В	66	1	SFH	62	63	61	No			
R285	G	-	1	vacant parcel	69	70	67	No			
R286	G	-	1	vacant parcel	67	67	65	No			
Residential Parcels/Unnamed Neighborhood (Figure 4, Details 01 & 02)											
R287	G	-	1	vacant parcel	65	66	63	No			

Notes: *Italicized* values meet or exceed the ADOT approach of the FHWA NAC for the listed Activity Category. *Italicized bold* values exceed indicates an exceedance of the ADOT approach of the FHWA Activity Category C NAC and a 3 dBA or more increase from No Build to Build peak hour noise level.

1. Interior noise levels assume a 20 dBA IL across a typical building shell with windows and doors closed.

East of I-40, South of Clacks Canyon Road

A total of 86 receivers (R1 to R86) were modeled representing 138 Activity Category B, C, D and E receptors, including the Fort Beale RV Park, Positive Alternative Campus school, Arizona Inn, Motel 6, and the City Park Addition, Monte Vista #1, Stowell Addition, and Longview Addition neighborhoods as well as homes in unnamed residential areas. As shown in **Table 4**, existing, No-Build and Build Alternative peak hour noise levels at the modeled receivers would range from:

Existing: 41 dBA to 70 dBANo-Build: 43 dBA to 72 dBA

Build Alternative: 43 dBA to 73 dBA

For the Build Alternative, exceedances of the Category B NAC are predicted to occur at 17 homes in the Monte Vista #1 and Longview Addition neighborhoods and 3 homes in unnamed residential areas and mitigation evaluation is required.

Impacts are also predicted at one stall and the pool area in the Fort Beale RV Park and outdoor common areas at the Arizona Inn and Motel 6 motels. Traditionally, motels and RV parks do not look favorably to noise walls as those reduce the visual exposure of the properties to travelling public. As the current design is at 30%, there will be a need to update the noise analysis at further stages of the design. Consequently, following the comments from the public, including the owners of the motels and the RV park, further consideration of those properties will be given, in line with ADOT NAR Chapter 2.1. Furthermore, there are access issues to the properties that would prohibit effective mitigation per ADOT feasible requirements.

It is noteworthy that noise levels are predicted to decrease by a decibel or more at R61 – R86 due to the shielding provided by a retaining wall/fill on the outside directional Ramp EN (I-40 EB to US 93 WB) before it crosses I-40 on structure. Increases above existing peak hour noise levels would not trigger additional impacts per the ADOT NAR 15 dBA substantial increase criterion. **Figure 4, Details 01** shows the location of the modeled receivers.

I-40 at Clacks Canyon Road

Six receivers (R87 to R92) were modeled representing six Activity Category B receptors, three on either side of I-40 and north of Clacks Canyon Road. As shown in the **Table 4**, existing, No-Build and Build Alternative peak hour noise levels at the modeled receivers would range from:

Existing: 64 dBA to 73 dBANo-Build: 66 dBA to 74 dBA

Build Alternative: 65 dBA to 73 dBA

For the Build Alternative, an approach or exceedance of the Category B NAC is predicted at four of the six locations; therefore, mitigation evaluation is required. Increases above existing peak hour noise levels would not trigger additional impacts per the ADOT NAR 15 dBA substantial increase criterion. **Figure 4, Details 01 and 03** show the location of the modeled receivers.

East of I-40, south of Stockton Hill Road

A total of 91 receivers (R93 to R167, R93gc-1 to R93gc-6, R109gc-1&2, R123gc-1 to R123gc-6) were modeled representing 211 Activity Category B, C and E receptors. Category B uses include the Country Club Canyon Estates, Cerbat Country Club Estates, Country Club Manor, and Kingman Golf Course Estates neighborhoods. Category C land uses include four assisted living facilities - Gardens at Kingsman Assisted Living Facility, Kingman Gardens Rehab and Care Center, Helen's Place Adult Living, and the Lingenfelter Center for Alzheimer's Care. Category C uses also include the Cerbat Hills Golf Course, which qualifies for Section 4(f) protection. Category E land uses include office space and the Home2Suites hotel. As shown in **Table 4**, existing, No-Build and Build Alternative modeled peak hour noise levels would range from:

Existing: 60 dBA to 79 dBANo-Build: 62 dBA to 81 dBA

Build Alternative: 62 dBA to 81 dBA

For the Build Alternative, an approach or exceedance of the Category B NAC is predicted at 48 homes in each of the four residential neighborhoods in this part of the study area and mitigation evaluation is required. An approach or exceedance of the Category C NAC is predicted at 28 locations including all four assisted living communities and the golf course; therefore, the evaluation of mitigation is required. Additionally, three locations representing the building façade for Helen's Place Adult Living exceed the Category E NAC and don't require consideration for mitigation, although noise reduction benefits for these receivers was included in evaluating feasibleness, reasonableness, and cost-benefit ratios per the ADOT NAR requirements for mitigation at adjacent impacted receivers.

Increases above existing peak hour noise levels would not trigger additional impacts per the ADOT NAR 15 dBA substantial increase criterion. **Figure 4, Detail 03** shows the location of the modeled receivers.

West of I-40, south of Stockton Hill Road

A total of 61 receivers (R168 to R228) were modeled representing 110 Activity Category B, C, D, and G receptors. Category B land uses include the Cimarron Apartments and single-family, multifamily, and mobile homes in the Kingman Country Club Addition and unnamed residential areas. Category C land use includes the basketball court at the Cimarron Apartments. Category D land uses include patient rooms at the KRMC Urgent Care facility and Category G land uses include vacant residential parcels in the Kingman Country Club Addition and unnamed residential areas. As shown in **Table 4**, existing, No-Build and Build Alternative modeled peak hour noise levels would range from:

Existing: 48 dBA to 75 dBANo-Build: 49 dBA to 75 dBA

Build Alternative: 49 dBA to 78 dBA

For the Build Alternative, an approach or exceedance of the Category B NAC is predicted at 51 residential receivers in each of the residential neighborhoods in this part of the study area and mitigation evaluation is required. Exceedance of the Category C NAC is predicted at the Cimarron Apartment basketball court and mitigation evaluation is also required.

Increases above existing peak hour noise levels would not trigger additional impacts per the ADOT NAR 15 dBA substantial increase criterion. **Figure 4, Detail 03** shows the location of the modeled receivers.

West of I-40, north of US 93/Beale Street

A total of 55 receivers (R229 to R279, R229-CBS1, R280-CBMC4 to R280-CBCMC6) were modeled representing 62 Activity Category B, C and E receptors. Category B land uses include the Kingman Place Apartments and single-family, multi-family, and mobile homes in Metcalfe Acres and Monte Vista and in unnamed residential areas. Category C land uses include two gazebos and a basketball court at the Kingman Place Apartments and two recreation areas afforded protection

as Section 4(f) resources - the Camp Beale Monolith Connector and the Camp Beale Springs parking area. As shown in **Table 4**, existing, No-Build and Build Alternative modeled peak hour noise levels would range from:

Existing: 53 dBA to 75 dBANo-Build: 54 dBA to 77 dBA

Build Alternative: 58 dBA to 73 dBA

For the Build Alternative, an approach or exceedance of the Category B NAC for three homes in the Metcalfe Acres neighborhood and one mobile home in an unnamed residential area is predicted and mitigation evaluation is also required. An approach or exceedance of the Category E NAC at the Tri-State Inn motel is predicted; however, mitigation at this location would be impractical due to access issues and were not considered further.

Increases above existing peak hour noise levels would not trigger additional impacts per the ADOT NAR 15 dBA substantial increase criterion. **Figure 4, Details 01 and 02** shows the location of the modeled receivers.

West of I-40, south of US 93/Beale Street

A total of 11 receivers (R280 – R287, R280-CBMC1 to R280-CBMC3) were modeled representing 11 Activity Category B, C and G receptors. Category B land uses include single-family homes in Metcalfe Acres and in an unnamed residential area. Category G land uses include two vacant residential parcels in Metcalfe Acres and a third vacant parcel in an unnamed residential area. Category C land used include three locations on the Camp Beale Monolith Connector trail, which is afforded protection as Section 4(f) resource. As shown in **Table 4**, existing, No-Build and Build Alternative modeled peak hour noise levels would range from:

Existing: 48 dBA to 68 dBANo-Build: 50 dBA to 70 dBA

• Build Alternative: 51 dBA to 66 dBA

For the Build Alternative, no approach or exceedance of the Category B and Category C NAC are predicted at any of the evaluated receivers. Increases above existing peak hour noise levels would not trigger additional impacts per the ADOT NAR 15 dBA substantial increase criterion. **Figure 4, Details 01 and 02** shows the location of the modeled receivers.

CONSIDERATION OF ABATEMENT

ADOT considers mitigation for receivers predicted to be impacted by traffic noise associated with a proposed transportation improvement project. Abatement considerations include acquisition of right-of-way, change in the horizontal or vertical alignment, insulation of Category D land use facilities, traffic management measures and noise barriers. Based on the purpose and need for this project and the design elements that take advantage of separating future freeway segments from existing noise-sensitive land uses, noise barriers are the mitigation measure evaluated in detail for this study.

For a mitigation measure, such as a noise barrier, to be proposed in the project it must meet both feasibility and reasonableness criteria. Pursuant to the 23 CFR 772.13(d)(1), the initial consideration for each abatement measure should be both the engineering and acoustic feasibility factors that determine whether it is possible to design and construct the measure.

As per Chapter 5.1 of ADOT NAR, engineering feasibility factors are:

- Safety, Barrier height, Curvature, and Breaks in barriers
- Topography, Drainage, Utilities
- Maintenance requirements, Access to adjacent properties
- Overall project purpose

As per Chapter 5.2 of ADOT NAR, for a noise abatement measure to be acoustically feasible ADOT requires achievement of at least a 5 dBA highway traffic noise reduction at 50% of impacted receptors. In some instances, the noise level at a particular location may be affected by an alternate noise source such as other roadways/streets, railroads, industrial facilities, and airplane flight paths. In such locations, noise abatement for the proposed transportation project may not be acoustically feasible, since a substantial overall noise reduction cannot be achieved due to other noise sources.

As per Chapter 6 of ADOT NAR, there are three reasonableness factors or "tests" that must collectively be achieved for a noise abatement measure to be deemed reasonable.

These are:

- Viewpoints or Preferences of Property Owners and Residents
- Noise Reduction Design Goal, and
- Cost-effectiveness

Noise barriers should be designed to reduce projected unmitigated noise levels by at least seven dBA for benefited Receptors <u>closest to the transportation facility</u>. To be considered reasonable, at least half of the benefited Receptors in the first row shall achieve this level of noise reduction. The maximum reasonable cost of abatement is \$49,000 per benefited Receptor (cost-per-benefited-Receptor) with barrier costs calculated at \$35 per square foot, \$85 per square foot if constructed on a structure. Any cost of removal of previously built walls, drainage, and other similar construction work shall be included in the cost assessment.

Tables 5 through **10** summarize the effect of proposed noise barriers on impacted receptors in the study area. Only receivers representing impacted noise receptors and those closest to them that would potentially benefit from noise barriers are listed in the tables. The considered barrier locations are shown in **Figure 5**, **Details 01 – 10**.

Figure 5. Noise Barrier Locations

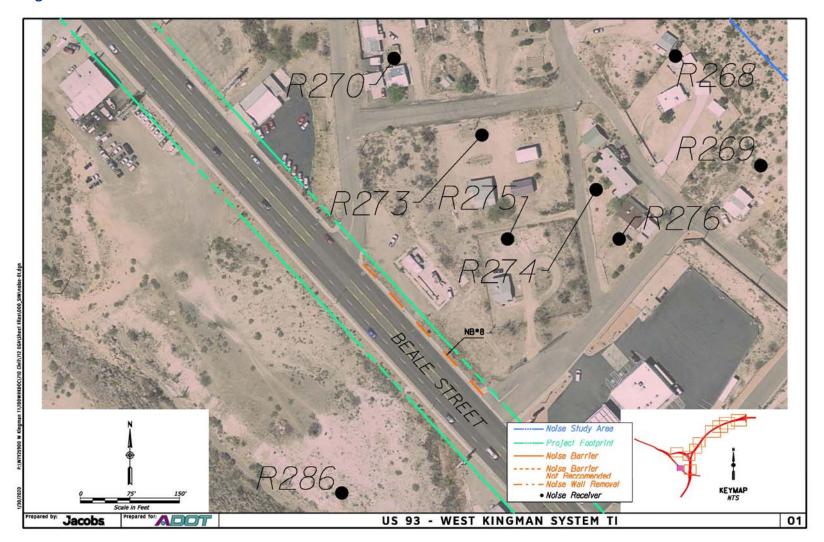


Figure 5. Noise Barrier Locations

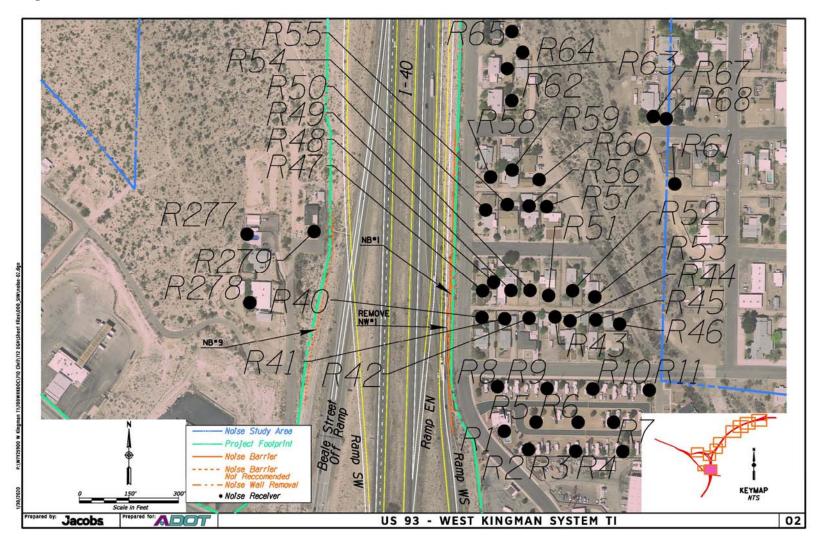


Figure 5. Noise Barrier Locations

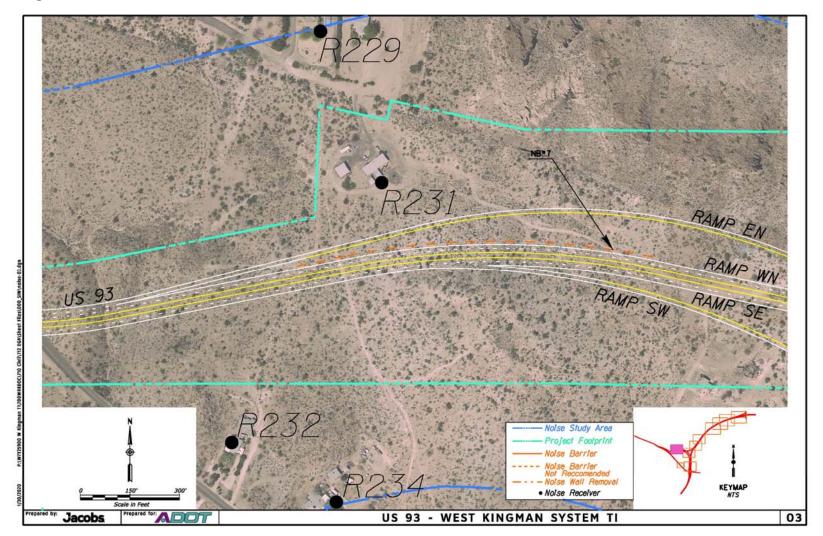


Figure 5. Noise Barrier Locations

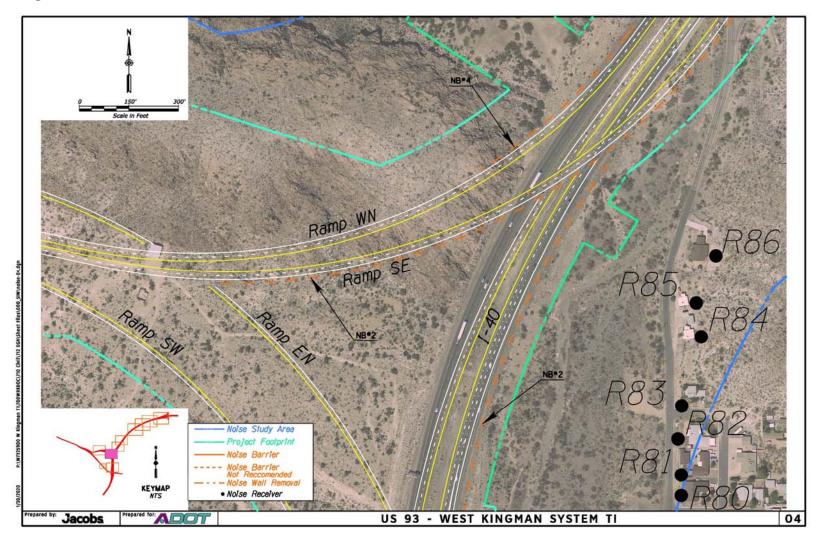


Figure 5. Noise Barrier Locations

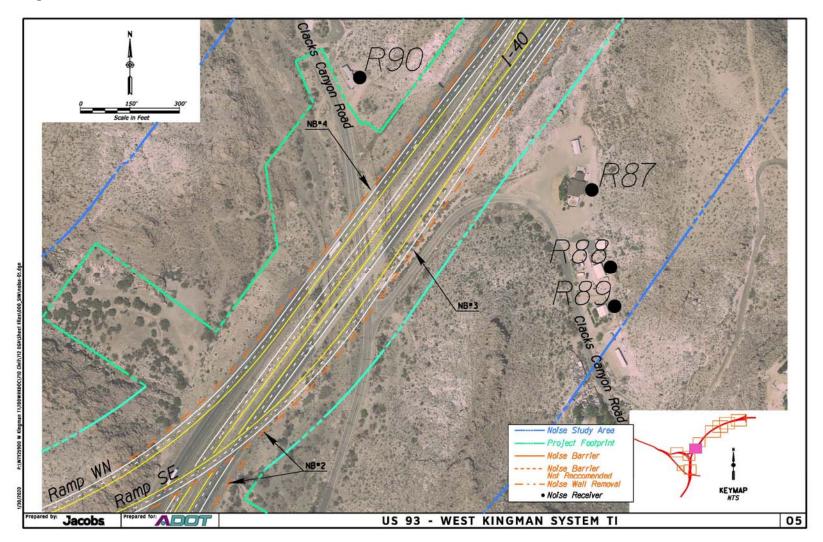


Figure 5. Noise Barrier Locations

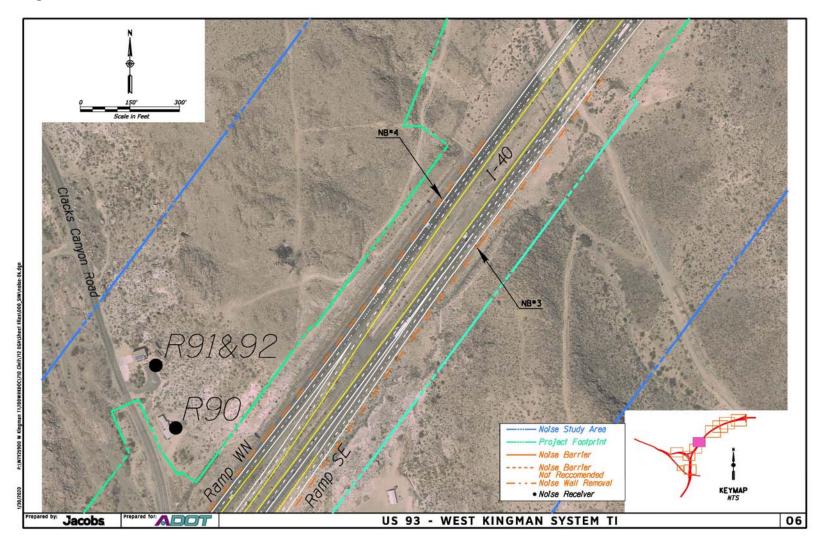


Figure 5. Noise Barrier Locations

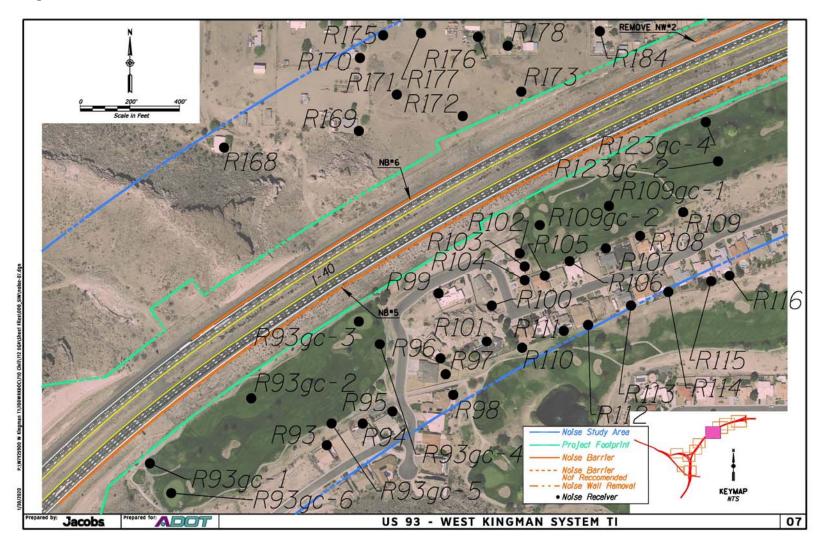


Figure 5. Noise Barrier Locations

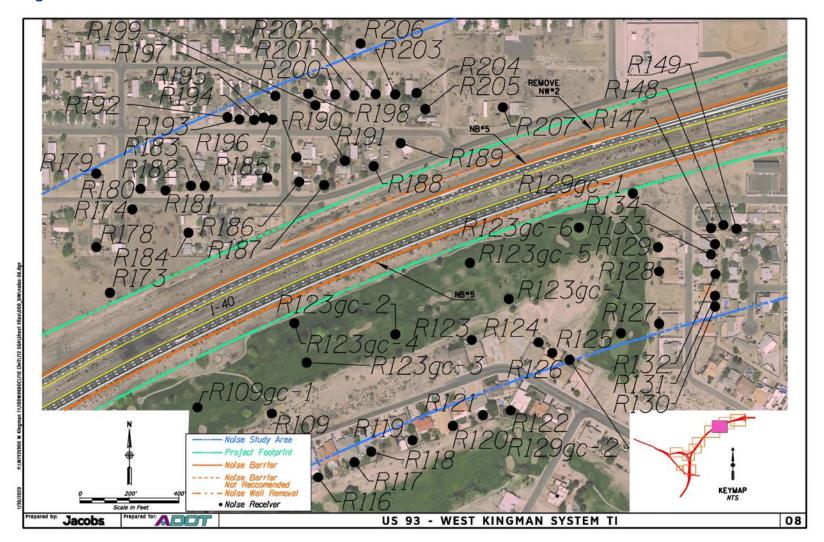


Figure 5. Noise Barrier Locations

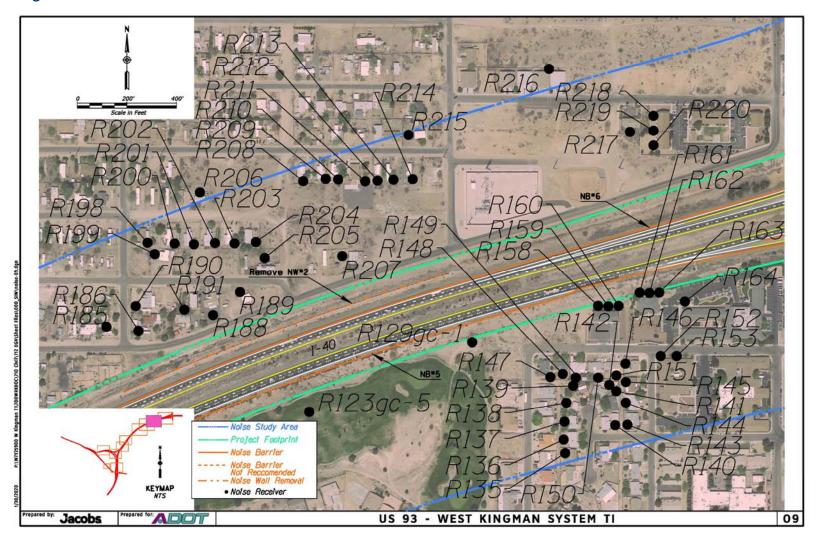
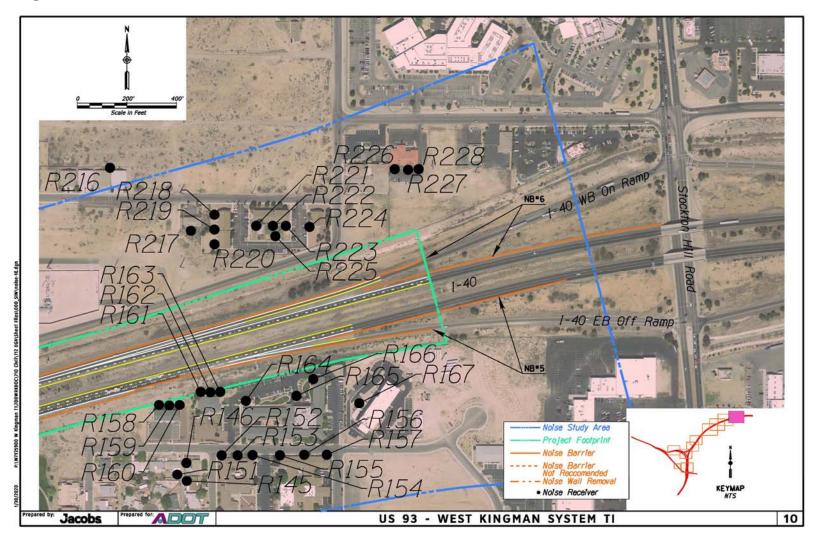


Figure 5. Noise Barrier Locations



East of I-40, South of Clacks Canyon Road

The Build Alternative I-40/US 93 system interchange will replace the existing two-lane I-40 EB onramp from Beale Street with a longer single-lane on-ramp that runs parallel to the new directional ramp I-40 EB to US 93 WB (Ramp EN). The existing noise combination wall/berm (NW#1) located adjacent to the existing I-40 on-ramp would be removed with the new interchange.

Noise Barrier #1 (NB#1) was evaluated to mitigate Build Alternative peak hour noise levels at impacted homes in the Monte Vista #1 neighborhood where peak hour noise impacts are predicted due to the future increase in traffic and removal of NW#1. Figure 5, Detail 02 shows the location of NB#1, which would be located at the outside shoulder of the I-40 EB on-ramp from Beale Street (Ramp WS).

Noise Barrier #2 (NB#2) was evaluated to mitigate Build Alternative peak hour noise levels at impacted homes in the Longview Addition neighborhood. The barrier would be located at the outside shoulder of the I-40 EB on-ramp. **Figure 5**, **Details 04 & 05** shows the location of NB#2, which is a combination of two noise walls, one at the outside should of Ramp WS continuing along the outside should of I-40 EB and the second at the outside should of direction ramp SE.

Table 5 provides an assessment of the effectiveness of these barriers in providing noise benefits (5 dBA or greater noise reduction) and the ADOT NAR design goal of a 7 dBA noise reduction for first row receptors. **Table 11** provides additional design details and a recommendation determination for these barriers.

Table 5. Noise Mitigation Evaluation for 2042 Build Alternative, East of I-40 and South of Clacks Canyon Road

Receiver ID	NO. of Dwelling Units	Unmitigated Noise Level (dB)	Mitigated Noise Level (dBA)	Insertion Loss (dBA)	Benefited Receiver (5 dBA) [Y/N]	1st Row Design Reduction (7 dBA) [Y/N]	Mitigation
	M	onte Vista #1 (Fi	gure 5, Detail 02	2) NAC 66 dE	BA ¹		
R40	1	73	67	5	Υ	N	
R41	1	69	66	4	N	N	
R42	1	67	65	3	N	N	
R43	1	66	63	2	N	N	Noise Barrier #1
R44	1	65	63	2	N	N	See Noise Barrier
R45	1	64	62	1	N	N	Recommendation
R46	1	63	62	1	N	N	Summary
R47	1	72	67	5	Υ	N	Table 10
R48	1	70	66	5	Υ	N	
R49	1	69	65	3	N	N	
R50	1	67	65	3	N	N	
R51	1	66	64	2	N	N	

Receiver ID	NO. of Dwelling Units	Unmitigated Noise Level (dB)	Mitigated Noise Level (dBA)	Insertion Loss (dBA)	Benefited Receiver (5 dBA) [Y/N]	1 st Row Design Reduction (7 dBA) [Y/N]	Mitigation
R52	1	65	63	2	N	N	
	M	onte Vista #1 (Fi	gure 5, Detail 02	2) NAC 66 dF	BA ¹		
R53	1	64	62	2	N	N	Noise Barrier #1
R54	1	69	64	5	Υ	N	
R55	1	65	63	3	N	N	See Noise Barrier
R56	1	64	62	2	N	N	Recommendation
R57	1	63	61	2	N	N	Summary
R58	1	69	66	3	N	N	Table 10
R59	1	66	63	2	N	N	
	Longvi	ew Addition (Fig	ure 5, Detail 04	& 05)) NAC	66 dBA ¹		
R78	1	67	60	7	Υ	Υ	
R79	1	65	59	6	Υ	N	Noise Barrier #2
R80	1	66	60	6	Υ	N	
R81	1	66	60	6	Υ	N	See Noise Barrier
R82	1	66	60	6	Υ	N	Recommendation
R83	1	67	60	7	Υ	Υ	Summary
R84	1	67	61	6	Υ	N	Table 10
R85	1	68	62	6	Υ	N	
R86	1	69	63	6	Υ	N	

I-40 at Clacks Canyon Road

Noise Barrier #3 (NB#3) was evaluated to mitigate Build Alternative peak hour noise levels at impacted homes located along Clacks Canyon Road east of I-40. Figure 5, Details 05 & 06 shows the location of NB#3, which would be located at the outside shoulder of the system interchange directional Ramp SE over Clacks Canyon Road. Noise Barrier #4 (NB#4) was evaluated to mitigate Build Alternative peak hour noise levels at impacted homes located along Clacks Canyon Road west of I-40. Figure 5, Details 04 - 06 shows the location of NB#4, which would be located at the outside shoulder of the system interchange directional WN over Clacks Canyon Road. Table 6 provides an assessment of the effectiveness of this barrier and Table 11 provides additional design details and a recommendation determination.

^{1.} ADOT NAR 1-decibel approach of FHWA Category B NAC.

Table 6. Noise Mitigation Evaluation for 2042 Build Alternative, I-40 @ Clacks Canyon Road

Receiver ID	NO. of Dwelling Units	Unmitigated Noise Level (dBA)	Mitigated Noise Level (dBA)	Insertion Loss (dBA)	Benefited Receiver (5 dBA) [Y/N]	1 st Row Design Goal (7 dBA) [Y/N]	Mitigation Noise Barrier #3
	Reside	ences East of I-40	O (Figure 5, Deta	iil 05) NAC 6	6 dBA ¹		Noise Barrier #3
R87	1	65	60	5	Υ	N	See Noise Barrier
R88	1	67	62	5	Υ	N	Evaluation Summary
R89	1	65	61	4	N	N	Table 10
	Residence	es West of I-40 (F	Figure 5, Details	05 & 06) NA	AC 66 dBA ¹		Noise Barrier #4
R90	1	71	66	5	Υ	N	See Noise Barrier
R91	1	73	72	2	N	N	Evaluation
R92 (2 nd Story)	1	73	72	2	N	N	Summary Table 10

1. ADOT NAR 1-decibel approach of FHWA Category B NAC.

East of I-40, south of Stockton Hill Road

Noise Barrier #5 (NB#5) was evaluated to mitigate Build Alternative peak hour noise levels at impacted Category B, C and E receptors located east of I-40 and south of Stockton Hill Road. Figure 5, Details 07 - 10 shows the location of NB#5, which is comprised of two noise walls. The first would be located at the outside shoulder of the I-40 EB approaching Stockton Hill Road from the west and continuing along the I-40 EB off-ramp. The second would be located inside the I-40 EB off-ramp at Stockton Hill Road at the I-40 EB shoulder approaching the overpass. Table 7 provides an assessment of the effectiveness of this barrier and Table 11 provides additional design details and a recommendation determination.

Table 7. Noise Mitigation Evaluation for 2042 Build Alternative, East of I-40 and South of Stockton Hill Road

Receiver ID	NO. of Dwelling Units	Unmitigated Noise Level (dB)	Mitigated Noise Level (dBA)	Insertion Loss (dBA)	Benefited Receiver (5 dBA) [Y/N]	1 st Row Design Goal (7 dBA) [Y/N]	Mitigation
	Country	Club Canyon Esta	ates (Figure 5, D	etail 07) NA	C 66 dBA ¹		Noise Barrier #5
R93	1	69	60	8	Υ	Υ	See Noise Barrier
R94	1	68	60	8	Y	Υ	Evaluation
R95	1	68	60	8	Y	Υ	Summary
R96	1	71	62	9	Υ	Υ	Table 10

						a ct -	I
						1 st Row	
	NO. of	Hamitian to d	Baitimete d	Insertion	Benefited Receiver	Design Goal	
Receiver	Dwelling	Unmitigated Noise Level	Mitigated Noise Level	Loss	(5 dBA)	(7 dBA)	
ID	Units	(dB)	(dBA)	(dBA)	(3 dBA) [Y/N]	(7 dBA) [Y/N]	Mitigation
טו		ıb Canyon Estate				[1/14]	Wittgation
R97	1	70	61	9	Y	N	
R98	1	68	60	8	Y	N	
R99	1	73	64	9	Y	Y	
R100	1	72	63	9	Y	N	
R101	1	71	62	9	Υ	N	
R102	1	74	64	10	Υ	Υ	
R103	1	73	64	10	Υ	N	
R104	1	72	63	9	Υ	N	
R105	1	72	63	9	Υ	Υ	
R106	2	72	63	9	Υ	Υ	
R107	2	72	63	8	Υ	Υ	
R108	2	71	63	8	Υ	Υ	
R109	1	71	63	8	Υ	Υ	
R110	2	69	61	9	Υ	N	
R111	1	68	60	8	Υ	N	
R112	2	66	59	7	Υ	N	Noise Barrier #5
R113	2	64	58	6	Υ	N	Noise Barrier #5
R114	2	65	59	7	Υ	N	See Noise Barrier
R115	1	67	59	8	Υ	N	Evaluation
R116	2	67	59	8	Υ	Υ	Summary
R117	1	65	59	7	Y	Υ	Table 10
R118	2	65	58	7	Υ	Υ	
R119	2	66	59	7	Υ	Υ	
R120	2	65	59	7	Υ	Υ	
R121	1	64	58	6	Υ	N	
	Kingman	Golf Course Esta	ates (Figure 5, D	etail 08) NA	C 66 dBA ¹		
R122	1	64	59	6	Υ	N	
	Cerbat C	Country Club Esta	ites (Figure 5, D	etail 08) NA	C 66 dBA ¹		
R123	1	68	63	6	Υ	N	
R124	1	68	61	7	Υ	Υ	
R125	1	67	61	7	Υ	Υ	
R126	1	63	58	5	Υ	N	
	Cour	ntry Club Manor			dBA ¹		
R127	1	64	58	6	Υ	N	
R128	1	70	63	8	Y	N	
R129	1	74	64	9	Υ	Υ	
R130	1	66	60	6	Υ	N	

						4 ct -p	
					D (*)	1 st Row	
	NO. of	l la mitigata d	Mitigatad	Insertion	Benefited	Design Goal	
Receiver	Dwelling	Unmitigated Noise Level	Mitigated Noise Level	Loss	Receiver (5 dBA)	(7 dBA)	
ID	Units	(dB)	(dBA)	(dBA)	(Y/N]	(7 dbA) [Y/N]	Mitigation
10		y Club Manor (Fi				[1/14]	Wittigation
R131	1	67	60	6	Y	N	-
R132	1	68	61	7	Υ	N	-
R133	1	70	62	8	Υ	N	-
R134	1	70	62	7	Υ	Υ	-
R135	1	65	60	5	Υ	N	-
R136	1	67	61	5	Υ	N	-
R137	1	68	62	6	Υ	N	-
R138	1	69	63	7	Υ	N	-
R139	1	70	63	7	Υ	Υ	1
R140	1	62	59	3	N	N	-
R141	1	66	61	5	Y	N	
R142	1	66	61	6	Y	N	
R143	1	67	62	5	Y	N	
R144	1	67	61	6	Υ	N	
R145	1	70	63	6	Y	N	
R146	1	71	64	7	Υ	Υ	Noise Barrier #5
R147	1	77	68	9	Υ	Υ	
R148	1	71	63	8	Υ	Υ	See Noise Barrier
R149	1	71	63	8	Υ	Υ	Evaluation
R150	1	70	63	7	Υ	Υ	Summary
R151	1	69	62	7	Υ	Υ	Table 10
	Cerb	at Cliffs GC (Figu		- 09) NAC 66	dBA ¹		
R93gc-1	1	79	68	11	Υ	Υ	
R93gc-2	5	74	64	10	Y	Y	
R93gc-3	5	75	65	10	Y	Υ	
R93gc-4	5	74	64	10	Y	N	_
R93gc-5	5	71	62	9	Y	N	_
R93gc-6	5	71	63	8	Y	N	_
R109gc-1	5	77	66	11	Y	Υ	_
R109gc-2	10	73	64	9	Y	Y	_
R123gc-1	6	73	64	9	Y	N	_
R123gc-2	6	72	64	8	Y	N	
R123gc-3	6	73	65	8	Y	N	_
R123gc-4	6	79	67	12	Y	Υ	
R123gc-5	6	76	65	11	Y	Y	
R123gc-6	6	79	67	12	Y	Υ	
R129gc-1	6	80	67	13	Υ	N	

Receiver ID	NO. of Dwelling Units	Unmitigated Noise Level (dB)	Mitigated Noise Level (dBA)	Insertion Loss (dBA)	Benefited Receiver (5 dBA) [Y/N]	1 st Row Design Goal (7 dBA) [Y/N]	Mitigation
	Ce	erbat Cliffs GC (Fi	gure 5, Detail 0	9) NAC 66 dI	BA ¹		
R129gc-2	6	67	60	7	Υ	N	
Gar	dens at King	gman Assisted Liv	ving (Figure 5, D	etails 09 & 1	10) NAC 66 dE	3A ¹	
R152	2	72	64	8	Υ	N	
R153	2	71	64	7	Υ	N	
R154	2	71	63	8	Υ	N	
Kingn	nan Garden:	s Rehab & Care C	enter (Figure 5,	Details 09 8	& 10) NAC 66	dBA ¹	
R155	5	70	63	7	Υ	N	
R156	5	69	63	6	Υ	N	
R157	5	70	64	6	Υ	N	Noise Barrier #5
	Helen's Pla	ace Adult Living (Figure 5, Detail	s 09 & 10) N	AC 71 dBA ¹		
R158	1	81	70	12	Υ	Υ	See Noise Barrier
R159	1	81	69	11	Υ	Υ	Evaluation
R160	1	80	69	11	Υ	Υ	Summary
	Helen's	Place Adult Livin	ng (Figure 5, Det	ails 09 &10)	66 dBA ¹		Table 10
R161	1	81	69	12	Υ	Υ	
R162	1	81	69	11	Υ	Υ	
R163	1	80	69	11	Υ	Υ	
Linger	nfelter Cent	er for Alzheimer'	s Care (Figure 5	, Details 09	& 10) NAC 66	dBA ¹]
R164	4	78	68	10	Υ	Υ	
R165	4	77	68	9	Υ	Υ	
R166	4	80	69	11	Υ	Υ	
	Home	2Suites by Hiltor	n (Figure 5, Deta	ail 10) NAC 7	1 dBA ²]
R167	2	68	61	7	Υ	Υ	

- 1. ADOT NAR 1-decibel approach of FHWA Category B and Category C NAC.
- 2. ADOT NAR 1-decibel approach of FHWA Category E NAC.

West of I-40, south of Stockton Hill Road

Noise Barrier #6 (NB#6) was evaluated to mitigate Build Alternative peak hour noise levels at impacted Category B, C and D receptors located west of I-40 and south of Stockton Hill Road. An existing 6-foot noise wall atop a berm (NW#2) is located on the north side of I-40 WB and provide noise mitigation for residences in the Kingman Country Club Addition. A new noise barrier was evaluated in this location, but it was determined not to be optimal for mitigating future Build Alternative noise impacts; therefore, removal of this wall is recommended, and a new wall located at the I-40 WB shoulder to take advantage of a higher base elevation was investigated.

Figure 5, Detail 07 - 10 shows the location of NW#2 (to be removed) and the proposed NB#6, which is comprised of two noise walls. Category G land uses were included in the evaluation for the purposes of determine feasibility and reasonability of proposed mitigation The first would be located at the outside shoulder of the I-40 EB approaching Stockton Hill Road from the west and continuing along the I-40 WB on-ramp. The second would be located inside the I-40 WB on-ramp at Stockton Hill Road at the I-40 WB shoulder west of the overpass. **Table 8** provides an assessment of the effectiveness of this barrier and **Table 11** provides additional design details and a recommendation determination.

Table 8. Noise Mitigation Evaluation for 2042 Build Alternative, West of I-40 and North of Stockton Hill Road

Receiver ID	NO. of Dwelling Units	Unmitigated Noise Level (dB)	Mitigated Noise Level (dBA)	Insertion Loss (dBA)	Benefited Receiver (5 dBA) [Y/N]	1 st Row Design Goal (7 dBA) [Y/N]	Mitigation
		ry Club Addition	, ,				Willigation
	Billall Court	-	ails 07 & 08) NA		a reagnizorno	ous	
R168	1	71	70	1	N	N	
R169	1	74	64	10	Υ	Υ	
R170	1	68	61	7	Y	N	
R171 ²	1	71	62	9	Υ	N	
R172 ²	1	76	66	11	Υ	Υ	
R173 ²	1	78	66	12	Y	Υ	
R174 ²	1	71	64	7	Υ	N	
R175	1	67	61	7	Υ	N	
R176	1	69	61	7	Υ	N	Noise Barrier #6
R177	1	71	63	8	Υ	N	See Noise Barrier
R178	1	73	64	9	Υ	N	Evaluation
R179	1	67	61	7	Υ	N	Summary
R180	1	70	63	7	Υ	N	Table 10
R181	1	71	64	7	Υ	Ν	
R182	1	71	64	7	Υ	Ν	
R183	1	72	64	7	Υ	Ν	
R184	1	<i>75</i>	65	9	Υ	Υ	
R185	3	73	65	8	Υ	Υ	
R186	1	74	67	7	Υ	Υ	
R187 ²	1	75	67	7	Υ	Υ	
R188	1	75	67	8	Υ	Υ	
R189	1	73	65	8	Υ	Υ	
R190	3	71	64	8	Υ	N	
R191	2	73	65	8	Υ	N	
R192	3	67	61	6	Υ	N	

			I				
						1 st Row	
					Benefited	Design	
	NO. of	Unmitigated	Mitigated	Insertion	Receiver	Goal	
Receiver	Dwelling	Noise Level	Noise Level	Loss	(5 dBA)	(7 dBA)	
ID	Units	(dB)	(dBA)	(dBA)	[Y/N]	[Y/N]	Mitigation
King	gman Counti	ry Club Addition			d Neighborho	ods	
5100	1		tails 08 - 10) NA				
R193	1	68	62	6	Y	N	
R194	1	68	62	6	Y	N	
R195	1	68	62	6	Y	N	
R196	1	68	62	6	Υ	N	
R197	1	67	61	6	Υ	N	
R198	1	68	62	6	Υ	N	
R199	1	69	62	7	Υ	N	
R200	1	69	62	6	Υ	N	
R201	1	69	62	7	Υ	N	
R202	1	69	62	7	Υ	N	
R203	1	70	63	7	Υ	N	
R204	1	70	63	7	Υ	N	
R205	2	72	64	8	Υ	Υ	
R206	1	65	59	6	Υ	N	
R207	3	74	66	8	Υ	Υ	Noise Barrier #6
R208	1	68	61	7	Υ	Υ	
R209	1	68	61	7	Υ	N	See Noise Barrier
R210	1	68	62	7	Υ	N	Evaluation
R211	1	69	62	7	Υ	Υ	Summary
R212	1	69	62	7	Υ	Υ	Table 10
R213	1	69	62	7	Υ	Υ	
R214	1	69	62	7	Υ	Υ	
R215	1	66	59	7	Υ	N	
R216	4	66	60	6	Υ	N	
R217	4	71	63	9	Υ	Υ	
	Cimarro	n Apartments (Fi	gure 5, Details (9 & 10) NA	C 66 dBA ¹		
R218	6	69	60	8	Υ	N	
R219	6	70	62	9	Υ	N	
R220	6	73	64	9	Υ	N	
R221	5	73	64	8	Υ	N	
R222	5	73	64	8	Υ	N	
R223	6	73	64	8	Υ	Υ	1
R224	6	73	64	9	Υ	Υ	1
R225	1	73	64	9	Υ	Υ	1
	KRN	иС Urgent Care (Figure 5, Detail	10) NAC 52	dBA ³]
R226	1	69 (49) ³	444	5	Υ	N	

Receiver ID	NO. of Dwelling Units	Unmitigated Noise Level (dB)	Mitigated Noise Level (dBA)	Insertion Loss (dBA)	Benefited Receiver (5 dBA) [Y/N]	1 st Row Design Goal (7 dBA) [Y/N]	Mitigation
	KRN	ЛС Urgent Care (Figure 5, Detail	10) NAC 52	dBA ³		Noise Barrier #6
R227	1	70 (50) ³	45 ⁴	5	Υ	N	See Noise Barrier Evaluation
R228	1	70 (50) ³	45 ⁴	5	Υ	N	Summary Table 10

- 1. ADOT NAR 1-decibel approach of FHWA Category B and Category C NAC.
- 2. There is no FHWA NAC for Category G land uses.
- 3. ADOT NAR 1-decibel approach of FHWA Category D NAC, which is an interior noise standard. Interior noise levels assume a 20 dBA IL across a typical building shell with windows and doors closed.
- 4. Minimum achievable interior noise level assuming listed IL from NB#6.

West of I-40/US 93 System Interchange

Noise Barrier #7 (NB#7) was evaluated to mitigate Build Alternative peak hour noise levels at homes located at the end of Wagon Trail Road, just north of the Build Alternative directional ram from I-40 EB to US 93 WB (Ramp EN). Figure 5, Detail 03 shows the location of NB#7, which would be located at the outside shoulder of Ramp EN and continuing along US 93 WB at the shoulder. Noise Barrier #8 (NB#8) was evaluated to mitigate Build Alternative peak hour noise levels at homes located along westbound Beale Street and west of the proposed I-40/US 93 system interchange. Figure 5, Detail 01 shows the location of NB#8, which would be located north of the sidewalk adjacent the exiting Beale Street westbound lanes. Noise Barrier #9 (NB#9) was evaluated to mitigate Build Alternative peak hour noise levels at homes located west of the proposed I-40/US 93 system interchange. Figure 5, Detail 02 shows the location of NB#9, which would be located at the right-of-way near the I-40 WB off-ramp to Beale Street. Table 9 provides an assessment of the effectiveness of these barriers and Table 10 provides additional design details and a recommendation determination for each.

Table 9. Noise Mitigation Evaluation for 2042 Build Alternative, West of I-40 and North of US 93/Beale Street

Receiver ID	NO. of Dwelling Units	Unmitigated Noise Level (dB)	Mitigated Noise Level (dBA)	Insertion Loss (dBA)	Benefited Receiver (5 dBA) [Y/N]	1 st Row Design Goal (7 dBA) [Y/N]	Mitigation
	Mobile and	Single-Family Ho	omes near Ram	EN (Figure	5, Detail 03)		Noise Barrier #7
R229	1	63	62	1	N	N	Evaluation Summary Table
R230	1	63	61	2	N	N	10

Receiver ID	NO. of Dwelling Units Mobile and	Unmitigated Noise Level (dB) Single-Family Ho	Mitigated Noise Level (dBA)	Insertion Loss (dBA)	Benefited Receiver (5 dBA) [Y/N] 5. Detail 03)	1 st Row Design Goal (7 dBA) [Y/N]	Mitigation See Noise Barrier
R231	1	69	62	7	У	У	Evaluation Summary Table 10
		Metcalfe Ad	res (Figure 5, D	etail 01)			Noise Barrier #8
R273	1	63	62	1	N	N	See Noise Barrier
R274	1	62	61	1	N	N	Evaluation
R275	1	66	63	3	N	N	Summary
R276	1	62	62	0	N	N	Table 10
	M	letcalfe Acres/M	onte Vista (Figu	re 5, Detail (02)		Noise Barrier #9
R277	1	65	64	1	N	N	See Noise Barrier
R278	1	71	66	5	Υ	N	Evaluation Summary
R279	1	73	61	12	Υ	Υ	Table 10

Summary of Noise Barrier Recommendations

A total of nine noise barriers were evaluated to provide mitigation of future (2042) peak hour noise levels associated with the Build Alternative. **Table 10** summarizes the final recommendation for each barrier or combination of barriers. Of the nine noise barriers evaluated for Build Alternative, two (NB#5 and NB#6) meet the ADOT NAR reasonable mitigation requirements of a 7 dBA noise reduction design goal for 50% of 1st row benefited receptors and \$49,000 maximum cost per benefited receptor. The barriers also satisfy the ADOT NAR acoustic feasibility factor of a 5 dBA noise reduction benefit at 50% of impacted receptors. The remaining six barriers (NB #2 – NB #4, NB #7 – NB #9) do not satisfy one or more of these requirements and are not recommended. Similarly, NB#1 does not satisfy one or more of these requirements; however, it is recommended because it would provide an equivalent noise reduction to receivers R40 – R59 (representing homes in the Monte Vista #1 neighborhood) that is provided by NW #1, which will be removed by the Build Alternative.

The recommended noise barriers are:

- NB#1 at the Ramp WS (I-40 EB on-ramp from Beale Street) outside shoulder
- Combination NB#5:
 - The first segment at the I-40 EB outside shoulder to the I-40 EB off-ramp outside shoulder
 - The second segment at the I-40 EB outside shoulder
- Combination NB#6:
 - o The first segment at the I-40 WB outside shoulder
 - The second segment at the I-40 WB on-ramp outside shoulder at Stockton Hill Road to I-40 WB

For recommended barriers NB #5 and NB #6, a sound absorptive material is recommended for the bottom six to eight feet of barrier surface above the jersey barrier. Examples include panels that can be mounted to the barrier surface or use or application of a surface treatment if the barrier is constructed of cast-in-place concrete-masonry. Per the ADOT NAR 4.1.2(b), sound absorbing wall, or material, considered must have been included in ADOT's Approved Products List, or as a minimum had been placed on the approved list by another state's Department of Transportation, and approved by ADOT to be considered as a noise abatement option for a noise barrier. The feasibility of construction for all recommended barriers would be evaluated at a later stage of design.

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⁷ The cost of panels varies dependent on the application. For mounted panels, an equivalent unit cost that is assumed for concrete masonry unit barriers of \$35 per square foot applies. A cast-in-place barrier with surface treatment would increase the unit cost by \$5 to \$15 per square foot depending on materials specifications. Per the ADOT NAR, these cost are not considered in the cost-per-benefit feasibility of evaluated barriers.

Table 10. Noise Barrier Recommendation Summary

Noise Barrier	Barrier Height (ft.)	Barrier Length (ft.)	Barrier Area (ft²)	Total Barrier Cost	No. of Benefited Receptors	Cost Per Benefit	No. of Impacted Receptors	No. of Impacted & Benefited	Impacted & Benefited	7 dBA Design Goal Met First Row	Noise Wall Recommended [Y/N]
				Noise B	arrier #1 (Figu	ure 5, Detail 02	2fi-10)			_	
Outside shoulder Ramp WS	10 – 18	923	12,278	\$497,502 ¹	4	\$124,376	12	4	33%	0 of 4	Y, Relocate/ Replace ²
				Noise Ba	rrier #2 (Figu	re 5, Details 02	2 & 04)				
Outside shoulder Ramp WS STA to I-40 EB	20	1,974	39,478	\$2,114,481 ²	9	\$234,942	8	8	100%	2 of 8	N2 ^{4,5}
Ramp SE outside shoulder	10	2,022	20,221	\$2,114,401	9	\$234, 3 42	0	0	100%	2016	NZ '
				Noise Ba	rrier #3 (Figu	re 5, Details 05	5 & 06)				
Ramp SE outside shoulder	20	3,090	64,208	\$2,272,300 ²	2	\$1,136,150	1	1	100%	0 of 3	N ^{4,5}
				Noise Ba	arrier #4 (Figu	re 5, Details 0	4 - 06)				
Ramp WN outside shoulder	20	2,662	38,039	\$1,883,537	1	\$1,888,537	3	1	33%	0 of 3	N ^{3,4,5}

Noise Barrier	Barrier Height (ft.)	Barrier Length (ft.)	Barrier Area (ft²)	Total Barrier Cost	No. of Benefited Receptors	Cost Per Benefit	No. of Impacted Receptors	No. of Impacted & Benefited	Impacted & Benefited	7 dBA Design Goal Met First Row	Noise Wall Recommended [Y/N]
				Noise Ba	arrier #5 (Figu	re 5, Details 0	7 - 10)				
Outside shoulder I-40 EB to I-40 EB off-ramp at Stockton Road	10 - 14	7,216	94,383	\$3,303,437	201	16,435	187	182	97%	98 of 102	Y ⁶
Outside shoulder I-40 EB	10 - 12										
				Noise Ba	arrier #6 (Figu	re 5, Details 0	7 - 10)				
Outside shoulder I-40 WB	12	6.720	00.746	62 227 0441	400	620.522	404	404	1000/	40 - 6 52	V6
Outside shoulder I-40 WB on-ramp at Stockton Road to I-40 WB	12 - 14	6,728	89,716	\$3,227,011 ¹	109	\$30,523	104	104	100%	49 of 53	γ6
		•		Noise	Barrier #7 (F	igure 5, Detail	03)				
Ramp SE outside shoulder	12 - 16	1,100	16,779	\$419,986	1	\$419,986	1	1	100%	1 of 1	N ⁵

Noise Barrier	Barrier Height (ft.)	Barrier Length (ft.)	Barrier Area (ft2)	Total Barrier Cost	No. of Benefited Receptors	Cost Per Benefit	No. of Impacted Receptors	No. of Impacted & Benefited	Impacted & Benefited	7 dBA Design Goal Met First Row	Noise Wall Recommended
				NOISE	Barrier #8 (F	igure 5, Detail	(101)				
Ramp WN outside shoulder	20	300	6,000	\$209,999	0	N/A	1	0	0%	0 of 1	N ^{3,4,5}
				Noise	Barrier #9 (F	igure 5, Detail	02)				
Right-of-Way I-40 WB off-ramp at Beale Street	14 - 18	585	9,618	\$336,636	2	\$168,318	2	2	100%	1 of 1	N ⁵

- 1. Includes cost of removing existing noise wall @ \$20/sq. ft.: NB #1 (NW #1) and NB #6 (NW #2).
- 2. Noise Barrier #1 does not satisfy the ADOT NAR feasible, reasonable or cost criterion; however, the barrier is recommended because it will provide an IL equivalent to NW#1, which will be removed by the Build Alternative.
- 3. Barrier does not achieve the ADOT NAR feasible criteria of a 5 dBA noise reduction benefit at 50% of impacted receivers.
- 4. Barrier does not meet the ADOT NAR reasonable design goal of a 7 dBA noise reduction for 1st row receptors.
- 5. Barrier does not meet the ADOT NAR \$49,000 cost-benefit ratio.
- 6. A sound absorptive material is recommended for the bottom 6 8 feet of barrier above the adjacent jersey barrier.

CONSTRUCTION NOISE AND VIBRATION

Depending on the nature of construction operations, the duration of the noise could last from seconds (e.g. a truck passing a customer) to months (e.g. constructing a bridge). Construction noise is also intermittent and depends on the type of operation, location, and function of the equipment and the equipment usage cycle. Construction equipment is typically considered as a point source, as opposed to traffic which is considered as a line source; therefore, the noise level decreases, theoretically, by 6 dBA per doubling the distance from it, as opposed to 3 dBA for line source. Noise levels, at various distances, using listed equipment, are shown in **Table 11**. ADOT has set forth guidelines for construction noise in the *Standard Specifications for Road and Bridge Construction*, 2008. Per ADOT specifications 104.08 Prevention of Air and Noise Pollution:

"The contractor shall comply with all local sound control and noise rules, regulations and ordinances which apply to any work pursuant to the contract. Each internal combustion engine used for any purpose on the work or related to the work shall be equipped with a muffler or a type recommended by the manufacturer. No internal combustion engine shall be operated on the work without its muffler being in good working condition."

Table 11. Construction Noise Levels at Various Distances from Equipment

	L ₁₀							
Equipment	R_300 ft	R_600 ft	R_900 ft	R_1200 ft	R_1500 ft			
Auger Drill Rig	64.8	58.8	55.3	52.8	50.8			
Boring Jack Power Unit	67.4	61.4	57.9	55.4	53.4			
Compactor (ground)	63.7	57.7	54.1	51.6	49.7			
Concrete Mixer Truck	62.3	56.2	52.7	50.2	48.3			
Dump Truck	59.9	53.9	50.4	47.9	45.9			
Excavator	64.2	58.1	54.6	52.1	50.2			
Generator	65.1	59.0	55.5	53.0	51.1			
Compressor (air)	61.1	55.1	51.6	49.1	47.1			
Grader	68.5	62.4	58.9	56.4	54.5			
Warning Horn	57.6	51.6	48.1	45.6	43.6			
All Other Equipment > 5 HP	69.4	63.4	59.9	57.4	55.4			
Bar Bender	60.4	54.4	50.9	48.4	46.5			
Concrete Pump Truck	61.8	55.8	52.3	49.8	47.9			
Soil Mix Drill Rig	64.4	58.4	54.9	52.4	50.4			
Concrete Saw	70.0	64.0	60.5	58.0	56.0			
Auger Drill Rig	64.8	58.8	55.3	52.8	50.8			
Roller	60.4	54.4	50.9	48.4	46.5			

Source: FHWA Roadway Construction Noise Model (FHWA, 2008).

 L_{10} – noise level exceeded 10 percent of the time during the noise measurement interval and due to sporadic or intermittent events, such as noise from construction equipment.

Ground vibration and ground-born noise can also be a source of annoyance to individuals who live or work close to vibration-generating activities. Pile driving, demolition activity, blasting, and crack-and-seat operations are the primary sources of vibration, while the impact pile driving can be the most significant source of vibration at construction sites. It is recommended to apply methods that may be practical and appropriate in specific situations, to reduce vibration to an acceptable level. Such measures may be:

- Jetting,
- Predrilling
- Cast-in-place or auger cast piles
- Non-displacement piles
- Pile cushioning
- Using alternative non-impact drivers
- Scheduling activities to minimize disturbance at near-construction sites

COORDINATION WITH LOCAL OFFICIALS

At the time of the preparation of this noise analysis technical report, results had not been presented to the local officials. Upon request of the local land use planning agency or local public agency, noise contour lines may be produced during the noise analysis process for project alternative screening and planning purposes only, as per ADOT NAR, Section 2.9.6 Noise Contours.

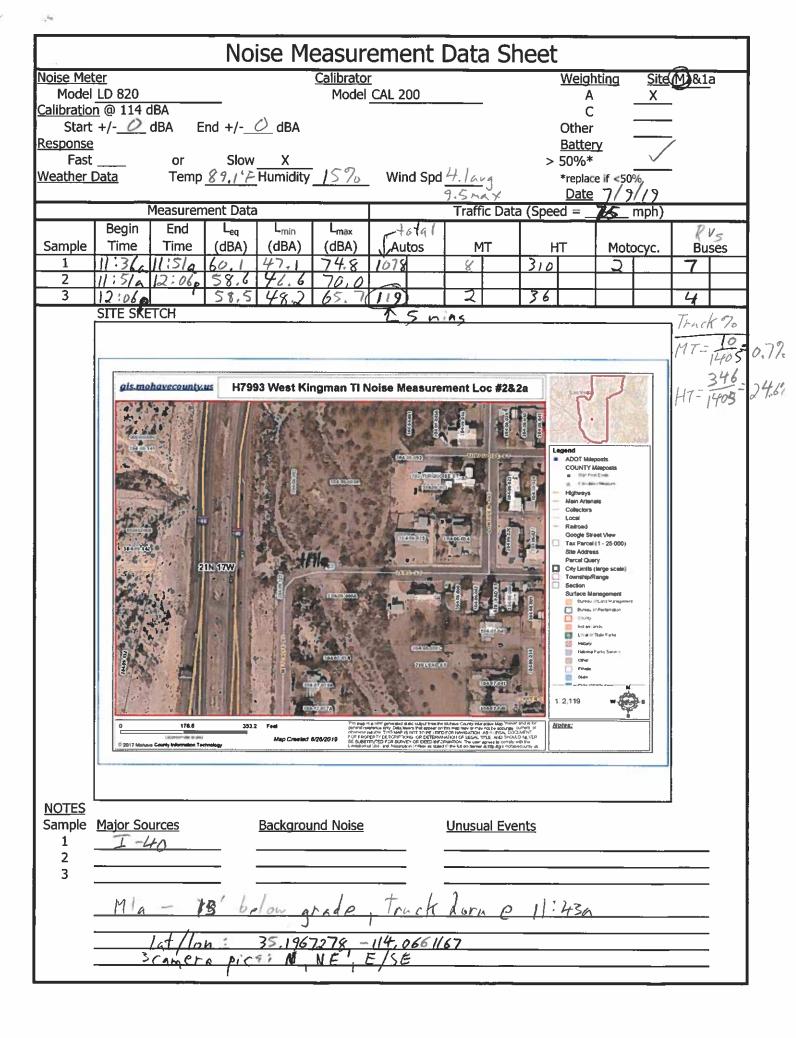
STATEMENT OF LIKELIHOOD

As per 23 CFR 772.13(g)(3), the noise analysis was completed to the extent of design information that is available at this time. This statement of likelihood about the study recommendations is included since feasibility and reasonableness determinations may change due to changes in project design after approval.

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APPENDIX A – NOISE MEASUREMENT DATA SHEETS



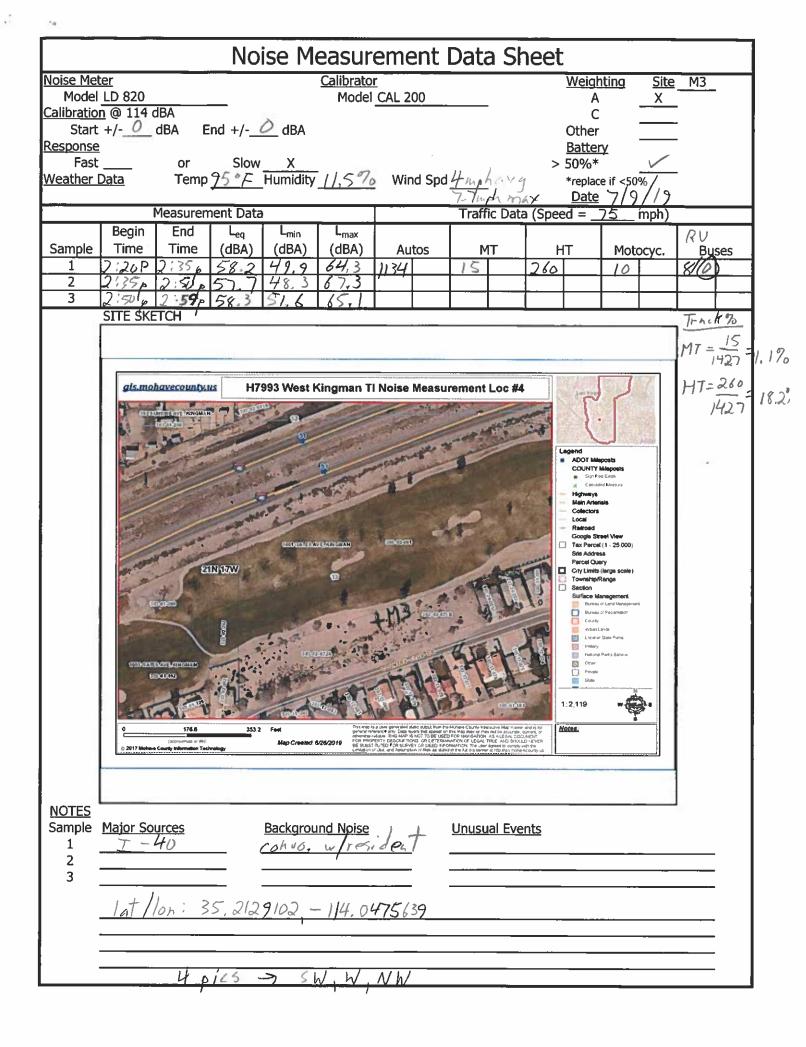
Noise Measurement Data Sheet Project West Kingman TI Date 7/9//9 Site Mik1a SITE SKETCH Mla downhill < I-40 EB open median Metralfe Rd Mla

	N	oise Measurer	ment Data S	Sheet			
	LD 820	<u>Calibrator</u> Model CA	AL 200	<u>Weigh</u> A	iting <u>Site</u> X	M18(1a)	
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Noise Measurement Data Sheet	
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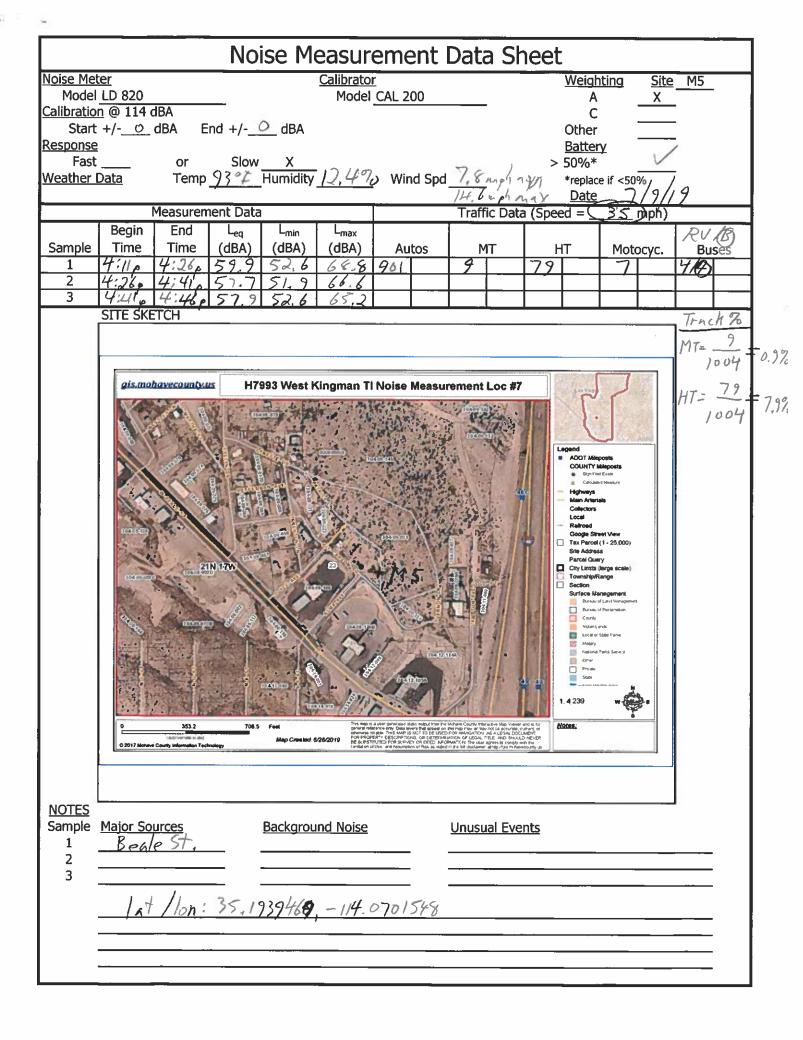
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APPENDIX B – FEDERAL TRANSIT ADMINISTRATION NOISE IMPACT ASSESSMENT SPREADSHEET SCENARIO RUNS FOR ATCHISON-TOPEKA

Federal Transit Administration Noise Impact Assessment Spreadsheet

version: 1/29/2019

Receiver Parameters	
Receiver:	Receiver 1
Land Use Category:	2. Residential
Existing Noise (Measured or Generic Value):	59 dBA

Noise Source Parameters		
	Number of Noise Sources:	1

Noise Source Param	neters	Source 1
	Source Type:	Fixed Guideway
	Specific Source:	Diesel Electric Locomotive
Daytime hrs	Avg. Number of Locos/train	2
	Speed (mph)	40
	Avg. Number of Events/hr	4.17
Nighttime hrs	Avg. Number of Locos/train	2
	Speed (mph)	40
	Avg. Number of Events/hr	4.17
Distance	Distance from Source to Receiver (ft)	840
	Number of Intervening Rows of Buildings	1
Adjustments		

	Noise Barrier?	No
	Joint Track/Crossover?	
	Embedded Track?	
	Aerial Structure?	No

Project Results Summary

Existing Ldn:	59 dBA
Total Project Ldn:	50 dBA
Total Noise Exposure:	60 dBA
Increase:	1 dB
Impact?:	None

Distance to Impact Contours

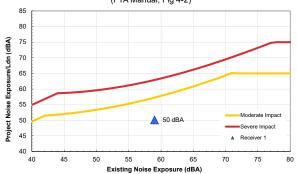
Dist to Mod. Impact Contour	
(Source 1):	561 ft
Dist to Sev. Impact Contour	
(Source 1):	235 ft

Source 1 Results

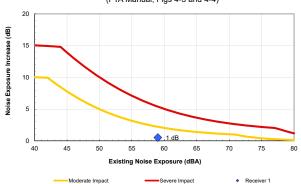
Leq(day): 43.7 dBA Leq(night): 43.7 dBA Ldn: 50.1 dBA

Noise Impact Criteria (FTA Manual, Fig 4-2)

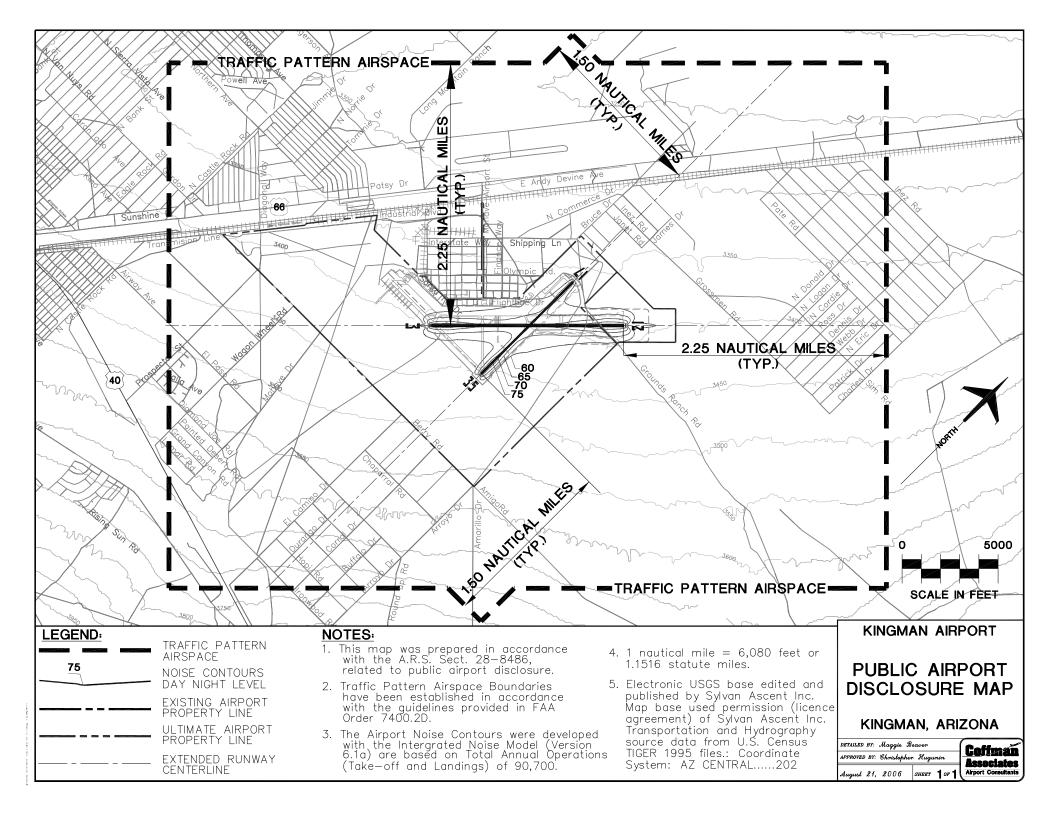




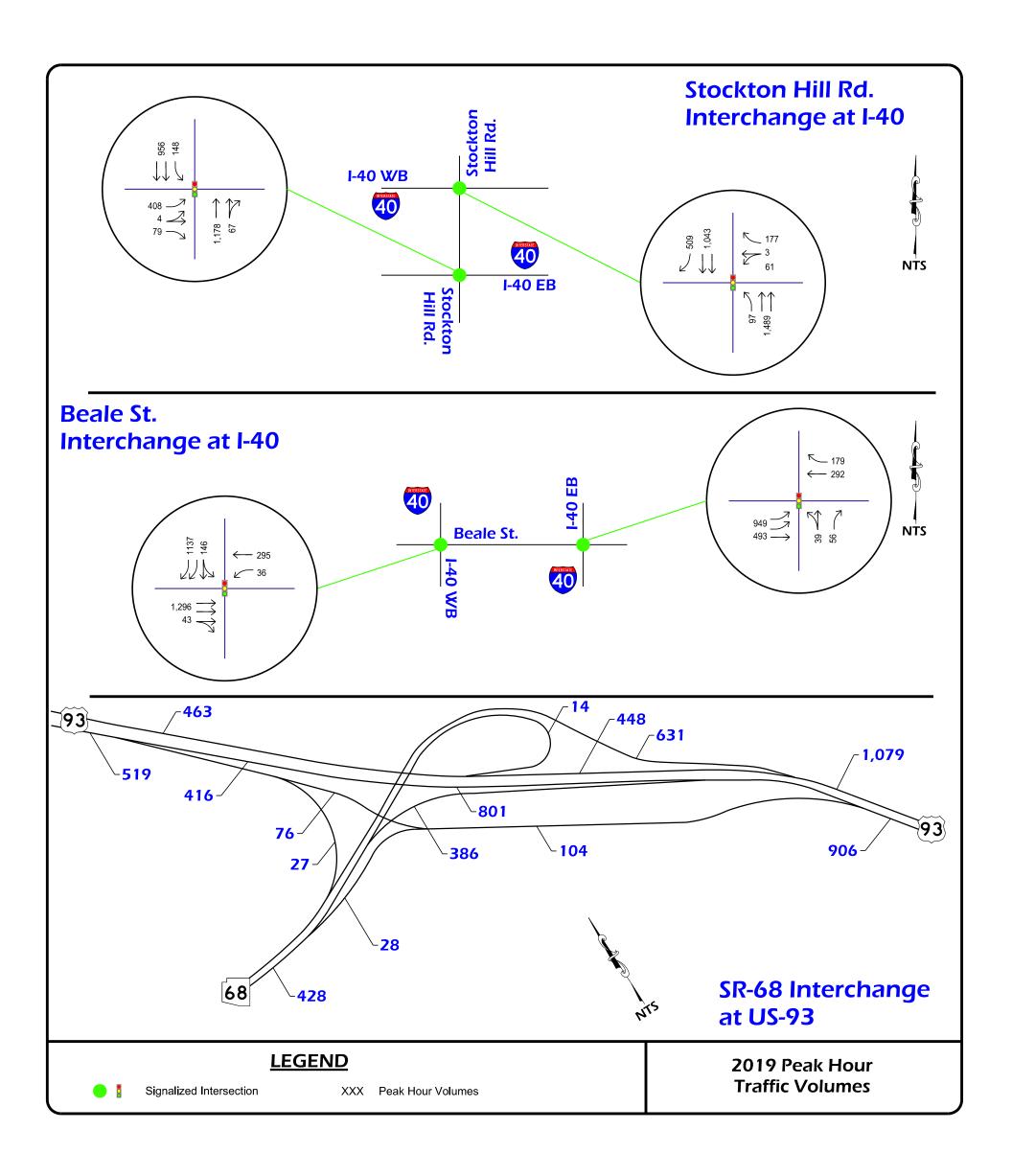
Increase in Cumulative Noise Levels Allowed (FTA Manual, Figs 4-3 and 4-4)



APPENDIX C – KINGMAN AIRPORT BASE NOISE CONTOURS

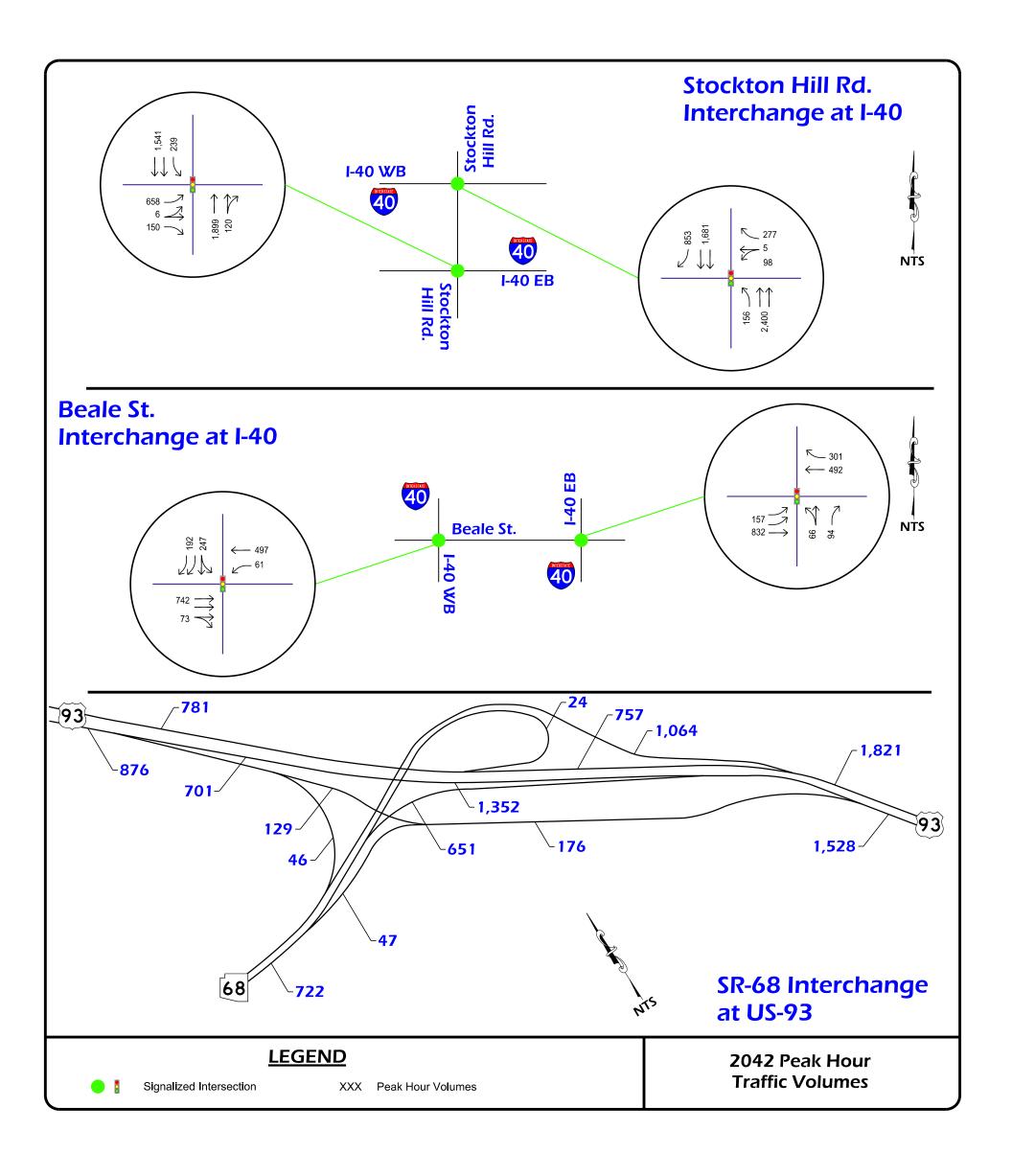


APPENDIX D – TRAFFIC DATA



Direction	Link Name	Segment Type	Link No	Volume	Speed	Density	No of lanes	Density/Lane	LOS
WB/SB	East of Stockton TI	3: Freeway (free lane selection)	1	2296	75.8	30.3	2	15.1	В
WB/SB	Between Stockton TI	3: Freeway (free lane selection)	2	2072	75.3	27.5	2	13.8	В
WB/SB	Stockton Off Ramp	6: Direct Connect & Ramps	3	227	53.4	4.3	1	4.3	А
WB/SB	Between Stockton TI	3: Freeway (free lane selection)	4	2047	75.3	27.2	2	13.6	В
WB/SB	Between Stockton TI	3: Freeway (free lane selection)	5	2072	75.3	27.5	2	13.8	В
WB/SB	Stockton On Ramp	6: Direct Connect & Ramps	6	633	49.1	12.9	1	12.9	В
WB/SB	West of Stockton TI	3: Freeway (free lane selection)	7	2676	63.4	42.2	3	14.1	В
EB/NB	West of Stockton TI	3: Freeway (free lane selection)	8	2388	63.7	37.5	2	18.7	С
EB/NB	Stockton Off Ramp	6: Direct Connect & Ramps	9	510	49.2	10.4	1	10.4	В
EB/NB	Between Stockton TI	3: Freeway (free lane selection)	10	1876	64.0	29.3	2	14.7	В
EB/NB	Between Stockton TI	3: Freeway (free lane selection)	11	1881	64.9	29.0	2	14.5	В
EB/NB	Between Stockton TI	3: Freeway (free lane selection)	12	1892	65.3	29.0	2	14.5	В
EB/NB	Stockton On Ramp	6: Direct Connect & Ramps	13	227	51.8	4.4	1	4.4	А
EB/NB	East of Stockton TI	3: Freeway (free lane selection)	14	2126	65.2	32.6	2	16.3	В
WB/SB	Lead to 1-40 to US-93 Ramp	3: Freeway (free lane selection)	16	2703	63.8	42.4	2	21.2	С
WB/SB	I-40 SB after ramp split	3: Freeway (free lane selection)	17	2658	56.4	47.2	2	23.6	С
EB/NB	US93 East of 68 Interchange	8: Merge	18	782	68.4	11.4	3	3.8	Α
EB/NB	I-40 NB Beale St On Ramp Merge	8: Merge	19	2385	62.2	38.4	3	12.8	В
EB/NB	I-40 NB E of Beale St Merge	3: Freeway (free lane selection)	20	2354	63.7	37.0	2	18.5	С
EB/NB	I-40N at US93E Ramp Merge	8: Merge	22	2411	64.7	37.3	2	18.6	В
EB/NB	I-40N East of US93E Ramp Merge	3: Freeway (free lane selection)	23	2389	65.2	36.6	2	18.3	С
EB/NB	West of Stockton TI	3: Freeway (free lane selection)	25	2319	65.3	35.5	2	17.8	В
EB/NB	East of Stockton TI	8: Merge	27	2078	64.3	32.3	3	10.8	В
WB/SB	I-40S S of US93 Ramp Merge	3: Freeway (free lane selection)	31	2707	53.4	50.7	2	25.4	С
EB/NB	N of Beal On Ramp Merge	3: Freeway (free lane selection)	35	2385	61.0	39.1	2	19.5	С
EB/NB	Between Beale TI	3: Freeway (free lane selection)	36	1263	66.6	19.0	2	9.5	А
WB/SB	Between Beale TI	3: Freeway (free lane selection)	40	1622	50.6	32.1	2	16.0	В
WB/SB	Beale Off Ramp	6: Direct Connect & Ramps	41	1264	46.2	27.4	1	27.4	С
WB/SB	Beale Off Ramp	6: Direct Connect & Ramps	42	1287	44.5	28.9	1	28.9	D
WB/SB	Beale Off Ramp	6: Direct Connect & Ramps	43	1268	46.4	27.3	3	9.1	Α
WB/SB	Beale Off Ramp	6: Direct Connect & Ramps	44	1080	45.0	24.0	2	12.0	В
EB/NB	Between Beale TI	3: Freeway (free lane selection)	46	1282	66.5	19.3	2	9.6	А
EB/NB	Between Beale TI	3: Freeway (free lane selection)	47	2205	63.0	35.0	4	8.7	Α
WB/SB	Between Beale TI	8: Merge	49	1401	62.6	22.4	2	11.2	В
EB/NB	Beale On Ramp	6: Direct Connect & Ramps	50	1121	62.7	17.9	2	8.9	А
EB/NB	S of Beale TI	3: Freeway (free lane selection)	51	1374	76.6	17.9	2	9.0	Α
EB/NB	S of Beale TI	3: Freeway (free lane selection)	52	1318	66.7	19.8	2	9.9	Α
EB/NB	Beale Off Ramp	6: Direct Connect & Ramps	53	92	51.8	1.8	1	1.8	А
WB/SB	Between Beale TI	3: Freeway (free lane selection)	54	1403	65.3	21.5	2	10.7	А
WB/SB	S of Beale TI	8: Merge	55	1490	65.4	22.8	3	7.6	А
WB/SB	Beale on Ramp	6: Direct Connect & Ramps	56	77	52.4	1.5	1	1.5	А
EB/NB	S of Beale TI	3: Freeway (free lane selection)	58	1504	66.0	22.8	2	11.4	В
WB	Beale St	1: Urban (motorized)	59	1050	53.1	19.8	2	9.9	Α
WB	Beale St	1: Urban (motorized)	60	1055	56.8	18.6	2	9.3	Α
EB	Beale St	1: Urban (motorized)	61	897	66.7	13.5	2	6.7	Α
EB	Beale St	1: Urban (motorized)	62	891	66.7	13.4	2	6.7	Α
WB	Beale St	1: Urban (motorized)	67	1049	56.8	18.5	2	9.2	А
EB	Beale St	1: Urban (motorized)	74	894	67.0	13.3	2	6.7	Α
EB/NB	US93 W of Beale St Merge	3: Freeway (free lane selection)	76	891	66.8	13.3	2	6.7	А
EB/NB	US93 E of Beale St Merge	3: Freeway (free lane selection)	77	900	66.8	13.5	2	6.7	Α
WB/SB	Beale St to US93 Merge Area	8: Merge	79	1045	62.4	16.7	2	8.4	Α

WB/SB	West of Beal St Merge	3: Freeway (free lane selection)	82	1052	66.1	15.9	2	8.0	А
WB/SB	East of Beal St Merge	3: Freeway (free lane selection)	84	1045	56.7	18.4	2	9.2	Α
EB/NB	West of Beale St Merge	3: Freeway (free lane selection)	85	891	66.8	13.3	2	6.7	Α
EB/NB	West of Beale St Merge	3: Freeway (free lane selection)	86	896	67.0	13.4	3	4.5	Α
EB/NB	West of Beale St Merge	3: Freeway (free lane selection)	87	136	67.5	2.0	1	2.0	Α
WB/SB	West of Beale St Merge	3: Freeway (free lane selection)	88	1056	66.4	15.9	2	7.9	Α
WB/SB	West of Beale St Merge	3: Freeway (free lane selection)	91	1045	66.5	15.7	3	5.2	Α
WB/SB	US93 West of 68 Split	3: Freeway (free lane selection)	92	407	66.9	6.1	2	3.0	Α
WB/SB	S 93 ramp to 68	3: Freeway (free lane selection)	94	597	66.7	8.9	2	4.5	Α
WB/SB	US93 West of 68 Split	3: Freeway (free lane selection)	95	439	67.1	6.6	2	3.3	Α
NB	68 Loop to US93	6: Direct Connect & Ramps	96	16	27.7	0.6	1	0.6	Α
WB/SB	68 Loop to US93 Merge	8: Merge	99	453	66.3	6.8	3	2.3	Α
WB/SB	US93 W of 68 Interchange	3: Freeway (free lane selection)	100	457	67.3	6.8	2	3.4	Α
WB	US93 Loop to 68	6: Direct Connect & Ramps	101	612	59.0	10.4	2	5.2	Α
WB	US93 Loop to 68	6: Direct Connect & Ramps	102	611	46.9	13.0	2	6.5	Α
EB/NB	US93 W of 68 Split	3: Freeway (free lane selection)	103	516	77.2	6.7	2	3.3	Α
WB/SB	US93 W of 68 Split	6: Direct Connect & Ramps	104	95	69.2	1.4	1	1.4	Α
EB/NB	US93 W of 68 Interchange	3: Freeway (free lane selection)	105	414	77.2	5.4	2	2.7	Α
WB/SB	US93 W of 68 Split	6: Direct Connect & Ramps	106	95	57.2	1.7	2	0.8	Α
WB	US93 Ramp to 68	6: Direct Connect & Ramps	107	27	57.1	0.5	1	0.5	Α
EB	US93 Ramp to Truck Stop	6: Direct Connect & Ramps	108	78	57.2	1.4	1	1.4	Α
WB/SB	US93 to 68 Merge Area	8: Merge	109	636	53.4	11.9	3	4.0	А
WB/SB	68 W of Interchange	3: Freeway (free lane selection)	111	643	64.4	10.0	2	5.0	Α
EB/NB	68 Ramp to Truck Stop	6: Direct Connect & Ramps	113	26	60.0	0.4	1	0.4	Α
EB/NB	Truck Stop	3: Freeway (free lane selection)	114	100	57.1	1.8	1	1.8	Α
EB/NB	68 W of Interchange	3: Freeway (free lane selection)	115	416	77.0	5.4	2	2.7	Α
EB/NB	68 Ramp to US93	6: Direct Connect & Ramps	116	381	59.4	6.4	1	6.4	Α
WB	68 Loop to US93	6: Direct Connect & Ramps	117	15	60.0	0.3	1	0.3	Α
EB/NB	US93 W of Beale St	3: Freeway (free lane selection)	118	784	69.9	11.2	2	5.6	Α
EB/NB	US93 W of Beale St	3: Freeway (free lane selection)	119	772	69.9	11.0	3	3.7	Α
EB/NB	Truck Stop	3: Freeway (free lane selection)	120	104	58.0	1.8	1	1.8	Α



Direction	Link Name	Segment Type	Link No	Volume	Speed	Density	No of lanes	Density/Lane	LOS
WB/SB	East of Stockton TI	3: Freeway (free lane selection)	1	3887.8	69.6	55.9	2	28.0	D
WB/SB	Between Stockton TI	3: Freeway (free lane selection)	2	3504.1	69.2	50.7	2	25.3	С
WB/SB	Stockton Off Ramp	6: Direct Connect & Ramps	3	387.0	51.9	7.5	1	7.5	А
WB/SB	Between Stockton TI	3: Freeway (free lane selection)	4	3460.5	70.6	49.0	2	24.5	С
WB/SB	Between Stockton TI	3: Freeway (free lane selection)	5	3500.8	71.2	49.2	2	24.6	С
WB/SB	Stockton On Ramp	6: Direct Connect & Ramps	6	1067.0	47.3	22.6	1	22.6	С
WB/SB	West of Stockton TI	3: Freeway (free lane selection)	7	4526.6	64.2	70.5	3	23.5	С
EB/NB	West of Stockton TI	3: Freeway (free lane selection)	8	3998.4	59.1	67.7	3	22.6	С
EB/NB	Stockton Off Ramp	6: Direct Connect & Ramps	9	852.4	46.6	18.3	1	18.3	В
EB/NB	Between Stockton TI	3: Freeway (free lane selection)	10	3124.8	60.4	51.7	2	25.9	С
EB/NB	Between Stockton TI	3: Freeway (free lane selection)	11	3123.9	62.0	50.4	2	25.2	С
EB/NB	Between Stockton TI	3: Freeway (free lane selection)	12	3143.6	58.8	53.7	2	26.9	D
EB/NB	Stockton On Ramp	6: Direct Connect & Ramps	13	383.4	50.5	7.6	1	7.6	А
EB/NB	East of Stockton TI	3: Freeway (free lane selection)	14	3538.3	57.7	61.3	2	30.6	D
WB/SB	West of Stockton TI	3: Freeway (free lane selection)	15	4552.6	64.7	70.4	3	23.5	С
WB/SB	Lead to 1-40 to US-93 Ramp	3: Freeway (free lane selection)	16	4550.8	52.9	86.3	3	28.8	D
WB/SB	I-40 SB after ramp split	3: Freeway (free lane selection)	17	2789.9	50.4	55.4	2	27.7	D
EB/NB	US93 East of 68 Interchange	8: Merge	18	1322.8	67.4	19.6	3	6.5	A
EB/NB	I-40 NB Beale St On Ramp Merge	8: Merge	19	2509.5	29.6	85.2	3	28.4	D
EB/NB	I-40 NB E of Beale St Merge	3: Freeway (free lane selection)	20	2588.5	57.6	44.9	2	22.5	С
EB/NB	US93E to I-40N Ramp	6: Direct Connect & Ramps	21	1400.2	66.4	21.1	2	10.5	В
EB/NB	I-40N at US93E Ramp Merge	8: Merge	22	3996.8	63.0	63.4	4	15.9	В
EB/NB	I-40N East of US93E Ramp Merge	3: Freeway (free lane selection)	23	3973.3	64.4	61.7	3	20.6	С
EB/NB	West of Stockton TI	3: Freeway (free lane selection)	25	3976.5	64.8	61.4	3	20.5	С
WB/SB	I-40S to US93W Ramp	6: Direct Connect & Ramps	26	1745.6	55.5	31.5	2	15.7	В
EB/NB	East of Stockton TI	8: Merge	27	3454.2	35.8	97.7	3	32.6	D
WB/SB	I-40S to US93W Ramp	6: Direct Connect & Ramps	28	1579.6	56.0	28.2	2	14.1	В
EB/NB	US93E to I-40N Ramp	6: Direct Connect & Ramps	29	1401.6	66.4	21.1	2	10.5	В
EB/NB	US93E to I-40N Ramp	6: Direct Connect & Ramps	30	1404.6	66.4	21.1	2	10.6	В
WB/SB	I-40S S of US93 Ramp Merge	3: Freeway (free lane selection)	31	2811.8	54.0	52.1	2	26.1	D
WB/SB	I-40N to US93W	6: Direct Connect & Ramps	32	22.2	57.0	0.4	1	0.4	А
SB	US93E to I-40S	6: Direct Connect & Ramps	33	32.6	57.2	0.6	1	0.6	A
EB/NB	Beale On Ramp	6: Direct Connect & Ramps	34	450.7	38.4	11.8	1	11.8	В
EB/NB	N of Beal On Ramp Merge	3: Freeway (free lane selection)	35	2576.4	51.9	49.6	2	24.8	С
EB/NB	Between Beale TI	3: Freeway (free lane selection)	36	2125.0	65.7	32.3	2	16.2	В
SB	US93E to I-40S Ramp	6: Direct Connect & Ramps	37	32.7	57.1	0.6	1	0.6	A
SB	US93E to I-40S Ramp	6: Direct Connect & Ramps	38	32.7	58.8	0.6	1	0.6	Α
WB/SB	Between Beale TI	3: Freeway (free lane selection)	40	2469.1	51.3	48.1	2	24.1	С
WB/SB	Beale Off Ramp	6: Direct Connect & Ramps	41	404.9	50.4	8.0	1	8.0	A
WB/SB	Beale Off Ramp	6: Direct Connect & Ramps	42	411.6	46.5	8.9	1	8.9	А
WB/SB	Beale Off Ramp	6: Direct Connect & Ramps	43	405.2	46.9	8.6	3	2.9	А
WB/SB	Beale Off Ramp	6: Direct Connect & Ramps	44	345.0	46.3	7.4	2	3.7	A
WB	I-40N to US93W	6: Direct Connect & Ramps	45	22.0	57.7	0.4	1	0.4	A
EB/NB	Between Beale TI	3: Freeway (free lane selection)	46	2133.2	65.6	32.5	2	16.2	В
EB/NB	Between Beale TI	3: Freeway (free lane selection)	47	2128.8	64.6	32.9	2	16.5	В

WB	I-40N to US93W	6: Direct Connect & Ramps	48	22.1	56.9	0.4	1	0.4	Α
WB/SB	Between Beale TI	8: Merge	49	2426.8	55.5	43.7	3	14.6	В
EB/NB	Beale On Ramp	6: Direct Connect & Ramps	50	452.9	54.6	8.3	1	8.3	А
EB/NB	S of Beale TI	3: Freeway (free lane selection)	51	2320.2	75.6	30.7	2	15.3	В
EB/NB	S of Beale TI	3: Freeway (free lane selection)	52	2221.8	65.8	33.7	2	16.9	В
EB/NB	Beale Off Ramp	6: Direct Connect & Ramps	53	156.5	51.7	3.0	1	3.0	А
WB/SB	Between Beale TI	3: Freeway (free lane selection)	54	2413.5	61.6	39.2	2	19.6	С
WB/SB	S of Beale TI	8: Merge	55	2561.8	62.8	40.8	3	13.6	В
WB/SB	Beale on Ramp	6: Direct Connect & Ramps	56	131.4	52.0	2.5	1	2.5	А
WB/SB	I-40N to US93W Merge Area	8: Merge	57	1761.1	58.2	30.3	3	10.1	В
EB/NB	S of Beale TI	3: Freeway (free lane selection)	58	2576.2	64.8	39.8	2	19.9	С
WB	Beale St	1: Urban (motorized)	59	70.9	53.5	1.3	2	0.7	Α
WB	Beale St	1: Urban (motorized)	60	71.4	57.1	1.2	2	0.6	Α
EB	Beale St	1: Urban (motorized)	61	80.4	57.0	1.4	2	0.7	А
EB	Beale St	1: Urban (motorized)	62	79.7	57.0	1.4	2	0.7	Α
WB/SB	US93 E of Beale St Merge	6: Direct Connect & Ramps	63	1738.6	56.0	31.0	2	15.5	В
WB	I-40N to US93W	6: Direct Connect & Ramps	64	22.5	57.3	0.4	1	0.4	Α
WB/SB	US93 E of Beale St Merge	3: Freeway (free lane selection)	65	1734.6	64.4	26.9	2	13.5	В
WB/SB	US93 E of Beale St Merge	6: Direct Connect & Ramps	66	1727.0	56.0	30.8	2	15.4	В
WB	Beale St	1: Urban (motorized)	67	70.5	57.2	1.2	2	0.6	Α
WB	Beale St ramp to US93	6: Direct Connect & Ramps	68	66.0	57.2	1.2	1	1.2	Α
WB	Beale St ramp to US93	6: Direct Connect & Ramps	69	71.2	57.2	1.2	1	1.2	Α
EB/NB	US93 E of Beale St Merge	3: Freeway (free lane selection)	70	1441.9	66.4	21.7	2	10.9	Α
SB	US93E to I-40S	6: Direct Connect & Ramps	71	32.0	59.5	0.5	1	0.5	Α
WB/SB	US93 E of Beale St Merge	6: Direct Connect & Ramps	72	1380.2	66.4	20.8	2	10.4	В
EB	Beale St	6: Direct Connect & Ramps	73	78.8	56.8	1.4	1	1.4	Α
EB	Beale St	1: Urban (motorized)	74	78.9	57.6	1.4	2	0.7	Α
EB	US93 Ramp to Beale St	6: Direct Connect & Ramps	75	80.6	56.9	1.4	1	1.4	Α
EB/NB	US93 W of Beale St Merge	3: Freeway (free lane selection)	76	1498.7	65.9	22.7	2	11.4	В
EB/NB	US93 E of Beale St Merge	3: Freeway (free lane selection)	77	1438.9	66.3	21.7	2	10.8	Α
EB	US93 Ramp to Beale St	6: Direct Connect & Ramps	78	80.1	58.1	1.4	1	1.4	Α
WB/SB	Beale St to US93 Merge Area	8: Merge	79	1825.1	65.3	27.9	3	9.3	Α
WB	Beale St ramp to US93	6: Direct Connect & Ramps	80	70.8	60.3	1.2	1	1.2	Α
WB/SB	West of Beal St Merge	3: Freeway (free lane selection)	82	1826.2	65.7	27.8	2	13.9	В
WB/SB	East of Beal St Merge	3: Freeway (free lane selection)	84	1755.8	64.9	27.1	2	13.5	В
EB/NB	West of Beale St Merge	3: Freeway (free lane selection)	85	1412.5	64.8	21.8	2	10.9	Α
EB/NB	West of Beale St Merge	3: Freeway (free lane selection)	86	1507.6	64.6	23.3	3	7.8	Α
EB/NB	West of Beale St Merge	3: Freeway (free lane selection)	87	1490.9	58.6	25.5	1	25.5	С
WB/SB	West of Beale St Merge	3: Freeway (free lane selection)	88	1849.2	65.5	28.2	2	14.1	В
WB/SB	West of Beale St Merge	3: Freeway (free lane selection)	91	1829.5	65.5	27.9	3	9.3	Α
WB/SB	US93 West of 68 Split	3: Freeway (free lane selection)	92	709.6	66.5	10.7	2	5.3	А
WB/SB	S 93 ramp to 68	3: Freeway (free lane selection)	94	1047.3	66.1	15.8	2	7.9	Α
WB/SB	US93 West of 68 Split	3: Freeway (free lane selection)	95	764.0	66.7	11.5	2	5.7	Α
NB	68 Loop to US93	6: Direct Connect & Ramps	96	27.1	27.6	1.0	1	1.0	Α
WB/SB	68 Loop to US93 Merge	8: Merge	99	787.4	65.9	11.9	3	4.0	А
WB/SB	US93 W of 68 Interchange	3: Freeway (free lane selection)	100	793.7	66.9	11.9	2	5.9	Α

WB	US93 Loop to 68	6: Direct Connect & Ramps	101	1072.9	58.5	18.3	2	9.2	Α
WB	US93 Loop to 68	6: Direct Connect & Ramps	102	1074.1	46.5	23.1	2	11.5	В
EB/NB	US93 W of 68 Split	3: Freeway (free lane selection)	103	869.6	77.0	11.3	2	5.6	Α
WB/SB	US93 W of 68 Split	6: Direct Connect & Ramps	104	155.0	69.0	2.2	1	2.2	Α
EB/NB	US93 W of 68 Interchange	3: Freeway (free lane selection)	105	701.6	76.9	9.1	2	4.6	Α
WB/SB	US93 W of 68 Split	6: Direct Connect & Ramps	106	155.2	57.2	2.7	2	1.4	Α
WB	US93 Ramp to 68	6: Direct Connect & Ramps	107	47.5	57.1	0.8	1	0.8	Α
EB	US93 Ramp to Truck Stop	6: Direct Connect & Ramps	108	124.0	57.0	2.2	1	2.2	Α
WB/SB	US93 to 68 Merge Area	8: Merge	109	1117.9	52.2	21.4	3	7.1	Α
WB/SB	68 W of Interchange	3: Freeway (free lane selection)	111	1129.9	63.3	17.8	2	8.9	Α
EB/NB	68 Ramp to Truck Stop	6: Direct Connect & Ramps	113	43.2	59.9	0.7	1	0.7	Α
EB/NB	Truck Stop	3: Freeway (free lane selection)	114	160.6	56.9	2.8	1	2.8	Α
EB/NB	68 W of Interchange	3: Freeway (free lane selection)	115	702.6	76.6	9.2	2	4.6	Α
EB/NB	68 Ramp to US93	6: Direct Connect & Ramps	116	644.6	58.7	11.0	1	11.0	В
WB	68 Loop to US93	6: Direct Connect & Ramps	117	26.7	59.6	0.4	1	0.4	Α
EB/NB	US93 W of Beale St	3: Freeway (free lane selection)	118	1325.7	68.7	19.3	2	9.6	Α
EB/NB	US93 W of Beale St	3: Freeway (free lane selection)	119	1298.3	68.9	18.8	3	6.3	Α
EB/NB	Truck Stop	3: Freeway (free lane selection)	120	167.6	57.8	2.9	1	2.9	Α
WB/SB	I-40 Ramp to US93	6: Direct Connect & Ramps	121	1732.4	52.4	33.1	2	16.5	В

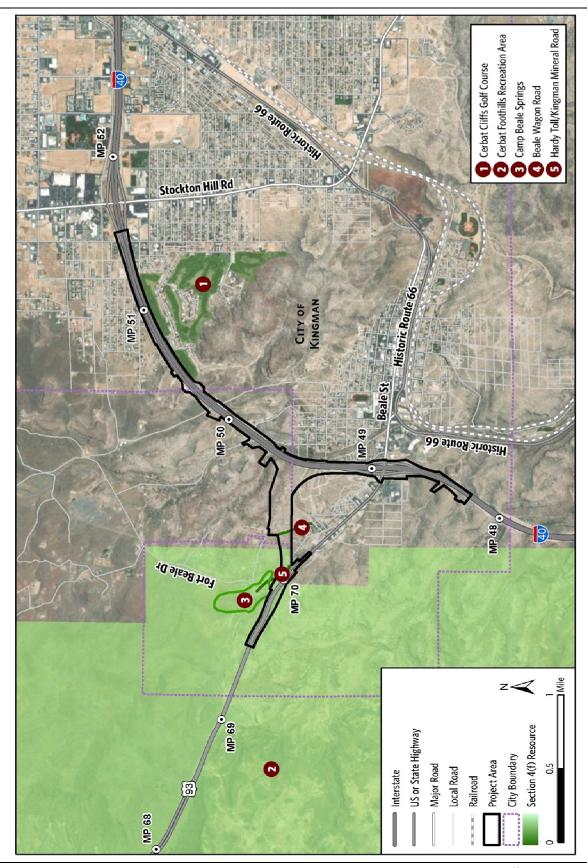
APPENDIX E – TNM 2.5 NOISE MODEL RUN FILE KEY

Note: files to be uploaded to ADOT EP Noise Specialist via ftp

H7993: I-40/US 93 West Kingman System Traffic Interchange – TNM FILE KEY					
File Folder	Run Name	Contents			
Existing Master 2019	Master file	All geometry			
	R1 – R92	Unmitigated			
	R1 rev	Updated R1			
	KITEV	unmitigated			
	R93 – R167	Unmitigated			
	R168 – R228	Unmitigated			
	R229 – R287	Unmitigated			
Validation	Master file	All geometry			
	M1	Unmitigated			
	M1a	Unmitigated			
	M2	Unmitigated			
	M3	Unmitigated			
	M4	Unmitigated			
	M5	Unmitigated			
	M6	Unmitigated			
No Build Master 2042	Master file	All geometry			
	R1 – R92	Unmitigated			
	D1 rov	Updated R1			
	R1 rev	unmitigated			
	R93 – R167	Unmitigated			
	R168 – R228	Unmitigated			
	R229 – R287	Unmitigated			
Build Master 2042	Master file	All geometry			
		R18 – R39,			
	R1 – R92	R75 – R92			
		unmitigated			
	R1 – R92 NW#r&e	R1 – R17, R40 – R74			
	NI - NJZ NVV#IQE	unmitigated			
	R93 – R167	Unmitigated			
	R168 – R228	Unmitigated			
	R229 – R287	Unmitigated			
Mitigation	Master file	All base geometry			
Mitigation	iviastei ille	(no barriers)			
	NB #1	Noise barrier eval			
	NB #2	Noise barrier eval			
	NB #3	Noise barrier eval			
	NB #4	Noise barrier eval			
	ND #E control	Noise barrier eval			
	NB #5 central	central recs			
	NP #5 cast	Noise barrier eval			
	NB #5 east	east end recs			

H7993: I-40/US 93 West Kingman System Traffic Interchange – TNM FILE KEY					
	NB #1 R123gc-4 129gcs	Noise barrier eval (listed receivers, west end)			
	NB #5 west	Noise barrier eval west end recs			
	NB #6 central	Noise barrier eval central recs			
	NB #6 east	Noise barrier eval east end recs			
	NB #6 west	Noise barrier eval west end recs			
	NB #7	Noise barrier eval			
	NB #8	Noise barrier eval			
	NB #9	Noise barrier eval			

APPENDIX F – SELECTION OF 4(F) RECEIVERS IN THE PROJECT AREA





Certificate Of Completion

Envelope Id: 91C6BF0EB2F647EA9A56D010270154D9

Subject: Approved_I-40 West Kingman TI Noise Analysis Technical Report Draft_02262020.pdf

Source Envelope:

Document Pages: 96 Certificate Pages: 2

AutoNav: Disabled

Envelopeld Stamping: Disabled Time Zone: (UTC-07:00) Arizona Signatures: 1

Initials: 0

Status: Completed

Envelope Originator:

Ivan Racic 206 S 17th Ave Phoenix, AZ 85007

IRacic@azdot.gov

IP Address: 162.59.200.193

Record Tracking

Status: Original

2/26/2020 1:04:28 PM

Holder: Ivan Racic IRacic@azdot.gov Location: DocuSign

Signer Events

Ivan Racic iracic@azdot.gov

Air and Noise Planner/Environmental planning

Arizona Dept of Transportation

Security Level: Email, Account Authentication

(None)

Signature

Ivan Racie D00D4A7BCC34420..

Signature Adoption: Pre-selected Style Using IP Address: 162.59.200.193

Timestamp

Sent: 2/26/2020 1:05:12 PM Viewed: 2/26/2020 1:05:20 PM Signed: 2/26/2020 1:08:27 PM

Freeform Signing

Electronic Record and Signature Disclosure:

Not Offered via DocuSign

In Person Signer Events

Signature **Timestamp**

Editor Delivery Events Status Timestamp

Agent Delivery Events Status Timestamp

Intermediary Delivery Events Status Timestamp

Certified Delivery Events Status Timestamp

Carbon Copy Events Status Timestamp

COPIED

COPIED

Dena Whitaker

dwhitaker@azdot.gov

ADOT

Security Level: Email, Account Authentication

(None)

Electronic Record and Signature Disclosure:

Not Offered via DocuSign

Joe D'Onofrio

joe.donofrio@jacobs.com

Security Level: Email, Account Authentication

(None)

Electronic Record and Signature Disclosure:

Sent: 2/26/2020 1:08:29 PM

Sent: 2/26/2020 1:08:29 PM Viewed: 2/26/2020 1:09:24 PM

Not Offered via DocuSign

Witness Events Signature **Timestamp**

Notary Events Signature Timestamp

Envelope Summary Events	Status	Timestamps
Envelope Sent	Hashed/Encrypted	2/26/2020 1:08:29 PM
Certified Delivered	Security Checked	2/26/2020 1:05:20 PM
Signing Complete	Security Checked	2/26/2020 1:08:29 PM
Completed	Security Checked	2/26/2020 1:08:29 PM
Payment Events	Status	Timestamps